

January 30, 2019

VIA ELECTRONIC FILING

Ms. Kimberly D. Bose, Secretary Federal Energy Regulatory Commission 888 First Street, NE Washington, DC 20426

Re: Public Service Company of Colorado
Southwestern Public Service Company
Xcel Energy Operating Companies Joint Open Access Transmission Tariff
Revisions to Wholesale Real Power Losses for Southwestern Public Service Company
Docket No. ER19-____-000

Dear Secretary Bose:

Pursuant to Section 205 of the Federal Power Act ("FPA"), Part 35 of the regulations of the Federal Energy Regulatory Commission ("FERC" or "Commission"), and Order No. 714, helic Service Company of Colorado ("PSCo"), on behalf of Southwestern Public Service Company ("SPS"), hereby submits eTariff records revising Sections 15.7 and 28.5 of the Xcel Energy Operating Companies Open Access Transmission Tariff ("Xcel Energy Tariff" or "Tariff"). The revisions update the stated real power loss percentages ("loss factors") for service on the SPS system so they (i) are based on the most recent study of SPS system losses, and (ii) are consistent with the loss factors approved for and reflected in SPS's retail rates in Texas and New Mexico.

SPS respectfully requests that the Commission accept the proposed tariff revisions for filing effective April 1, 2019, sixty (60) days after filing, without suspension.

² 18 C.F.R. § 35.13 (2018).

¹ 16 U.S.C. § 824d.

Electronic Tariff Filings, FERC Stats. & Regs. ¶ 31,276 (2008).

PSCo is the designated eTariff filing entity for the Xcel Energy OATT consistent with the requirements of Order No. 714. PSCo is a party to this filing solely as the eTariff filing entity.

⁵ Xcel Energy Operating Companies, FERC Electric Tariff, Third Revised Volume No. 1.

I. BACKGROUND

SPS is a New Mexico corporation and a wholly owned subsidiary of Xcel Energy Inc. ("Xcel Energy"). SPS is an operating utility engaged in, *inter alia*, the generation, purchase, transmission, distribution and sale of electricity to approximately 390,000 retail customers in portions of Texas and New Mexico. SPS also sells electric power and provides transmission service at wholesale to other utilities and electric cooperatives in Texas, New Mexico, Kansas, and Oklahoma.

SPS is a transmission-owning member of the Southwest Power Pool, Inc. ("SPP"), a FERC-approved Regional Transmission Organization ("RTO"). Transmission service over the SPS transmission system has been available under the SPP Open Access Transmission Tariff ("SPP Tariff") since June 2000.

Xcel Energy Services Inc. ("XES") is the centralized service company subsidiary of Xcel Energy and, as such, performs an array of administrative and general services on behalf of the Xcel Energy Operating Companies. Among other things, XES submits filings with and appears in proceedings before the Commission on behalf of SPS.

II. REASONS FOR THIS FILING

A. Updated Transmission and Distribution Loss Study.

The primary reason for this filing is to ensure that the transmission and distribution real power losses charged to SPS's wholesale customers reflect the most recent analysis of the losses SPS experiences in providing such services and are consistent with the loss factors reflected in SPS's retail rates in Texas and New Mexico. As discussed further by SPS Witness Mr. Wesley L. Berger, the existing Transmission and Distribution System – Primary Voltage real power loss factors set out in the Xcel Energy Tariff applicable to SPS were accepted effective May 1, 2016, Docket No. ER16-1030-000.⁷ The real power loss factors established in that docket were based on a loss study that analyzed data for the period from July 2012 through June 2013 (the "2013 Loss Study").

The updated real power loss factors contained in this filing are based upon the most recent SPS loss study, completed in 2017 for the period of January 2016 through December 2016 (the "2016 Loss Study"). The 2016 Loss Study uses the same methodology as the 2013 Loss Study, with minor enhancements discussed by SPS Witness Mr. Duane J. Ripperger, and was accepted by the retail regulatory agencies with jurisdiction over SPS in 2018: the Public Utility Commission of Texas ("PUCT") and the New Mexico Public Regulation Commission

The Xcel Energy Operating Companies are: SPS, PSCo, and Northern States Power Company, a Minnesota corporation, and Northern States Power Company, a Wisconsin corporation (collectively, the "NSP Companies"). The instant filing does not affect the rates for transmission service on the PSCo or NSP Companies' systems.

Public Service Company of Colorado, Docket No. ER16-1030-000, delegated letter order (April 28, 2016).

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("NMPRC"). SPS then began to prepare this filing to similarly update the loss factors used in calculating wholesale rates.

As discussed more fully by Mr. Ripperger, the 2016 Loss Study quantifies, through engineering analysis and calculations, the physical power and energy losses that occurred on the SPS transmission and distribution system during the study period. The 2016 Loss Study reflects the impacts of changes to the SPS system since the 2013 Loss Study, including initiation of the SPP Integrated Marketplace, installation of new 345 kV transmission facilities, and increased wind and solar generation, including generation connected to the SPS distribution system. ⁹ Implementing the updated loss factors in the Xcel Energy Tariff will provide for consistent allocations of costs between the three SPS rate jurisdictions: FERC wholesale, Texas retail, and New Mexico retail.

B. Summary of Current and Proposed Real Power Loss Factors.

The real power demand and energy loss factors for service on the SPS transmission system ("Transmission Loss Factors") are stated as percentage values in Sections 15.7 and 28.5 of the Xcel Energy Tariff and incorporated into Attachment M, Appendix 1 of the SPP Tariff. The real power demand and energy loss factors for service on the SPS distribution system ("Distribution Loss Factors"), applicable to those SPS wholesale customers taking service at primary distribution voltage, are also stated in Sections 15.7 and 28.5 of the Xcel Energy Tariff. As discussed by Mr. Berger, the transmission loss factors total two transmission level loss factors described in the 2016 Loss Study into a composite transmission loss factor for the Xcel Energy Tariff and the SPP Tariff. ¹⁰

As noted, the currently effective Transmission Loss Factors and Distribution Loss Factors accepted in Docket No. ER16-1030-000 were based on the 2013 Loss Study. ¹¹ In this filing, SPS proposes to update the Transmission Loss Factors and Distribution Loss Factors with the values derived from the 2016 SPS Loss Study and accepted by the PUCT and NMPRC. The following table shows SPS's currently effective and proposed loss demand and energy factors:

See In the Matter of Southwestern Public Service Company's Application for Revision of its Retail Electric Rates Pursuant to Advice Notice No. 272, NMPRC Case No. 17-00255-UT, Final Order Adopting Recommended Decision (September 5, 2018); and Application of Southwestern Public Service Company for Authority to Change Rates, PUCT Docket No. 47527, Final Order (December 10, 2018).

Direct Testimony of Duane J. Ripperger, Exhibit No. SPS-0004 at PP. 15-17.

Direct Testimony of Wesley L. Berger ("Berger Direct Testimony), Exhibit No. SPS-0001 at P. 10.

See fn. 8. The 2013 Loss Study used the same methodology (with certain enhancements) that had been used by SPS in a 2009 Loss Study that supported SPS's updated loss factors accepted effective December 1, 2012, pursuant to a Commission-approved uncontested settlement in Docket No. ER12-1682-000. See Public Service Company of Colorado, 142 FERC ¶ 61,099 (2013).

Table 1 – Current and Proposed Loss Factors

	Demand Loss Factors		Energy 1	Loss Factors
	Current	<u>Proposed</u>	Current	Proposed
Transmission	3.107161%	2.738606%	2.881556%	3.203203%
Distribution –	8.157751%	8.846390%	6.035731%	6.327826%
Primary Voltage				

C. Impact of Proposed Tariff Revisions on Wholesale Customers.

The proposed updated Transmission and Distribution Loss Factors affect network transmission service customers in SPP Zone 11 who purchase transmission service under the SPP Tariff as well as wholesale production service customers who purchase power from SPS under wholesale requirements power sale agreements at the transmission and distribution level. The Tariff revisions will affect the calculations of billing demands for both network transmission service under the SPP Tariff and wholesale production services provided by SPS. Specifically, the updated loss factors affect these wholesale power supply services because the loss factors are included in the calculation of how much energy each wholesale customer is purchasing under its power supply agreement. Therefore, although this filing is not amending these power supply agreements, the updated real power loss factors will affect the calculation of charges pursuant to the power supply agreements' existing terms.

Initially, SPS estimates the updated loss factors together will result in a net decrease in the overall annual costs to wholesale customers of approximately \$230,700, or approximately 0.07 percent. The overall charges to network transmission service customers under the SPP Tariff in Zone 11 (the SPS zone) will be reduced due to the reduction in the transmission Demand Loss Factor. The impact of the revised real power loss factors on wholesale production customers is a small annual cost increase. Exhibit No. SPS-0003 calculates the estimated impact by SPS wholesale customer using the revised loss factors applied to 2018 billings. 15

The affected wholesale transmission service customers in Zone 11 are: Golden Spread Electric Cooperative, Inc. (for itself and Tri-County Electric Cooperative, Inc.); Farmers' Electric Cooperative, Inc.; Lea County Electric Cooperative, Inc.; Central Valley Electric Cooperative, Inc.; Roosevelt County Electric Cooperative, Inc.; and West Texas Municipal Power Agency. All of these network transmission service customers also purchase power from SPS pursuant to Commission-approved cost-based wholesale requirements power supply sale agreements. Golden Spread purchases wholesale requirements power only for its Tri-County Electric Cooperative, Inc. member load.

For example, see the Replacement Power Sales Agreement between SPS and Central Valley Electric Cooperative dated January 15, 2010, SPS Electric Rate Schedule 114, Service Schedule A, Sections 3, 4, 5, and 6.

See Exhibit No. SPS-0003.

Berger Direct Testimony, Exhibit No. SPS-0001 at P. 14. The net impact to each wholesale customer is an estimated cost reduction, with the exception of Central Valley Electric Cooperative, Inc. ("Central Valley"). Central Valley is estimated to see a small total cost increase – approximately \$6800 compared to

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Notably, the proposed Tariff revisions will not affect the collection of energy losses for transmission services under the SPP Tariff. Under Section II.(b) of Attachment M to the SPP OATT, energy losses are determined by the SPP regional system dispatch and included in the locational marginal prices charged to market participants, including SPS and network customers on the SPS system. The revised Energy loss factors affect only the allocation of SPS system energy costs between SPS wholesale production and retail customers.

D. Stakeholder Communications

In addition to being stated in the Xcel Energy Tariff, the SPS Transmission Demand loss factor is included in Attachment M (Loss Compensation Procedure), Appendix 1, to the SPP Tariff. SPS will work with SPP to file to modify Attachment M, Appendix 1 to the SPP Tariff to reflect the updated SPS transmission demand loss factors for purposes of calculating monthly billing determinants for the wholesale loads taking network service in the SPS rate zone (Zone 11). SPS discussed the need for this revision to Attachment M, Appendix 1 with SPP, and SPP has indicated it expects to submit companion changes to the SPP Tariff shortly after SPS submits this filing, to be effective on the same effective date approved by the Commission in this proceeding.

Prior to submitting this filing, on January 18, 2019, SPS also provided information to its wholesale transmission and production customers to notify them of the proposed changes to the SPS real power losses factors and the anticipated financial impact to each affected wholesale customer, and offered to hold individual meetings with each wholesale customer. ¹⁷

E. The Tariff Revisions Should be Accepted for Filing

For the reasons stated above, SPS requests that the Commission accept the proposed changes to Sections 15.7 and 28.5 of the Xcel Energy Tariff for filing, to be subsequently incorporated into Attachment M, Appendix 1 of the SPP Tariff. The proposed revisions are further explained in the attached Testimonies and Exhibits of Mr. Wesley L. Berger and Mr. Duane J. Ripperger in support of the instant filing, including the 2016 Loss Study included as Exhibit No. SPS-0005 to Mr. Ripperger's testimony. As noted, the 2016 Loss Study uses the same basic methodology used in the 2013 Loss Study supporting SPS's currently effective real power loss factors in Sections 15.7 and 28.5, with certain refinements discussed by Mr. Ripperger.

total transmission service and production service billings of \$29.97 million – because of the high load factor at which Central Valley purchases energy from SPS. *Id.* at P. 15.

Berger Direct Testimony, Exhibit SPS-0001 at P. 6. Attachment M, Appendix 1 refers to a Delivery Loss Factor ("DLF") and an Injection Loss Factor ("ILF"). The ILF equals the SPS Demand Loss factor stated in Section 15.7 and 28.5. The DLF is calculated as 1/(1-ILF)-1. So an SPS transmission demand real power loss factor (ILF) of 2.738606% would result in an SPP DLF of 2.8115717%. *Id.* at PP. 12-13.

Berger Direct Testimony, Exhibit SPS-0001 at P. 15.

III. ADDITIONAL INFORMATION SUBMITTED IN SUPPORT OF FILING

A. Information Required by Section 35.13 of the Commission's Regulations, 18 C.F.R. § 35.13

1. Contents of Filing – Section 35.13(b)(1)

In addition to this transmittal letter, the filing consists of the following:

- Electronic marked and clean versions of Sections 15 and 28 of the Xcel Energy Tariff in eTariff format, including the revisions to Section 15.7 and 28.5;
- the testimony, exhibits and affidavit of Mr. Wesley L. Berger (Exhibit Nos. SPS-0001, SPS-0002, and SPS-0003); and
- the testimony, exhibit and affidavit of Mr. Duane J. Ripperger (Exhibit Nos. SPS-0004 and SPS-0005), including the 2016 Loss Study.

B. Requested Effective Date – Section 35.13(b)(2)

SPS respectfully requests that the Commission allow the proposed revised Tariff revisions to be effective April 1, 2019, sixty (60) days after filing, without suspension or condition for good cause shown. As noted, the transmission Demand Loss change will result in a small reduction in fixed charges to network transmission service customers (due to lower billing determinants after adjusting for transmission demand losses), and overall the proposed loss factors result in a net cost decrease to SPS wholesale customers of approximately \$230,700 annually. The revised real power loss factors reflect the most current SPS system loss study available, and will provide for consistent cost allocations between the three SPS rate jurisdictions (FERC wholesale, Texas retail and New Mexico retail).

If the Commission nonetheless believes a suspension is warranted, SPS respectfully asks that the Commission allow the proposed revised tariff provisions to become effective April 1, 2019, subject to refund, after only a nominal suspension. In *West Texas Utilities Co.*, the Commission explained that a minimal suspension period is justified in cases where no more than ten percent of the proposed increase appears to be excessive. ¹⁹ The overall rate change proposed here is negligible (-0.072 percent), and no portion of the minimal change in charges is excessive.

SPS believes the materials submitted herewith comply with the Commission's filing requirements and will permit the Commission to review the proposed revisions and determine them to be just and reasonable. SPS respectfully requests waiver of any applicable filing or notice requirements under the Commission's Rules and Regulations as may be necessary to accept the proposed revisions to the Xcel Energy Tariff on the date requested.

See Exhibit No. SPS-0003.

¹⁹ *West Texas Utilities Co.*, 18 FERC ¶ 61,189, at 61,375 (1982).

1. The Names and Addresses of Persons to Whom a Copy of the Rate Change Has Been Posted – Section 35.13(b)(3)

An electronic notice of this filing will be served on the state commissions with jurisdiction over SPS. Electronic notice of this filing will also be provided to SPP and all network transmission service customers taking service under the SPP Tariff in the SPS rate zone (Zone 11), and on SPS's wholesale production service customers. A courtesy copy or notice will be served on the Commission's Director of the Division of Tariffs and Market Development (Central).

In addition, pursuant to 18 C.F.R. § 35.2(d), a copy of this filing will be available for public inspection at the offices of SPS in Amarillo, Texas. Finally, a copy of this filing will be posted at the Open Access Transmission Tariff link at the Xcel Energy Transmission website: (www.transmission.xcelenergy.com/Resources/Open-Access-Same-Time-Information-System-&-Open-Access-Transmission-Tariff).

2. Brief Description of Rate Change – Section 35.13(b)(4)

See Sections II and III above.

3. Statement of Reasons for Rate Change – Section 35.13(b)(5)

See Sections II and III above.

4. Requisite Agreement for Rate Change – Section 35.13(b)(6)

See Section II above.

5. Statement Showing Expenses or Costs Included in Cost-of-Service Statements – Section 35.13(b)(7)

None of the costs related to this filing have been alleged in any administrative or judicial proceeding to be illegal, duplicative, or unnecessary costs that are demonstrably the product of discriminatory practices.

C. Communications and Service

Please direct any communication or correspondence with respect to this filing to the following: 20

SPS respectfully requests waiver of 18 C.F.R. Section 385.203(b)(3) of the Commission's regulations to permit the designation of more than two persons upon whom service is to be made in this proceeding.

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IV. **CONCLUSION**

For the reasons stated above, SPS requests that the Commission accept the proposed revisions to Sections 15.7 and 28.5 of the Xcel Energy Tariff to update SPS's Transmission Loss Factors and the Distribution System - Primary Voltage Loss Factors effective April 1, 2019.

SPS appreciates the Commission's prompt attention to this matter. Please direct any questions regarding this filing to the undersigned at (806) 378-2891 or Ms. Tracee Holte at (612) 330-6206.

Respectfully submitted,

/s/ Wesley Berger

Wesley Berger Manager, Rate Cases Southwestern Public Service Company

Cc: State Commissions service list

SPS Transmission and Production customers

Southwest Power Pool, Inc.

Director, Division of Tariffs and Market Development (Central)

CERTIFICATE OF SERVICE

I, Elizabeth A. Walkup, hereby certify that I have this day electronically served a notice of the foregoing document via email on the Public Utility Commission of Texas, the New Mexico Public Regulation Commission, Southwest Power Pool, Inc., all SPS wholesale transmission customers within the SPS pricing zone taking service under the SPP OATT, and all SPS wholesale production customers.

Dated at Minneapolis, Minnesota this 30th day of January 2019.

/s/ Elizabeth A. Walkup Elizabeth A. Walkup Business Analyst Xcel Energy Services Inc. 414 Nicollet Mall Minneapolis, MN 55401 Tel: 612-330-6780

Elizabeth.A.Walkup@xcelenergy.com

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Proposed Effective Date: 4/1/2019

Part II, Section 15
Service Availability
Version 0.3.0
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15 Service Availability

- **General Conditions:** The Transmission Provider will provide Firm and Non-Firm Point-To-Point Transmission Service over, on or across its Transmission System to any Transmission Customer that has met the requirements of Section 16.
- **Determination of Available Transfer Capability:** A description of the Transmission Provider's specific methodology for assessing available transfer capability posted on the Transmission Provider's OASIS (Section 4) is contained in Attachment C of the Tariff. In the event sufficient transfer capability may not exist to accommodate a service request, the Transmission Provider will respond by performing a System Impact Study.
- 15.3 Initiating Service in the Absence of an Executed Service Agreement: If the Transmission Provider and the Transmission Customer requesting Firm or Non-Firm Point-To-Point Transmission Service cannot agree on all the terms and conditions of the Point-To-Point Service Agreement, the Transmission Provider shall file with the Commission, within thirty (30) days after the date the Transmission Customer provides written notification directing the Transmission Provider to file, an unexecuted Point-To-Point Service Agreement containing terms and conditions deemed appropriate by the Transmission Provider for such requested Transmission Service. The Transmission Provider shall commence providing Transmission Service subject to the Transmission Customer agreeing to (i) compensate the Transmission Provider at whatever rate the Commission ultimately determines to be just and reasonable, and (ii) comply with the terms and conditions of the Tariff including posting appropriate security deposits in accordance with the terms of Section 17.3.
- 15.4 Obligation to Provide Transmission Service that Requires Expansion or Modification of the Transmission System, Redispatch or Conditional Curtailment:
 - (a) If the Transmission Provider determines that it cannot accommodate a Completed Application for Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will use due diligence to expand or modify its Transmission System to provide the requested Firm Transmission Service, consistent with its planning obligations in Attachment R, provided the Transmission Customer agrees to compensate the Transmission Provider for such costs pursuant to the terms of Section 27. The Transmission Provider will conform to Good Utility Practice and its planning obligations in Attachment R, in determining the need for new facilities and in the design and construction of such facilities. The obligation applies only to those facilities that the Transmission Provider has the right to expand or modify.
 - (b) If the Transmission Provider determines that it cannot accommodate a

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Completed Application for Long-Term Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will use due diligence to provide redispatch from its own resources until (i) Network Upgrades are completed for the Transmission Customer, (ii) the Transmission Provider determines through a biennial reassessment that it can no longer reliably provide the redispatch, or (iii) the Transmission Customer terminates the service because of redispatch changes resulting from the reassessment. A Transmission Provider shall not unreasonably deny self-provided redispatch or redispatch arranged by the Transmission Customer from a third party resource.

- (c) If the Transmission Provider determines that it cannot accommodate a Completed Application for Long-Term Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will offer the Firm Transmission Service with the condition that the Transmission Provider may curtail the service prior to the curtailment of other Firm Transmission Service for a specified number of hours per year or during System Condition(s). If the Transmission Customer accepts the service, the Transmission Provider will use due diligence to provide the service until (i) Network Upgrades are completed for the Transmission Customer, (ii) the Transmission Provider determines through a biennial reassessment that it can no longer reliably provide such service, or (iii) the Transmission Customer terminates the service because the reassessment increased the number of hours per year of conditional curtailment or changed the System Conditions.
- **Deferral of Service:** The Transmission Provider may defer providing service until it completes construction of new transmission facilities or upgrades needed to provide Firm Point-To-Point Transmission Service whenever the Transmission Provider determines that providing the requested service would, without such new facilities or upgrades, impair or degrade reliability to any existing firm services.
- 15.6 Other Transmission Service Schedules: Eligible Customers receiving transmission service under other agreements on file with the Commission may continue to receive transmission service under those agreements until such time as those agreements may be modified by the Commission.

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Real Power Losses: Real Power Losses are associated with all transmission service. The Transmission Provider is not obligated to provide Real Power Losses. The Transmission Customer is responsible for replacing losses associated with all transmission service as calculated by the Transmission Provider. The applicable Real Power Losses are as follows:

For Service on the NSP Transmission System: 2.4%

For Service on the PSCo System:

Transmission System: Demand 2.20% 1.70%
Distribution System – Primary Voltage: 3.75% 2.07%

For Service on the SPS System:

<u>Demand</u> <u>Energy</u> 2.7386063.107161%

Transmission System: 3.2032032.881556%

Distribution System – Primary Voltage: 8.8463908.157751%

6.3278266.035731%

The loss factors for Direct Assignment Facilities shall be determined on a case by case basis.

Part III, Section 28
Nature of Network Integration Transmission Service
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28 Nature of Network Integration Transmission Service

- **Scope of Service**: Network Integration Transmission Service is a transmission service that allows Network Customers to efficiently and economically utilize their Network Resources (as well as other non-designated generation resources) to serve their Network Load located in the Transmission Provider's Control Area and any additional load that may be designated pursuant to Section 31.3 of the Tariff. The Network Customer taking Network Integration Transmission Service must obtain or provide Ancillary Services pursuant to Section 3.
- 28.2 Transmission Provider Responsibilities: The Transmission Provider will plan, construct, operate and maintain its Transmission System in accordance with Good Utility Practice and its planning obligations in Attachment R in order to provide the Network Customer with Network Integration Transmission Service over the Transmission Provider's Transmission System. Transmission Provider, on behalf of its Native Load Customers, shall be required to designate resources and loads in the same manner as any Network Customer under Part III of this Tariff. This information must be consistent with the information used by the Transmission Provider to calculate available transfer capability. The Transmission Provider shall include the Network Customer's Network Load in its Transmission System planning and shall, consistent with Good Utility Practice and Attachment R, endeavor to construct and place into service sufficient transfer capability to deliver the Network Customer's Network Resources to serve its Network Load on a basis comparable to the Transmission Provider's delivery of its own generating and purchased resources to its Native Load Customers.
- 28.3 Network Integration Transmission Service: The Transmission Provider will provide firm transmission service over its Transmission System to the Network Customer for the delivery of capacity and energy from its designated Network Resources to service its Network Loads on a basis that is comparable to the Transmission Provider's use of the Transmission System to reliably serve its Native Load Customers.
- 28.4 Secondary Service: The Network Customer may use the Transmission Provider's Transmission System to deliver energy to its Network Loads from resources that have not been designated as Network Resources. Such energy shall be transmitted, on an as-available basis, at no additional charge. Secondary service shall not require the filing of an Application for Network Integration Transmission Service under the Tariff. However, all other requirements of Part III of the Tariff (except for transmission rates) shall apply to secondary service. Deliveries from resources other than Network Resources will have a higher priority than any Non-Firm Point-To-Point Transmission Service under Part II of the Tariff.
- **28.5** Real Power Losses: Real Power Losses are associated with all transmission service. The Transmission Provider is not obligated to provide Real Power

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Losses. The Network Customer is responsible for replacing losses associated with all transmission service as calculated by the Transmission Provider. The applicable Real Power Losses are as follows:

For Service on the NSP Transmission System: 2.4%

For Service on the PSCo System:

Transmission System: Demand 2.20% 1.70%
Distribution System – Primary Voltage: 3.75% 2.07%

For Service on the SPS System:

<u>Demand</u> <u>Energy</u> 2.7386063.107161%

Transmission System: 3.2032032.881556%

Distribution System – Primary Voltage: <u>8.8463908.157751</u>%

6.3278266.035731%

The loss factors for Direct Assignment Facilities shall be determined on a case by case basis.

Restrictions on Use of Service: The Network Customer shall not use Network Integration Transmission Service for (i) sales of capacity and energy to non-designated loads, or (ii) direct or indirect provision of transmission service by the Network Customer to third parties. All Network Customers taking Network Integration Transmission Service shall use Point-To-Point Transmission Service under Part II of the Tariff for any Third-Party Sale which requires use of the Transmission Provider's Transmission System. The Transmission Provider shall specify any appropriate charges and penalties and all related terms and conditions applicable in the event that a Network Customer uses Network Integration Transmission Service or secondary service pursuant to Section 28.4 to facilitate a wholesale sale that does not serve a Network Load.

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Part II, Section 15 Service Availability Version 0.3.0 Page 1 of 3 Approved Effective Date:

15 Service Availability

- **15.1 General Conditions:** The Transmission Provider will provide Firm and Non-Firm Point-To-Point Transmission Service over, on or across its Transmission System to any Transmission Customer that has met the requirements of Section 16.
- **Determination of Available Transfer Capability:** A description of the Transmission Provider's specific methodology for assessing available transfer capability posted on the Transmission Provider's OASIS (Section 4) is contained in Attachment C of the Tariff. In the event sufficient transfer capability may not exist to accommodate a service request, the Transmission Provider will respond by performing a System Impact Study.
- 15.3 Initiating Service in the Absence of an Executed Service Agreement: If the Transmission Provider and the Transmission Customer requesting Firm or Non-Firm Point-To-Point Transmission Service cannot agree on all the terms and conditions of the Point-To-Point Service Agreement, the Transmission Provider shall file with the Commission, within thirty (30) days after the date the Transmission Customer provides written notification directing the Transmission Provider to file, an unexecuted Point-To-Point Service Agreement containing terms and conditions deemed appropriate by the Transmission Provider for such requested Transmission Service. The Transmission Provider shall commence providing Transmission Service subject to the Transmission Customer agreeing to (i) compensate the Transmission Provider at whatever rate the Commission ultimately determines to be just and reasonable, and (ii) comply with the terms and conditions of the Tariff including posting appropriate security deposits in accordance with the terms of Section 17.3.
- 15.4 Obligation to Provide Transmission Service that Requires Expansion or Modification of the Transmission System, Redispatch or Conditional Curtailment:
 - (a) If the Transmission Provider determines that it cannot accommodate a Completed Application for Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will use due diligence to expand or modify its Transmission System to provide the requested Firm Transmission Service, consistent with its planning obligations in Attachment R, provided the Transmission Customer agrees to compensate the Transmission Provider for such costs pursuant to the terms of Section 27. The Transmission Provider will conform to Good Utility Practice and its planning obligations in Attachment R, in determining the need for new facilities and in the design and construction of such facilities. The obligation applies only to those facilities that the Transmission Provider has the right to expand or modify.
 - (b) If the Transmission Provider determines that it cannot accommodate a

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Completed Application for Long-Term Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will use due diligence to provide redispatch from its own resources until (i) Network Upgrades are completed for the Transmission Customer, (ii) the Transmission Provider determines through a biennial reassessment that it can no longer reliably provide the redispatch, or (iii) the Transmission Customer terminates the service because of redispatch changes resulting from the reassessment. A Transmission Provider shall not unreasonably deny self-provided redispatch or redispatch arranged by the Transmission Customer from a third party resource.

- (c) If the Transmission Provider determines that it cannot accommodate a Completed Application for Long-Term Firm Point-To-Point Transmission Service because of insufficient capability on its Transmission System, the Transmission Provider will offer the Firm Transmission Service with the condition that the Transmission Provider may curtail the service prior to the curtailment of other Firm Transmission Service for a specified number of hours per year or during System Condition(s). If the Transmission Customer accepts the service, the Transmission Provider will use due diligence to provide the service until (i) Network Upgrades are completed for the Transmission Customer, (ii) the Transmission Provider determines through a biennial reassessment that it can no longer reliably provide such service, or (iii) the Transmission Customer terminates the service because the reassessment increased the number of hours per year of conditional curtailment or changed the System Conditions.
- **Deferral of Service:** The Transmission Provider may defer providing service until it completes construction of new transmission facilities or upgrades needed to provide Firm Point-To-Point Transmission Service whenever the Transmission Provider determines that providing the requested service would, without such new facilities or upgrades, impair or degrade reliability to any existing firm services.
- 15.6 Other Transmission Service Schedules: Eligible Customers receiving transmission service under other agreements on file with the Commission may continue to receive transmission service under those agreements until such time as those agreements may be modified by the Commission.

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Proposed Effective Date: 4/1/2019

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Real Power Losses: Real Power Losses are associated with all transmission service. The Transmission Provider is not obligated to provide Real Power Losses. The Transmission Customer is responsible for replacing losses associated with all transmission service as calculated by the Transmission Provider. The applicable Real Power Losses are as follows:

For Service on the NSP Transmission System: 2.4%

For Service on the PSCo System:

Transmission System: Demand 2.20% 1.70%
Distribution System – Primary Voltage: 3.75% 2.07%

For Service on the SPS System:

Transmission System: Distribution System – Primary Voltage: Demand 2.738606% 3.203203% 8.846390% 6.327826%

The loss factors for Direct Assignment Facilities shall be determined on a case by case basis.

Xcel Energy Operating Companies FERC FPA Electric Tariff Third Revised Volume No. 1 Part III, Section 28
Nature of Network Integration Transmission Service
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28 Nature of Network Integration Transmission Service

- **Scope of Service**: Network Integration Transmission Service is a transmission service that allows Network Customers to efficiently and economically utilize their Network Resources (as well as other non-designated generation resources) to serve their Network Load located in the Transmission Provider's Control Area and any additional load that may be designated pursuant to Section 31.3 of the Tariff. The Network Customer taking Network Integration Transmission Service must obtain or provide Ancillary Services pursuant to Section 3.
- 28.2 Transmission Provider Responsibilities: The Transmission Provider will plan, construct, operate and maintain its Transmission System in accordance with Good Utility Practice and its planning obligations in Attachment R in order to provide the Network Customer with Network Integration Transmission Service over the Transmission Provider's Transmission System. Transmission Provider, on behalf of its Native Load Customers, shall be required to designate resources and loads in the same manner as any Network Customer under Part III of this Tariff. This information must be consistent with the information used by the Transmission Provider to calculate available transfer capability. The Transmission Provider shall include the Network Customer's Network Load in its Transmission System planning and shall, consistent with Good Utility Practice and Attachment R, endeavor to construct and place into service sufficient transfer capability to deliver the Network Customer's Network Resources to serve its Network Load on a basis comparable to the Transmission Provider's delivery of its own generating and purchased resources to its Native Load Customers.
- 28.3 Network Integration Transmission Service: The Transmission Provider will provide firm transmission service over its Transmission System to the Network Customer for the delivery of capacity and energy from its designated Network Resources to service its Network Loads on a basis that is comparable to the Transmission Provider's use of the Transmission System to reliably serve its Native Load Customers.
- 28.4 Secondary Service: The Network Customer may use the Transmission Provider's Transmission System to deliver energy to its Network Loads from resources that have not been designated as Network Resources. Such energy shall be transmitted, on an as-available basis, at no additional charge. Secondary service shall not require the filing of an Application for Network Integration Transmission Service under the Tariff. However, all other requirements of Part III of the Tariff (except for transmission rates) shall apply to secondary service. Deliveries from resources other than Network Resources will have a higher priority than any Non-Firm Point-To-Point Transmission Service under Part II of the Tariff.
- **28.5** Real Power Losses: Real Power Losses are associated with all transmission service. The Transmission Provider is not obligated to provide Real Power

Xcel Energy Operating Companies FERC FPA Electric Tariff Third Revised Volume No. 1 Part III, Section 28
Nature of Network Integration Transmission Service
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Losses. The Network Customer is responsible for replacing losses associated with all transmission service as calculated by the Transmission Provider. The applicable Real Power Losses are as follows:

For Service on the NSP Transmission System: 2.4%

For Service on the PSCo System:

Transmission System: Demand 2.20% 1.70%
Distribution System – Primary Voltage: 3.75% 2.07%

For Service on the SPS System:

Transmission System: Distribution System – Primary Voltage: Demand 2.738606% 3.203203% 8.846390% 6.327826%

The loss factors for Direct Assignment Facilities shall be determined on a case by case basis.

Restrictions on Use of Service: The Network Customer shall not use Network Integration Transmission Service for (i) sales of capacity and energy to non-designated loads, or (ii) direct or indirect provision of transmission service by the Network Customer to third parties. All Network Customers taking Network Integration Transmission Service shall use Point-To-Point Transmission Service under Part II of the Tariff for any Third-Party Sale which requires use of the Transmission Provider's Transmission System. The Transmission Provider shall specify any appropriate charges and penalties and all related terms and conditions applicable in the event that a Network Customer uses Network Integration Transmission Service or secondary service pursuant to Section 28.4 to facilitate a wholesale sale that does not serve a Network Load.

UNITED STATES OF AMERICA BEFORE THE FEDERAL ENERGY REGULATORY COMMISSION

Southwestern Public Service Company)	Docket No. ER19	000
)		

DIRECT TESTIMONY OF WESLEY L. BERGER

ON BEHALF OF SOUTHWESTERN PUBLIC SERVICE COMPANY

JANUARY 30, 2019

DIRECT TESTIMONY OF WESLEY L. BERGER

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EXHIBITS TO DIRECT TESTIMONY OF WESLEY L. BERGER

Exhibit No.	<u>Description</u>
SPS-0002	Calculation of Proposed Loss Factors
SPS-0003	Estimated Annual Cost Impact to Wholesale Customers

UNITED STATES OF AMERICA BEFORE THE FEDERAL ENERGY REGULATORY COMMISSION

Southwestern Public Service Company)	Docket No. ER19	000
)		

Summary of the Direct Testimony of Wesley L. Berger

Mr. Berger provides testimony in support of the filing by Southwestern Public Service Company ("SPS") to revise SPS's loss factors set forth in the Xcel Energy Open Access Transmission Tariff ("Xcel Energy Tariff"), the Southwest Power Pool, Inc. Open Access Transmission Tariff ("SPP Tariff"), and certain wholesale production requirements contracts. Mr. Berger provides an overview of SPS; introduces SPS's other witness in this proceeding (Mr. Duane J. Ripperger); and explains and supports the changes to Sections 15.7 and 28.5 of the Xcel Energy Tariff proposed to be effective April 1, 2019. Mr. Berger also calculates the estimated cost impact of the revised loss factors on wholesale transmission service customers in the SPS rate zone (Zone 11) under the SPP Tariff and on customers currently receiving wholesale production service from SPS. Mr. Berger estimates that the overall impact to SPS wholesale customers of the proposed changes to the loss factors is a cost decrease of \$230,728 annually.

DIRECT TESTIMONY OF

WESLEY L. BERGER

I. INTRODUCTION AND EXPERIENCE

1	Q.	PLEASE STATE YOUR NAME AND BUSINESS ADDRESS.

- 2 A. My name is Wesley L. Berger. My business address is 790 S. Buchanan St., Amarillo,
- 3 TX 79101.

4 Q. BY WHOM ARE YOU EMPLOYED AND WHAT IS YOUR POSITION?

- 5 A. I am employed by Southwestern Public Service Company ("SPS"), a New Mexico
- 6 corporation and wholly owned subsidiary of Xcel Energy Inc. ("Xcel Energy"), as
- 7 Manager, Rate Cases.

8 Q. PLEASE DESCRIBE XCEL ENERGY.

- 9 A. Xcel Energy is a public utility holding company with, among other subsidiaries, four
- wholly owned, vertically integrated public utility operating company subsidiaries: SPS,
- Northern States Power Company, a Minnesota corporation ("NSPM"), Northern States
- Power Company, a Wisconsin corporation ("NSPW"), and Public Service Company of
- 13 Colorado ("PSCo") (together, the "Xcel Energy Operating Companies").

14 Q. ON WHOSE BEHALF ARE YOU TESTIFYING?

15 A. I am testifying on behalf of SPS.

16 Q. PLEASE DESCRIBE YOUR EDUCATIONAL BACKGROUND.

- 17 A. I graduated from New Mexico State University in 1993, receiving a Bachelor of Science
- degree in Mathematics and a Bachelor of Arts degree in Economics. I received a Master

of Arts degree in Economics with specialization in public utility regulation from New
Mexico State University in 1995.

3 Q. WHAT IS YOUR PROFESSIONAL EXPERIENCE?

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4 From June 1995 through April 1997, I worked as a Regulatory Compliance Coordinator A. 5 for SPS providing rate design and general regulatory compliance support. After SPS and 6 Public Service Company of Colorado merged to form New Century Energies in May 7 1997, I worked as a Pricing Analyst and later as a Pricing Specialist through July 2000. I 8 provided cost of service and rate design support for the retail and wholesale jurisdictions 9 of SPS. After the merger creating Xcel Energy in August 2000, I became a Contract 10 Administration Manager in the Wholesale Origination department, where I attended 11 wholesale market development meetings and regional tariff meetings, and I supported the 12 negotiation of wholesale power purchase and sale agreements. In August 2004, I became 13 an Originator, which meant that my duties focused more on negotiating purchase and sale 14 agreements. In 2005, I returned to Regulatory Administration to direct a retail rate case 15 filing in Texas. In May 2006, I assumed my current position as Manager, Rate Cases.

Q. HAVE YOU ATTENDED OR TAKEN ANY SPECIAL COURSES OR SEMINARS RELATING TO PUBLIC UTILITIES?

A. Yes. In addition to my public utility regulation courses at New Mexico State University,

I have completed the advanced rate design course presented by the Edison Electric

Institute. I have also attended multiple seminars, including a Regulatory & Accounting

seminar presented by PricewaterhouseCoopers, a Utility Finance & Accounting seminar

presented by Financial Accounting Institute, and the Public Utility Conference sponsored

by New Mexico State University.

1	Q.	WHAT ARE YOUR DUTIES IN YOUR CURRENT POSITION?
2	A.	I oversee rate filings with the Federal Energy Regulatory Commission ("FERC" or
3		"Commission") that impact SPS. I also provide input on SPS's cost allocation and cost
4		of service issues for its retail jurisdictions in Texas and New Mexico. In addition, I
5		provide regulatory policy input on various issues impacting SPS.
6	Q.	HAVE YOU PREVIOUSLY SUBMITTED TESTIMONY BEFORE THE
7		FEDERAL ENERGY REGULATORY COMMISSION OR ANY OTHER
8		REGULATORY COMMISSION?
9	A.	Yes. I have filed written testimony with the Commission. Specifically, I have filed
10		testimony in Docket Nos. ER00-536, ER12-1682, ER16-1030, and ER19-675. I have
11		also testified before the Public Utility Commission of Texas ("PUCT") and the New
12		Mexico Public Regulation Commission ("NMPRC").
		II. PURPOSE OF TESTIMONY
13	Q.	WHAT IS THE PURPOSE OF YOUR TESTIMONY IN THIS PROCEEDING?
14	A.	The purpose of my testimony is to support SPS's proposal to update the real power
15		transmission and distribution line loss factors stated in Sections 15.7 and 28.5 of the Xcel
16		Energy Tariff applicable to SPS wholesale customers. In my testimony:

1		• I provide an overview of SPS;	
2 3		• I provide an overview of the fil Duane J. Ripperger;	ing and introduce SPS's other witness, Mr.
4 5 6 7		were derived from the 2016 Tra	emand and energy loss factors proposed by SPS ansmission and Distribution System Loss oss Study") discussed and supported by Mr. ibit No. SPS-0005;
8 9 10			energy loss factors stated in the Xcel Energy ills to network transmission service and es; and
11 12			pact of the proposed changes to the current loss assistsion and production customers.
13	Q.	ARE YOU SPONSORING ANY EXHIB	BITS?
14	A.	Yes. I am sponsoring the following exhibit	it, which is attached to my testimony:
		Exhibit No.	Description
		SPS-0002	Calculation of Proposed Loss Factors
		SPS-0003	Estimated Annual Cost Impact to Wholesale Customers
15		Submitted with this filing are the clean and	d marked tariff pages to Sections 15 and 28 of
16		the Xcel Energy Tariff. I am sponsoring th	he proposed tariff revisions.
17	Q.	WERE YOUR TESTIMONY AND EXE	HIBITS PREPARED BY YOU OR UNDER
18		YOUR DIRECT SUPERVISION?	
19	A.	Yes.	

III. OVERVIEW OF SPS'S FILING

A. Overview of SPS

Q. PLEASE DESCRIBE SPS.

A.

Headquartered in Amarillo, Texas, SPS is a vertically integrated generation, transmission, and distribution electric utility that serves approximately 390,000 retail and wholesale customers in a 52,000 square-mile area of the Panhandle and the South Plains of Texas, and eastern and southern New Mexico. SPS's service area extends approximately 400 miles from north to south and 200 miles from east to west. SPS also owns certain transmission facilities in Kansas and Oklahoma. SPS provides regulated, cost-based retail services subject to the jurisdiction of the PUCT and the NMPRC. SPS also provides cost-based requirements wholesale service to cooperative and municipal power customers, with rates determined under production formula rate templates that are part of the individual wholesale power sales agreements.

SPS is a member of the SPP regional transmission organization ("RTO") and is synchronously connected to the Eastern Interconnection grid. With limited exceptions, all transmission services on the SPS system are provided under the SPP Tariff. SPS is also connected to the Western Interconnection grid through three high-voltage direct-current back-to-back converters. Although SPS operates adjacent to the Electric Reliability Council of Texas ("ERCOT") grid, it has no direct interconnections with ERCOT transmission owners.

Q. PLEASE DESCRIBE SPS'S SERVICE AREA.

A. The Texas retail jurisdiction is SPS's single largest regulatory jurisdiction. SPS also serves retail customers in a large portion of eastern and southeastern New Mexico. SPS's

service territory in both Texas and New Mexico is primarily agricultural, with large areas of oil and natural gas production. Additionally, wholesale power sales and transmission services have historically been a significant business segment for SPS. SPS directly serves six wholesale requirements power sales (production) customers, who in turn may serve member customers, and provides wholesale Network Integration Transmission Service ("NITS") to various customers with loads on the SPS transmission system. The SPS transmission system is included in Zone 11 of the SPP Tariff. In total, wholesale production services currently account for approximately 22 percent of SPS's total production demand, and wholesale transmission services currently account for approximately 36 percent of SPS's total transmission network demand.

B. SPS's Filing and the Associated Testimony

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- 11 Q. PLEASE SUMMARIZE THE CHANGES TO THE XCEL ENERGY TARIFF SPS
 12 PROPOSES IN THIS FILING.
- 13 A. SPS proposes to update its transmission and distribution real power loss factors stated in 14 Sections 15.7 and 28.5 of the Xcel Energy Tariff. Under the Xcel Energy Tariff and the 15 SPP Tariff, customers are responsible for replacing the real power losses associated with 16 transmission service. SPS has conducted a loss study to determine the amount of real 17 power losses on its system and, based on this analysis, has updated the real power loss 18 percentages for its transmission system and its distribution-primary voltage system. 19 Because transmission service over the SPS system is primarily provided under the SPP Tariff, SPP will separately make a filing to update the SPS loss factors in Attachment M, 20 21 Appendix 1 of the SPP Tariff, to conform to the updated SPS loss factors in the Xcel

Energy Tariff, to be effective on the same effective date approved by the Commission in this proceeding.

Q. WHY IS SPS SEEKING TO UPDATE ITS TRANSMISSION AND

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DISTRIBUTION PRIMARY REAL POWER LOSS FACTORS?

A. The current transmission and distribution primary real power loss factors do not accurately reflect the most recent study of the transmission and distribution losses SPS experiences in providing service to its customers, including wholesale customers. SPS's current transmission and distribution loss factors stated in the Xcel Energy Tariff were accepted in Docket No. ER16-1030-000, using a loss study that included data from July 2012 through June 2013 (the "2013 Loss Study"). In 2017, SPS completed an updated loss study based on data from January 2016 through December 2016 (the "2016 Loss Study") and calculated new loss factors. The new loss factors were then filed with the PUCT and the NMPRC. The updated loss factors were accepted by the NMPRC in its final order in NMPRC Case No. 17-00255-UT, issued on September 5, 2018, and accepted by the PUCT in its final order in PUCT Docket No. 47527, issued on December 10, 2018. SPS proposes to use the 2016 Loss Study as the basis for the updated real power loss factors stated in the Xcel Energy Tariff applicable to SPS to ensure comparability and consistency among all three jurisdictions (New Mexico, Texas, and FERC).

Q. WHY DOES SPS NEED TO FILE DISTRIBUTION LOSS FACTORS WITH THE COMMISSION?

A. SPS has transmission and wholesale production service customers who have delivery points at primary distribution voltage. These real power demand and energy loss factors

- need to be updated so that they are consistent with the primary distribution loss factors

 applied to SPS's retail customers.
- 3 Q. HOW DO THE PROPOSED LOSS FACTORS COMPARE TO THE CURRENT

4 LINE LOSS FACTORS?

The proposed transmission loss factor for demand is slightly lower than the current transmission demand loss factor, while the proposed transmission loss factor for energy is slightly higher than the current transmission energy loss factor. SPS's proposed primary distribution loss factors are higher than the current distribution loss factors. A comparison of the current and proposed loss factors is shown in Table 1:

10 **Table 1**

	Demand Loss Factors		Energy Loss Factor	
	Current	<u>Proposed</u>	<u>Current</u>	Proposed
Transmission	3.107161%	2.738606%	2.881556%	3.203203%
Distribution -	8.157751%	8.846390%	6.035731%	6.327826%
Primary Voltage				

11 Q. WHAT IS THE PROPOSED EFFECTIVE DATE FOR THE REVISED LOSS

12 **FACTORS?**

- 13 A. SPS is requesting an effective date of April 1, 2019 for the revisions to Sections 15.7 and 28.5 of the Xcel Energy Tariff to reflect new demand and energy loss factors.
- 15 Q. PLEASE INTRODUCE THE OTHER WITNESS PROVIDING TESTIMONY IN
 16 SUPPORT OF SPS'S PROPOSED LOSS FACTORS.
- 17 A. SPS's filing is also supported by the Direct Testimony of Mr. Duane J. Ripperger,
- Manager, Regional Transmission Initiatives for XES, Exhibit Nos. SPS-0004 and SPS-
- 19 0005 (the "Ripperger Testimony").

1	Q.	WHAT DOES MR. RIPPERGER ADDRESS IN HIS TESTIMONY?
2	A.	Mr. Ripperger discusses how a system loss study is performed, and the methodology used
3		by SPS for the 2016 Loss Study. Mr. Ripperger also discusses certain refinements to the
4		2016 Loss Study as compared to the 2013 Loss Study.
5	Q.	HAVE YOU QUANTIFIED THE IMPACT OF THE CHANGE PROPOSED IN
6		THE REVISED TEMPLATE ON SPS'S WHOLESALE DISTRIBUTION
7		SERVICE CUSTOMERS?
8	A.	Yes. In Exhibit No. SPS-0003, I present the annual customer impact of the new loss
9		factors. In Section V of my testimony, I discuss my calculations of the annual customer
10		impact presented in Exhibit No. SPS-0003.
		IV. CALCULATION OF PROPOSED LOSS FACTORS
11	Q.	WHAT IS THE BASIS FOR THE REAL POWER LOSS FACTORS SPS
12		PROPOSES IN THIS PROCEEDING?
13	A.	SPS is using the 2016 Loss Study, its most recent system loss study, as presented by Mr.
14		Ripperger. As I mentioned, the loss factors resulting from this study have been accepted
15		by the PUCT and the NMPRC.
16	Q.	WHAT MODIFICATIONS DID YOU MAKE TO THE 2016 LOSS STUDY
17		RESULTS TO DERIVE THE PROPOSED WHOLESALE LOSS FACTORS?
18	A.	The primary distribution loss factors proposed by SPS come directly from Appendices O
19		and P to the 2016 Loss Study (attached as Exhibit No. SPS-0005 to Mr. Ripperger's
20		testimony).
21		I also used the loss factors from the 2016 Loss Study as the basis for SPS's
22		proposed transmission loss factors, but modified the loss factors to tailor them to

1 wholesale service. Specifically, I began with the Energy and Demand loss factors shown 2 in Appendices O and P to the 2016 Loss Study, and made one modification: I combined 3 the two transmission level loss factors described in the 2016 Loss Study into the 4 composite transmission loss factor for the Xcel Energy Tariff and the SPP Tariff. 5 Q. PLEASE DESCRIBE YOUR MODIFICATION IN ORDER TO CREATE A 6 COMPOSITE CALCULATION. 7 A. Both the Xcel Energy Tariff and the SPP Tariff employ a single loss factor for all 8 transmission voltage facilities. The 2016 Loss Study, however, contains two 9 transmission loss factors. Specifically, the 2016 Loss Study calculates a loss factor for 10 transmission facilities with a voltage of 115 kV or higher and a separate loss factor for 11 transmission facilities at a voltage level of 69 kV. Therefore, it was necessary for me to 12 calculate a composite transmission loss factor applicable to all transmission voltages to 13 be set out in the Xcel Energy Tariff and SPP Tariff. The current SPS transmission loss 14 factors accepted in Docket No. ER16-1030-000 were also calculated as composite factors. 15 16 The modification I made to the Appendix O and P loss factor calculations was to 17

sum the losses for the two transmission service levels (levels 2 and 3) into a single total transmission losses number. The total is shown on line 21 in the kW Loss by Level column (column E) on page 1 and on line 21 in the kWh Loss by Level column (column E) on page 2 of Exhibit No. SPS-0002. The remaining mathematical calculations on line 21 on both pages are identical to the original loss factor calculations done by Mr. Ripperger and accepted by the PUCT and NMPRC.

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1	Q.	IS IT NECESSARY TO MAKE A MODIFICATION TO THE 2016 LOSS STUDY
2		TO REMOVE GENERATOR STEP-UP TRANSFORMER LOSSES?
3	A.	No. As discussed in the 2016 Loss Study, SPS metered its generators at the high side of
4		the generator step-up transformers during the time period of the 2016 Loss Study.
5	Q.	WHAT ARE SPS' PROPOSED LOSS FACTORS AFTER THESE
6		CALCULATIONS?
7	A.	SPS proposes a transmission demand loss factor of 2.738606%, as shown on page 1, line
8		21 (column C) of Exhibit No. SPS-0002, and a transmission energy loss factor of
9		3.203203%, as shown on page 2, line 21 (column C) of Exhibit No. SPS-0002. SPS
10		proposes a distribution demand loss factor of 8.846390%, as shown on page 1, line 25
11		(column C) of Exhibit No. SPS-0002, and a distribution energy loss factor of 6.327826%,
12		as shown on page 2, line 25 (column C) of Exhibit No. SPS-0002. Table 1, on page 8
13		above, compares the currently effective wholesale transmission and distribution loss
14		factors with the proposed factors.
15 16		V. APPLICATION OF REAL POWER LOSS FACTORS TO CALCULATE RATES APPLICABLE TO WHOLESALE SERVICES
17	Q.	WHAT CUSTOMERS ARE AFFECTED BY SPS'S PROPOSED CHANGE TO
18		ITS LOSS FACTORS?
19	A.	The network transmission service customers that purchase transmission service under the
20		SPP Tariff for loads on the SPS system (SPP Zone 11), and production service customers
21		who purchase power from SPS under wholesale requirements power sale agreements, are
22		both affected by SPS's proposal to update its real power loss values. The demand loss
23		change will affect the calculation of billing demands for both network and production
24		customers, and the energy loss change will affect charges to production customers.

Q. HOW DOES SPS APPLY THE LOSS FACTORS TO DETERMINE THE

A.

CHARGES APPLICABLE TO NETWORK TRANSMISSION CUSTOMERS?

The loss factors developed by Mr. Ripperger in the 2016 Loss Study are what are termed injection loss factors. However, these loss factors are typically applied to metered usage values of network transmission customers in calculating monthly network demands.

Therefore, it is necessary to use what are termed delivery loss factors. Mr. Ripperger explains how the delivery loss factors in the 2016 Loss Study are calculated.

As shown on page 1, line 21 (column B) of Exhibit No. SPS-0002, the transmission demand delivery loss factor to be applied to metered usage is 1.028157. The metered usage is multiplied by the delivery loss factor to determine the monthly network demand. For example, if a customer has a metered demand of 600,000 kW, the monthly network demand for billing purposes is 600,000 *1.028157 = 616,894 kW. Similar delivery loss factors are shown in Exhibit No. SPS-0002 for the transmission energy, distribution demand, and distribution energy loss factors.

Alternatively, a delivery loss factor can be expressed as a percentage as is done in Attachment M, Appendix 1 to the SPP Tariff. This is calculated by the following equation: delivery loss factor = [(1/(1 - injection loss factor)) - 1] * 100. Using the transmission demand injection loss factor in Exhibit No. SPS-0002 on page 1, line 21 (column C) of 2.738606%, we can calculate the delivery loss factor SPP will show in Attachment M as [(1/(1-.02738606)) - 1] * 100 = 2.815717%. The metered usage is added to the product of the metered usage and the delivery loss factor expressed as a percentage to determine monthly network demand. For example, if a customer has a

1		metered demand of 600,000 kW, the monthly network demand for billing purposes is
2		600,000 + (600,000 * 2.815717%) = 616,894 kW.
3		Note that although the arithmetic calculations are performed differently, both
4		methodologies result in the same billing demand.
5	Q.	HOW DOES SPS APPLY THE LOSS FACTORS TO DETERMINE THE
6		CHANGES APPLICABLE TO WHOLESALE PRODUCTION REQUIREMENTS
7		SERVICE CUSTOMERS?
8	A.	SPS applies the delivery loss factors calculated using the first method described above to
9		the wholesale customers' metered monthly usage. For example, if a wholesale customer
10		has a monthly demand of 100,000 kW and monthly energy usage of 50,000,000 kWh,
11		SPS would calculate the monthly billing determinants using the delivery loss factors
12		shown in line 21, Column B of pages 1 and 2 of SPS Exhibit 2. Specifically, billing
13		demand equals 100,000 * 1.028157 = 102,816 kW and billing energy equals 50,000,000
14		* 1.033092 = 51,654,600 kWh.
15	Q.	WILL THE PROPOSED LOSS FACTOR CHANGES AFFECT ENERGY
16		LOSSES BILLED TO NETWORK CUSTOMERS UNDER THE SPP TARIFF?
17	A.	No. Under Attachment M to the SPP OATT, energy losses are determined by the SPP
18		regional system dispatch and included in the locational marginal prices charged in the
19		SPP Integrated Marketplace to market participants, including network transmission
20		customers on the SPS system. The SPS Tariff loss factors do not affect these
21		calculations.

1	Ų.	IS IT NECESSARY TO UPDATE ANY SPS WHOLESALE PRODUCTION
2		SERVICE AGREEMENTS TO REFLECT THE REVISED LOSS FACTORS?
3	A.	No. The SPS production service agreements refer to the loss values as stated in the
4		applicable Tariff. As such, while the revised loss values will affect the calculation of
5		bills for SPS's production customers, Commission acceptance of the revised real power
6		loss factors will not require revisions to the underlying agreements.
		VI. COST IMPACT OF THE PROPOSED LOSS FACTORS
7	Q.	HAVE YOU ESTIMATED THE COST IMPACT TO WHOLESALE
8		CUSTOMERS OF THE PROPOSED TARIFF CHANGES?
9	A.	Yes. I estimated the cost impact to individual network transmission service customers
10		and wholesale requirements customers on the SPS system by recalculating SPS bills to
11		wholesale customers for calendar year 2018 using the proposed loss factors in place of
12		the currently effective loss factors.
13	Q.	WHAT IS THE ESTIMATED COST IMPACT OF THE PROPOSED TARIFF
14		CHANGES TO SPS'S NETWORK TRANSMISSION SERVICE AND
15		WHOLESALE REQUIREMENTS CUSTOMERS?
16	A.	The overall cost impact to these customers of the changes to the current loss factors is
17		estimated to be a decrease of \$230,728 annually or approximately -0.072%. Exhibit No
18		SPS-0003 shows the estimated transmission bill impact, production bill impact and net
19		impact for each wholesale customer. As noted, this estimate reflects billing data for the
20		twelve months from January 2018 through December 2018 and compares the amounts
21		billed using the current loss factors to the amounts that would have been billed had the
22		proposed loss factors been in effect.

1 Exhibit No. SPS-0003 shows that charges to network transmission service 2 customers would be reduced as a result of the lower demand loss factor by approximately 3 \$419,000 per year, while charges to wholesale production customers would increase by 4 approximately \$188,000 per year. With one exception, all of SPS's wholesale customers 5 are expected to see a slight net reduction. Central Valley Electric Cooperative is 6 estimated to see a slight increase (\$6,833) because Central Valley Electric Cooperative 7 has a relatively high load factor and the energy loss factor is increasing. 8 Q. HAS SPS CALCULATED THE COST IMPACT TO POINT-TO-POINT 9 TRANSMISSION SERVICE CUSTOMERS? 10 A. No. Point-to-point service is provided only by SPP under the SPP Tariff. SPS does not 11 have the information necessary to calculate the impact of the slight reduction of the 12 transmission demand loss factor on SPP point-to-point transmission service customers. 13 Further, similar to network transmission customers, point-to-point customers' energy 14 charges will not be impacted by this change to the SPS transmission energy loss factor 15 because energy losses are determined by the SPP regional system dispatch and included 16 in the locational marginal prices charged in the SPP Integrated Marketplace. 17 Q. DID SPS SHARE THE PROPOSED LOSS FACTOR CHANGES AND THE 18 ESTIMATED COST IMPACT WITH ITS WHOLESALE CUSTOMERS PRIOR 19 TO SUBMITTING THIS FILING? 20 A. Yes. SPS provided the proposed loss factors and the estimated cost impact analysis to 21 each of its wholesale customers on January 18, 2019, and offered to hold pre-filing 22 conference calls with each of the customers to explain the calculations and why SPS was

making this filing. SPS answered a few questions, but none of the customers requested a pre-filing meeting.

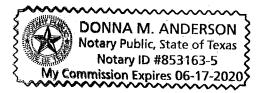
VII. CONCLUSION

- 3 Q. PLEASE SUMMARIZE YOUR RECOMMENDATIONS.
- 4 A. I recommend that the Commission approve SPS's proposed revisions to Sections 15.7
- and 28.5 of the Xcel Energy Tariff to incorporate the new SPS loss factors discussed in
- 6 my testimony, effective on April 1, 2019. The Tariff changes are just and reasonable
- because they incorporate information from SPS's most recent system loss study, and that
- 8 same loss study has recently been approved by the NMPRC and PUCT for retail
- 9 ratemaking purposes.
- 10 Q. DOES THIS CONCLUDE YOUR PRE-FILED DIRECT TESTIMONY?
- 11 A. Yes.

UNITED STATES OF AMERICA BEFORE THE FEDERAL ENERGY REGULATORY COMMISSION

Southwestern Public Service Company)	Docket No. ER19		
AFF	IDAVIT			

Wesley L. Berger, being duly sworn, deposes and states: that the Direct Testimony of Wesley L. Berger was prepared by me or under my direct supervision, and that the statements contained therein are true and correct to the best of my knowledge and belief.



Subscribed and sworn before me this 29 day of January 2019.

Notary Public
My commission expires: [date] 6/17/2020

Line No. 1 2

3

SOUTHWESTERN PUBLIC SERVICE COMPANY DEMAND LOSS FACTOR CALCULATION 12 MONTHS ENDING DECEMBER 2016

Loss Factor Calculation

3	Loss Factor Calculation					<u></u>		
4			Total Ger	neration Inputs =	6,003,000 Kv	N		
5			S	ystem Peak Hr.	6,003,000 Kv	N		
6		(A)	(B)	(C)	(D)	(E)	(F)	(G)
7		` ,	Loss factor to	` '	` ,	` ,	` '	` ,
8		Loss Factor to	gross up 1 level	%	KW Flow	KW Loss	KW Demand	Loss Check
9		Gross up to Gen	1/(1-loss %)	loss by level	into each level	by Level	by loss level	Loss fac X sales
10		·	, , , , ,					
11								
12	Sales at the Generator	1.000000	1.000000	0.000000%	6,003,000	0	0	0
13	@ Generation						<u> </u>	
14								
15	Sales @ 115, 230 & 345 KV	1.023667	1.023667	2.311973%	6,003,000	138,788	2,244,415	2,297,533
16	Level 2							
17							<u> </u>	
18	Sales @ 69 KV	1.030961	1.007126	0.707520%	3,619,798	25,611	1,090,485	1,124,247
19	Level 3							
20								
21	Transmission Losses	1.028157	1.028157	2.738606%	6,003,000	164,399	3,334,899	
22	Levels 2 and 3 combined							
23								
24								
25	Sales @ Primary (33kv - 2.4kv)	1.131015	1.097049	8.846390%	2,503,702	221,487	436,754	493,975
26	Level 4							
27								
28	Secondary Sales @ the Transf.	1.161769	1.027192	2.647180%	1,845,461	48,853	640,746	744,399
29	Level 5							
30	0.1	4.400500	4 00 44 00	0.4000050/	4.455.000	4.700	4 44 4 70 4	4 000 000
31	Sales served by secondary lines	1.166539	1.004106	0.408905%	1,155,862	4,726	1,114,734	1,300,380
32	Level 6							
33								
34	Total		1.078990	7.320754%	5,966,598 =	439,465	5,527,133	5,960,535
35	Composite Footon Lovele 5 and 2	4.404000	4.000004	0.00000000	4.045.404	50.570	4 755 400	
36	Composite Factor Levels 5 and 6	1.164833	1.029901	2.903288%	1,845,461	53,579	1,755,480	

-4,233

Check using rounded factors

7,366,895,848

140,137,228

Line No. 1 2

3

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37 38 39

40 41 Composite Factors 5 & 6 to Gen.

SOUTHWESTERN PUBLIC SERVICE COMPANY ENERGY LOSS FACTOR CALCULATION 12 MONTHS ENDING DECEMBER 2016

31,758,276,076 kWh

7,507,033,076

Total Generation Inputs =

Loss Factor Calculation

(A) (B) (C) (D) (E) (F) (G) Loss factor to Loss Factor to gross up 1 level % **KWH Flow KWH Loss KWH Sales Loss Check** Gross up to Gen 1/(1-loss %) into each level by Level by loss level Loss fac X sales loss by level Sales at the Generator 1.000000 1.000000 0.000000% 0 8,295,082 8,295,082 31,758,276,076 @ Generation Sales @ 115, 230 & 345 KV 1.029633 1.029633 2.877997% 31,749,980,994 913,763,470 13,821,244,766 14,230,809,712 Level 2 Sales @ 69 KV 1.035919 1.006105 0.606835% 17,014,972,758 103,252,764 4,942,501,116 5,120,030,814 Level 3 18,763,745,882 1.033092 1.033092 1,017,016,234 **Transmission Losses** 3.203203% 31,749,980,994 Levels 2 and 3 combined Sales @ Primary (33kv - 2.4kv) 1.105898 1.067553 6.327826% 11,969,218,878 757,391,388 3,704,794,414 4,097,124,733 Level 4 Secondary Sales @ the Transf. 1.125047 1.017315 1.702074% 7,507,033,076 127,775,281 3,205,486,688 3,606,323,182 Level 5 Sales served by secondary lines 1.128389 1.002971 0.296182% 4,173,771,108 12,361,948 4,161,409,160 4,695,688,321 Level 6 1,914,544,850 + 29.843.731.226 Total 1.064152 6.028491% 31,758,276,076 = 31,758,271,843

1.866746%

Loss factor calculation for gross up to a target level equals the product of loss factors for each level up through the target level.

1.019023

1.126935

\$ 112,792,734

112,373,708

(419,027)

(419,027)

(230,728)

-0.072%

<u>Line</u> <u>No.</u>		<u>Ce</u>	ntral Valley	<u>Farmers</u>]	Lea County	Roosevelt	WTMPA	lden Spread <u>Fri-County)</u>	<u>Go</u>	lden Spread*	<u>Total</u>
1	Production Demand											
2	Current	\$	7,411,636	\$ 3,870,853	\$	13,216,957	\$ 1,516,124	\$ 49,016,199	\$ 5,483,249	\$	-	\$ 80,515,020
3	Proposed		7,370,042	3,852,157		13,150,440	1,507,465	48,859,356	5,462,471		-	80,201,932
4	Change	\$	(41,594)	\$ (18,697)	\$	(66,517)	\$ (8,660)	\$ (156,843)	\$ (20,778)	\$	-	\$ (313,088)
5												
6	Production - Energy & Fuel											
7	Current	\$	15,289,781	\$ 4,635,246	\$	21,730,993	\$ 2,245,149	\$ 74,689,469	\$ 9,880,499	\$	-	\$ 128,471,138
8	Proposed		15,365,731	4,664,705		21,837,680	2,259,011	74,932,072	9,913,327		-	128,972,525
9	Change	\$	75,950	\$ 29,459	\$	106,687	\$ 13,862	\$ 242,603	\$ 32,827	\$	- '	\$ 501,387
10												
11	Total Production	\$	34,356	\$ 10,762	\$	40,169	\$ 5,202	\$ 85,760	\$ 12,049	\$	-	\$ 188,299
12												
13	Transmission											

1,541,995 \$

(5,843) \$

(5,843) \$

(641) \$

1,536,152

32,393,247 \$

(117,010) \$

(117,010) \$

(31,250) \$

32,276,237

3,652,788 \$

(13,842) \$

(13,842) \$

(1,793) \$

3,638,946

52,124,076

51,929,209

(194,868)

(194,868)

Total % Change

(194,868) \$

\$

\$

Cost Impact Estimate Summary (Using Calendar Year 2018 data)

* Column represents Golden Spread loads where no wholesale power requirements are supplied by SPS. These loads incur only network transmission service and local distribution facilities charges.

12,045,284 \$

(45,645) \$

(45,645) \$

(5,476) \$

11,999,638

7,263,150 \$

(27,524) \$

(27,524) \$

6,833 \$

7,235,627

Current \$

Change \$

Proposed

Total Change \$

Total Transmission \$

3,772,194 \$

(14,295) \$

(14,295) \$

(3,533) \$

3,757,899

14

15

16

17

18

19 20

UNITED STATES OF AMERICA BEFORE THE FEDERAL ENERGY REGULATORY COMMISSION

Southwestern Public Service Company)	Docket No. ER19	000
)		

DIRECT TESTIMONY OF DUANE J. RIPPERGER

ON BEHALF OF SOUTHWESTERN PUBLIC SERVICE COMPANY

JANUARY 30, 2019

DIRECT TESTIMONY OF DUANE J. RIPPERGER

TABLE OF CONTENTS

I.	INTRODUCTION AND EXPERIENCE	
II.	PURPOSE OF TESTIMONY	3
III.	SPS'S 2016 LOSS STUDY	3
IV.	CALCULATION OF LOSS FACTORS	18
V.	CONCLUSION	18

EXHIBITS TO DIRECT TESTIMONY OF DUANE J. RIPPERGER

Exhibit No.	<u>Description</u>
SPS-0005	SPS's 2016 Transmission and Distribution System Loss
	Evaluation Study

UNITED STATES OF AMERICA BEFORE THE FEDERAL ENERGY REGULATORY COMMISSION

	Southwestern Public Service Company)	Docket No. ER19000
1	Summary of the Direct	t Testimony	of Duane J. Ripperger
2	Mr. Ripperger discusses SPS's 2016 To	ransmission a	and Distribution System Loss
3	Evaluation Study (the "2016 Loss Stud	ly") conducte	ed for the period from January 1, 2016
4	through December 31, 2016 ("Study Pe	eriod") and c	ompleted in July 2017. The 2016
5	Loss Study is the basis for the updated	wholesale lo	ss factors proposed by SPS in this
6	proceeding.		

DIRECT TESTIMONY OF

DUANE J. RIPPERGER

1		I. INTRODUCTION AND EXPERIENCE
2	Q.	PLEASE STATE YOUR NAME AND BUSINESS ADDRESS.
3	A.	My name is Duane J. Ripperger. My business address is 790 S. Buchanan Street,
4		Amarillo, Texas 79101.
5	Q.	ON WHOSE BEHALF ARE YOU TESTIFYING IN THIS PROCEEDING?
6	A.	I am filing testimony on behalf of Southwestern Public Service Company, a New Mexico
7		corporation ("SPS") and wholly-owned electric utility subsidiary of Xcel Energy Inc.
8		("Xcel Energy").
9	Q.	BY WHOM ARE YOU EMPLOYED AND IN WHAT POSITION?
10	A.	I am employed by Xcel Energy Services Inc. ("XES") as Manager, Regional
11		Transmission Initiatives.
12	Q.	PLEASE BRIEFLY DESCRIBE YOUR DUTIES AS MANAGER, REGIONAL
13		TRANSMISSION INITIATIVES.
14	A.	I am responsible for supporting the implementation of strategic transmission priorities.
15		These priorities include the planning for large electric transmission projects, support of
16		transmission-related regulatory activities, and the implementation of evolving
17		technologies on the transmission grid.
18	Q.	PLEASE DESCRIBE YOUR EDUCATIONAL BACKGROUND.
19	A.	I earned a bachelor's degree in Electrical Engineering from Iowa State University and a
20		master's degree in Engineering Management from the University of Colorado.

1 Q. PLEASE DESCRIBE YOUR PROFESSIONAL EXPERIENCE.

- 2 A. I have 34 years of experience in the electric utility industry obtained through various
- 3 engineering and management assignments. I have been employed by SPS or XES since
- 4 June 1984. I have held positions in distribution engineering, electrical operations,
- 5 transmission and distribution planning, asset management, and most currently in
- 6 transmission project planning and public policy.

7 Q. DO YOU HOLD A PROFESSIONAL LICENSE?

- 8 A. Yes. I am currently licensed as a Professional Engineer in the states of New Mexico,
- 9 Texas, and Colorado.
- 10 Q. ARE YOU A MEMBER OF ANY PROFESSIONAL ORGANIZATIONS?
- 11 A. Yes. I am a senior member of the Institute of Electrical and Electronics Engineers.
- 12 Q. HAVE YOU TESTIFIED BEFORE ANY REGULATORY AUTHORITIES?
- 13 A. Yes. I filed testimony with the Public Utility Commission of Texas ("PUCT") on behalf
- of SPS regarding: transmission capital additions in Docket No. 46877, SPS's 2017
- proceeding to adjust its Transmission Cost Recovery Factor; and the 2016 System Loss
- Study and the 2017 Radial line study in Docket No. 47527, SPS's 2017 Texas base rate
- 17 case. I have also filed testimony with the New Mexico Public Regulatory Commission
- 18 ("NMPRC") on behalf of SPS regarding the 2016 System Loss Study and the 2017
- 19 Radial line study in Case No. 17-00255-UT, SPS's 2017 New Mexico base rate case.
- Additionally, I filed affidavit testimony with the Federal Energy Regulatory Commission
- 21 ("FERC") regarding a filing by the Southwest Power Pool, Inc. ("SPP") in FERC Docket
- 22 No. ER18-2358-000.

II. PURPOSE OF TESTIMONY

2 Q. WHAT IS THE SCOPE OF YOUR DIRECT TESTIMONY?

A. I will discuss the results of SPS's 2016 Transmission and Distribution System Loss

Evaluation Study (the "2016 Loss Study") conducted for the period from January 1,

2016 through December 31, 2016 ("Study Period") and completed in July 2017. The

2016 Loss Study is the basis for the updated wholesale loss factors proposed by SPS in

this proceeding. Exhibit No. SPS-0005 is a copy of the 2016 Loss Study, which consists

of a narrative explanation of the study results and numerous detailed work papers.

9 Q. WAS YOUR DIRECT TESTIMONY PREPARED BY YOU OR UNDER YOUR 10 DIRECT SUPERVISION?

11 A. Yes.

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III. SPS'S 2016 LOSS STUDY

13 Q. WHAT IS A LOSS STUDY?

A. A loss study is an engineering evaluation of the transmission and distribution ("T&D") losses incurred on an electrical system for a specified period of time. The goal of such a study is to determine where the losses have occurred, that is, on what T&D elements (transmission lines and transformers, distribution lines and transformers, and Generator Step Up transformers) the losses occur and to then properly allocate the losses to each individual type of element of the system. The losses determined in an engineering evaluation should reasonably match losses derived from accounting records comparing energy deliveries and energy supplies into the T&D system. After the losses have been determined, loss factors representing the T&D losses on specific voltage levels of the system are developed for rate making purposes.

Q. WHY DID SPS PREPARE THE 2016 LOSS STUDY?

1

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2 A. The previous SPS loss study had been completed utilizing data from July 1, 2012 through 3 June 30, 2013 ("2013 Loss Study"), and loss factors based on this study were 4 incorporated in the Xcel Energy Open Access Transmission Tariff ("Xcel Energy Tariff") 5 in Docket No. ER16-1030-000 effective May 1, 2016. The SPS system has experienced 6 several significant changes since 2013, including implementation of the SPP Integrated 7 Marketplace, installation of new 345 kV transmission facilities by SPS, and increased 8 wind and solar generation. SPS concluded it would be appropriate to perform a new Loss 9 Study. Additionally, SPS committed to perform a new loss study that would cover a 10 study period ending no later than December 31, 2016 in both NMPRC Case No. 14-11 00348-UT and in the Non-Unanimous Stipulation in PUCT Docket No. 42004. HOW DOES THE 2016 LOSS STUDY COMPARE TO THE 2013 LOSS STUDY? 12 Q. During the Study Period, energy supplies (i.e., "Resources") and energy deliveries 13 A. ("Sales") were lower in absolute terms than in the 2013 Loss Study. As a percentage of 14 15 SPS's total Resources, however, actual losses in the 2016 Loss Study were slightly higher 16 than in the 2013 Loss Study. The losses calculated in the 2016 Loss Study are 1,948,829 17 megawatt hours ("MWh"), which is only 1.79% more than the actual losses of 1,914,545

MWh, i.e., calculated losses equal 101.79% of actual losses.

The sum of energy SPS sold to customers and delivered to interconnections with other utilities at the points the energy left the SPS transmission and distribution system, collectively "Sales." "Sales" thus include deliveries of power produced by suppliers other than SPS to transmission-only customers.

The following Table DJR-1 compares data and results from the 2013 and 2016

2 Loss Studies.

3

Table DJR-1 Comparison of 2013 and 2016 Loss Study Data²

Subject	2013 Loss Study	2016 Loss Study
Total Resources	32,964,320 MWh	31,758,276 MWh
Total Sales	31,142,401 MWh	29,843,731 MWh
Actual Losses	1,821,919 MWh	1,914,545 MWh
Overall Loss Percentage	5.53%	6.03%
Calculated Losses	1,836,997 MWh	1,948,829 MWh
Calculated Losses as % of Actual Losses	100.83%	101.79%
Undeterminable Losses	-15,079 MWh	-34,284 MWh
Peak Load	6,079 MW	6,003 MW

4 Q. DID YOU PARTICIPATE IN THE PREPARATION OF THE 2016 LOSS STUDY?

- 5 A. Yes. I participated in the preparation of the 2016 Loss Study and oversaw its completion.
- 6 Several SPS and XES staff provided the necessary data updates required for the 2016
- 7 Loss Study.

_

Data presented are rounded, which may result in calculations not totaling properly. Loss study spreadsheets frequently display rounded data, but use the unrounded data in the calculations.

Q. HAS SPS SUBMITTED THE 2016 LOSS STUDY TO ITS STATE REGULATORY

AGENCIES?

A.

A. Yes. As discussed in the Direct Testimony of Mr. Wesley L. Berger, SPS submitted the 2016 Loss Study to the PUCT and the NMPRC, and these commissions accepted the loss factors derived from the 2016 Loss Study in orders issued in 2018. SPS proposes to revise the wholesale real power loss percentages set out in the Xcel Energy Tariff to be consistent with the 2016 Loss Study and the loss factors used to calculate retail rates to provide consistency across SPS's three jurisdictions (FERC, Texas and New Mexico).

9 Q. WHAT ARE ELECTRICAL "LINE LOSSES"?

As electrical current flows from a generation source to customers' loads, it passes through wires and transformers that have an inherent electrical resistance to the flow of electricity. This electrical resistance causes some of the energy flowing in the system to be converted to heat and is, thereby, "lost." Total losses are the difference between the electrical energy put onto the T&D system and the electrical energy that was either sold to customers or delivered to exit points on the utility's T&D system. For example, if a utility generates 1,000 MWh and experiences overall losses of 6%, it will deliver only 940 of the 1,000 MWh generated. The 60 MWh difference between the amounts generated and delivered to customers are the T&D losses. Such losses are an inherent characteristic of a properly functioning electrical system and are unavoidable.

Q. IN YOUR EXAMPLE, WOULD EACH TYPE OF CUSTOMER CAUSE THE UTILITY TO LOSE 6% OF THE ENERGY GENERATED?

A. No, not generally, and not on SPS's system. In order for electricity to reach a typical residential customer, it must flow from the generator through generation unit main

transformers, then through bulk transmission lines and related autotransformers, then through transformers at a distribution substation, then through primary distribution lines, then through a pole top transformer, then through a secondary distribution line from the pole top transformer to a pole behind the residence, and finally through a service line from the pole to the meter on the side of the house. At each step, losses are incurred to serve the residential customer.

By contrast, to reach a wholesale or industrial customer taking service at 230 kilovolts ("kV"), the electricity has to flow through only the generation unit main transformer, some bulk transmission lines, and a 345/230 kV autotransformer. None of the losses incurred at distribution substations, primary distribution lines, distribution transformers, secondary lines, and service lines are experienced in serving an industrial customer taking service at transmission voltage. Thus, in general, customers taking service at higher voltages cause fewer losses to be incurred than do customers taking service at lower voltages.

On the SPS system, customers take service at multiple voltages ranging from 230 kV to 120 volts. For example, on the SPS system, a wholesale customer may take service at transmission voltages from 230, 115, or 69 kV. Wholesale customers may also take service at various distribution voltages from 34 to 2.4 kV. A wholesale customer taking service at a transmission voltage should only be required to pay for the losses incurred as the power moves from the generators through the transmission system (or through the distribution system for wholesale loads served at distribution voltage).

1 Q. DO UTILITIES IN GENERAL, AND SPS IN PARTICULAR, HAVE METERS 2 INSTALLED AT EACH STEP IN THE ELECTRICAL FLOW DESCRIBED 3 ABOVE SO THAT LOSSES AT EACH STEP CAN BE MEASURED? 4 A. No. In general and on SPS's system, meters exist at generators, at locations where SPS's 5 transmission lines interconnect with transmission lines of other utilities, and at points of 6 delivery to customers. Thus, SPS can use meters to measure the total electrical energy 7 placed on its T&D system, whether from generators located within or outside its system, 8 and the total energy Sales. The difference between total Resources and total Sales is the 9 actual loss incurred. 10 Given that meters do not exist at each step at which losses are incurred, a loss 11 evaluation study is performed to quantify, through engineering analysis and calculations, 12 the power and energy losses that occurred at the different loss levels on the T&D system 13 during the study period. The calculated loss values for each loss level are used with the 14 undeterminable losses (discussed later) to assign the proper portion of actual losses to 15 Loss Level 2 through Loss Level 6 discussed below. 16 Q. WHAT CIRCUIT ELEMENTS OF SPS'S ELECTRICAL SYSTEM WERE 17 **ANALYZED IN THE 2016 LOSS STUDY?** 18 A. The circuit elements analyzed were: (1) the transmission lines, (2) the transmission 19 autotransformers, (3) the distribution substation transformers, (4) the distribution primary 20 feeder circuits, (5) the distribution line transformers, and (6) the distribution secondary

21

lines and service lines.

1	Q.	YOU STATED THAT THE 2016 LOSS STUDY CALCULATES LOSSES AT
2		SEVERAL LEVELS. PLEASE IDENTIFY THE LOSS LEVELS AND THE
3		CIRCUIT ELEMENTS CONTAINED IN EACH LOSS LEVEL.
4	A.	Loss Level 1 is the generator and generator step-up transformer and no losses are
5		calculated at this level because the Backbone Transmission is considered the delivery
6		point of the electricity from the generator. Loss Levels 2 through 6 and the circuit
7		elements in each loss level are identified below.
8		<u>Loss Level 2 – Backbone Transmission</u>
9		• Bulk transmission lines (345 kV, 230 kV, and 115 kV); and
10		• Autotransformers (345/230 kV and 230/115 kV).
11		<u>Loss Level 3 – Sub-Transmission</u>
12		• 69 kV transmission lines; and
13		• Autotransformers (115/69 kV).
14		<u>Loss Level 4 – Distribution Primary</u>
15		Transformers located at distribution substations; and
16		• Primary Distribution Lines ("feeders") (34.5 kV – 2.4 kV).
17		Loss Level 5 – Distribution Secondary Transformers
18		Transformers located on primary distribution lines.
19		Loss Level 6 – Distribution Secondary and Service Lines
20		Secondary distribution lines running from Level 5 transformers to other poles or
21		service points and service lines running to the customers' premises.
22		The losses at Levels 5 and 6 are combined to create a "Distribution Secondary"
23		classification.

1 Q. YOU NOTED THAT THE 2016 LOSS STUDY COVERED A 12-MONTH 2 PERIOD. IS IT APPROPRIATE TO PERFORM A LOSS EVALUATION STUDY 3 **OVER A PERIOD SHORTER THAN 12 MONTHS?** 4 A. In general, no. The loss evaluation study must correlate energy generated and purchased 5 for customers with Sales to those customers. SPS bills some customers every normal 6 business day of each month. Customers are usually billed once per month; however, the 7 billing period start and end dates do not always respect the calendar month boundary. 8 The billing period may cover part of a previous calendar month or may only cover part of 9 the current month, with no overlap into a previous month. When all Sales are totaled and 10 compared to that billing month's generation and power purchases, there will be a 11 difference, which may be a positive or a negative number. This difference does not 12 necessarily reflect the actual losses incurred on the T&D system during this billing 13 month. This precludes doing a loss evaluation study for a short period of time. 14 Q. HOW DOES A LONGER TIME PERIOD AID IN PREPARING A LOSS STUDY? 15 By using a longer time period, such as one year, the effects of the different customer A. 16 billing cycles are minimized. I would note that the previous 2009 and 2013 loss studies 17 used to update the SPS loss factors included in the Xcel Energy Tariff in 2012 (Docket 18 No. ER12-1682-000) and 2016 (Docket No. ER16-1030-000) also used historic one year 19 study periods.

Q. DID THE 2016 LOSS STUDY CONSIDER LOSSES OF CUSTOMERS

2 OPERATING THEIR OWN TRANSMISSION AND/OR DISTRIBUTION

3 **SYSTEMS?**

1

- 4 A. No. SPS evaluated losses up to the customers' meters but not beyond, because SPS does
- 5 not incur the losses that occur beyond the customers' meters.

6 Q. PLEASE DESCRIBE THE METHODOLOGY USED TO DETERMINE THE

7 TRANSMISSION SYSTEM LOSSES.

8 For peak demand losses, the 2016 summer peak was modeled with powerflow studies and A. 9 the losses per circuit element were tabulated and grouped by voltage category. Any loss 10 contribution due to no-load losses was also calculated. For energy losses, the Study 11 Period was divided into four time segments consisting of whole months, and average 12 loads were computed for each time segment. Powerflow studies determined the losses 13 for each circuit element for the average load during each of the four segments. The 14 average loss per circuit element was determined and multiplied by the hours in the load 15 segment to determine the energy losses. The months included in each load segment are 16 identified in Appendix A of Exhibit No. SPS-0005.

17 Q. WHAT ARE "NO-LOAD LOSSES"?

A. Whenever a transformer is energized, a relatively small loss occurs even during hours
when no load current is passing through the transformer. These losses are referred to as
"no-load losses." Since transformers are typically energized every hour of the year, noload losses must be calculated for each transformer in order to accurately estimate losses
incurred at each transformer location.

1	Q.	WHERE ARE TRANSMISSION LEVEL LOSSES DISCUSSED IN THE 2016
2		LOSS STUDY?
3	A.	The circuit elements (i.e., lines and transformers) of the transmission system are
4		identified in Section 1.1 of Exhibit No. SPS-0005, and the process for calculating
5		transmission level losses for each type of circuit element is discussed in Sections 4
6		through 5.
7		Appendix M of Exhibit No. SPS-0005 presents a summary of losses for each type
8		of circuit element at both transmission and distribution levels.
9		Energy losses by level are stated in Appendix O of Exhibit No. SPS-0005 in the
10		column labeled "kWh Loss by Level" and Levels 2 and 3 are the transmission voltage
11		levels.
12		Losses for individual transmission circuit elements are tabulated in Appendices E
13		F, and G of Exhibit No. SPS-0005.
14		The summary results of the powerflow studies are in Appendix N of Exhibit No.
15		SPS-0005.
16	Q.	PLEASE DESCRIBE THE METHODOLOGY USED TO DETERMINE THE
17		DISTRIBUTION SYSTEM LOSSES.
18	A.	Peak demand and energy losses were calculated for the elements in the distribution
19		system and accumulated based on a typical representation of SPS's distribution system.
20		Losses were calculated for the distribution substation transformer, the primary feeders,
21		the secondary system (including distribution transformers), and the service lines to the
22		customers. The annual energy loss was determined by calculating annual energy loss per

1		distribution element and summing up the total energy loss. Similarly, demand losses		
2		were determined on each component of the distribution system and aggregated.		
3	Q.	Q. WHERE ARE DISTRIBUTION LEVEL LOSSES DISCUSSED IN THE 2016		
4		LOSS STUDY?		
5	A.	The circuit elements (i.e., lines and transformers) of the distribution system are identified		
6		in Section 1.1 of Exhibit No. SPS-0005, and the process for calculating losses for each		
7		type of circuit element is discussed in Sections 6 through 10.		
8		Appendix M of Exhibit No. SPS-0005 presents a summary of losses for each type		
9		of circuit element at both transmission and distribution levels.		
10		Energy losses by level are stated in Appendix O of Exhibit No. SPS-0005 in the		
11		column labeled "kWh Loss by Level" and Levels 4, 5, and 6 are the distribution voltage		
12		levels.		
13		Losses for individual distribution circuit elements are tabulated in Appendices I,		
14		J, K, and L of Exhibit No. SPS-0005.		
15	Q.	WHAT ARE THE RESULTS OF THE 2016 LOSS STUDY?		
16	A.	Total actual losses for the Study Period were 1,914,545 MWh, and the losses determined		
17		through the 2016 Loss Study's engineering analysis were 1,948,829 MWh. The		
18		undetermined losses are the difference, -34,284 MWh, which is -1.79% of the actual		
19		losses. See Appendix M of Exhibit No. SPS-0005, Line No. 44 for total actual losses,		
20		Line No. 42 for total determined losses, and Line No. 43 for undeterminable losses.		

1 Q. CAN YOU DETERMINE THE REASON FOR THE -34,284 MWH DIFFERENCE 2 BETWEEN THE LOSSES CALCULATED IN THE 2016 LOSS STUDY AND THE 3 ACTUAL LOSSES INCURRED? 4 A. No. Undeterminable losses are equal to the Total Actual Losses minus the Total 5 Determined Losses (calculated losses). The -34,284 MWh of undeterminable losses 6 cannot be assigned to any particular cause. A loss evaluation study is an engineering 7 analysis of line losses attributable to average electrical loadings of particular components 8 of the T&D system. There is always a difference between the actual and calculated 9 losses, which can be positive or negative, between the results of a computer analysis 10 using average loads and the actual line losses experienced. The small 1.79 percent 11 difference between the actual losses and calculated losses indicates the 2016 Loss Study reasonably represents the losses on the SPS T&D systems. 12 13 Q. ARE UNDETERMINABLE LOSSES TAKEN INTO ACCOUNT IN 14 **DETERMINING LOSS FACTORS?** A. Yes. The loss factors must be based on actual losses to ensure correct fuel factors. Thus, 15 16 the undeterminable losses, whether positive or negative, are assigned to the circuit 17 elements for which losses have been calculated in the study based on the ratio of each 18 circuit element's calculated loss to the total of all calculated losses. The results of this 19 assignment process appear in Appendix M of Exhibit No. SPS-0005 in the "Adjusted 20 Energy MWH" and "Factored KWH" columns. The totals for those columns tie to the

Total Losses on Line No. 66 of Appendix A of Exhibit No. SPS-0005.

21

1 DID ANY OF THE DATA OR METHODS USED TO CALCULATE LOSSES IN Q. 2 THE APPENDICES OF THE 2016 LOSS STUDY CHANGE FROM THE DATA 3 **USED IN THE 2013 LOSS STUDY?** 4 Yes, there are always changes in data from one study to the next. Changing the Study A. 5 Period changes much of the data, e.g. generation amounts, power purchases, peak load, 6 powerflow case results, Sales data, miles of T&D lines, customer meter counts, etc. The 7 updated data are reflected in the appendices of the 2016 Loss Study. 8 The SPS T&D systems modelled in the 2016 Loss Study have experienced four 9 major changes since the 2013 Loss Study. 10 First, there was significantly more wind and solar generation connected to SPS's transmission system in 2016 than in 2013. The effect of this additional 11 12 generation injecting power into the transmission system at different locations 13 than in the past has a significant effect on losses. 14 Second, a significant amount of wind and solar generation has been connected 15 to the SPS distribution system since the 2013 Loss Study. This wind and solar generation delivers energy directly to the distribution system in contrast to the 16 historical norm of nearly all the energy flowing through the transmission system 17 18 into the SPS distribution system. 19 Third, three new 345 kV lines that significantly strengthen the SPS connection 20 to the rest of the SPP grid were placed in service in 2014. The installation of 21 these transmission lines has allowed SPS and other wholesale load serving 22 entities ("LSEs") on the SPS system to purchase significant amounts of low-cost 23 energy from the SPP Integrated Marketplace and import that power into the SPS 24 system. These imports could significantly change the flows on the SPS 25 transmission system and therefore affect losses. 26 Fourth, there have been changing patterns of power delivery on SPS's system. 27 Recently, SPS has been transmitting more wholesale customer-procured power 28 than in the past.

Q. DID ANY OF THE METHODOLOGIES USED TO CALCULATE LOSSES IN

THE APPENDICES OF THE 2016 LOSS STUDY CHANGE FROM THE

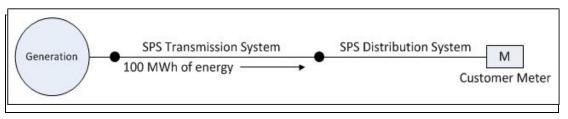
METHODOLOGIES USED IN THE 2013 LOSS STUDY?

A.

Yes. While the majority of the fundamental methodologies did not change, the increase in generation connected to the SPS distribution system from 2013 to the present Study Period has required a change in study methodology to accurately account for losses.

In previous studies, nearly all the generation was connected to the transmission system and the generated energy flowed through the transmission system to the distribution system. This energy flow scenario is shown graphically in Figure DJR-1:

Figure DJR-1
Historical SPS Energy Flow

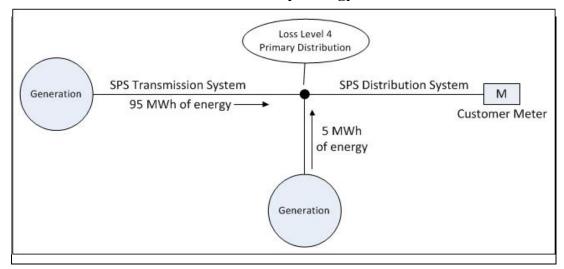


In Figure DJR-1, 100 MWh of energy flows through the transmission system to the distribution system, resulting in transmission losses in proportion to the 100 MWh flow of energy.

In the 2016 Loss Study, a significant amount of generation had been connected to the SPS distribution system, delivering energy directly to the distribution system. In this simplistic example, the energy delivered directly to the distribution system does not cause losses in the transmission system, resulting in lower transmission losses than in the scenario shown in Figure DJR-1. This new energy flow scenario is shown graphically in Figure DJR-2 (next page):

1 2

Figure DJR-2
2016 Loss Study Energy Flows



In Figure DJR-2, only 95 MWh of energy flows through the transmission system to the distribution system, while 5 MWh of energy is generated and delivered directly to the distribution system. This scenario results in transmission losses from only 95 MWh of energy flow instead of 100 MWh as in the first scenario.

In the 2016 Loss Study, the significant increase in generation connected directly to the distribution system necessitated a change in the study methodology to account for this change in the energy flows. The Loss Study now includes data in Appendix B of Exhibit No. SPS-0005 that summarizes the energy and demand delivered directly to the distribution system. Updates were made to the spreadsheets in the Excel workbook to reflect this change in flows so that the resulting loss calculations are accurate. The methodology used in the 2016 Loss Study shows the generation connected to the distribution system flowing into the distribution system at the low voltage side of the distribution substation transformer.

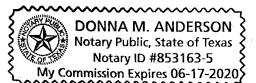
1	Q.	WAS THERE ANY CHANGE IN THE TREATMENT OF WHOLESALE
2		TRANSACTIONS WITH ENTITIES OUTSIDE OF SPS'S SERVICE AREA?
3	A.	No. The same net metering approach was used in the 2016 Loss Study as was used in the
4		2013 Loss Study.
5		IV. <u>CALCULATION OF LOSS FACTORS</u>
6	Q.	WHAT ARE "LOSS FACTORS"?
7	A.	A loss factor is simply a number, which when multiplied by a given amount of Sales,
8		yields the amount of energy that must be generated to produce the Sales amount. If, for
9		example, losses at a specific service level are 10%, then 100 MWh have to be generated
10		to yield 90 MWh of Sales. Thus, the loss factor at that level is 1.1111 (90 MWh sold x
11		1.1111 loss factor = 100 MWh generated).
12	Q.	DOES THE 2016 LOSS STUDY CONTAIN CALCULATED LOSS FACTORS?
13	A.	Yes. The Energy Loss Factor and the Demand Loss Factor for each SPS loss level are
14		shown in Appendices O and P of Exhibit No. SPS-0005. Loss factor derivation is
15		discussed in Section 12.0 of Exhibit No. SPS-0005. These loss factors were calculated
16		using the same methodology as in previous loss studies.
17		In his Direct Testimony, Mr. Berger discusses the necessary adjustments to the
18		results of the 2016 Loss Study he made to arrive at the real power loss factors (stated on a
19		loss percentage basis) SPS is proposing in this filing to include in the Xcel Energy Tariff.
20		V. <u>CONCLUSION</u>
21	Q.	DOES THIS CONCLUDE YOUR PRE-FILED DIRECT TESTIMONY?
22	A.	Yes.

UNITED STATES OF AMERICA **BEFORE THE** FEDERAL ENERGY REGULATORY COMMISSION

Docket No. ER19- -000

AFFIDAVIT

Duane J. Ripperger, being duly sworn, deposes and states: that the Direct Testimony of Duane J. Ripperger was prepared by me or under my direct supervision, and that the statements contained therein are true and correct to the best of my knowledge and belief.



Subscribed and sworn before me this 29th day of January 2019.

Donna M. Anderson
Notary Public
My commission expires: 6/17/2020

Exhibit No. SPS-0005 Page 1 of 95

Sponsor: Duane J. Ripperger

Southwestern Public Service Company 2016 Loss Evaluation Study

January - December 2016

SPS Transmission Planning Xcel Energy Services, Inc.

July 2017

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1.0 Overview

This report discusses an evaluation of transmission and distribution system losses for the 12 month period January – December 2016 (2016 Study Period). This evaluation was designed to be as introspective as technically possible and provide a significant level of confidence in determining the electrical losses on the Southwestern Public Service (SPS) transmission and distribution systems. This evaluation determines actual losses and then uses engineering principles to calculate both demand and energy losses at specific voltage levels.

SPS operates an electrical system consisting of 345 kV, 230 kV, 115 kV and 69 kV transmission lines and a distribution system with lines operating at 33 kV to 2.4 kV. The system spans a large 52,000 square mile area from the Oklahoma panhandle through the Texas panhandle and into eastern and southeastern New Mexico. SPS has generation on both 230 kV and 115 kV busses throughout this area. Since 2009 SPS and other power producers have installed significant wind and solar generation within the SPS boundary. Most of this generation is connected at transmission voltage levels and some at distribution primary voltage levels. The scope of this study was to determine the demand and energy losses for the following components:

Transmission System Components:

Generation Unit Main Transformers

Transmission Lines

Autotransformers

Distribution System Components:

Distribution Substation Transformers

Distribution System, including Primary, Secondary and Service Lines

Transformers

Southwestern Public Service Company Loss Evaluation Study for 2016 Study Period

The losses related to these elements of the power system are frequently seen in accounting reports as "Unaccounted For Energy." The purpose of this study is to determine actual losses and then specifically assign losses by the components identified above for the 2016 Study Year.

The losses of customer-operated transformers, transmission systems and distribution systems are not considered in this study. Any losses occurring in auxiliary busses at power plants are not considered in this study. Also, losses related to the generator step-up transformers are not included since net generation is recorded at the high voltage side of these transformers.

The analysis of losses requires consideration of both demand, or power, losses and energy losses. The demand losses are typically measured in megawatts (MW), kilowatts (kW), or watts. The energy losses are measured in megawatt-hours (MWh), kilowatt-hours (kWh), or watt-hours (Wh). Certain components of the energy losses are present even though there is very low electrical load passing through the device. An example of this is the magnetizing current and related losses of a transformer. After the transformer is energized, these losses will occur. Power flow through the transformer will increase the losses, but even in the absence of any power flow, the transformer will experience "no-load losses" simply because it is energized.

To provide a basis for the calculations in this study, data was gathered for the transmission and distribution systems. This data and associated calculations are shown in the Appendices of Attachment DJR-RD-2. All references in this document to a specific appendix are found in Attachment DJR-RD-2. Each Appendix corresponds to a section of the total loss calculation or provides data used in other appendices. Actual counts exist for the devices and miles of electric lines that cause losses at the transmission level. The calculation of losses at the transmission level involves very little engineering judgment. Actual counts of devices and line data exist for much of the

distribution system as well. In some cases, however, data does not exist for the distribution system and engineering approximations or judgments must be and were made to determine losses at specific voltage levels. These approximations are noted in the discussion.

1.1 Loss Levels

The energy losses for each physical category (lines, transformers, etc.) are grouped by the six Loss Levels. These Loss Levels, which are shown in Appendix H, are:

Loss Level 1 - Generation

Loss Level 2 – Backbone Transmission

Loss Level 3 – Sub - Transmission

Loss Level 4 - Primary Distribution

Loss Level 5 - Secondary Distribution Transformers

Loss Level 6 - Secondary Distribution Lines

Losses are not calculated at Level 1. The other levels are composed of the following physical loss categories:

Loss Level 2 – Backbone Transmission

345 kV, 230 kV and 115 kV Transmission Lines

345/230 kV, 230/115 kV Autotransformers

Loss Level 3 – Sub - Transmission

69 kV Lines

115/69 kV Autotransformers

Loss Level 4 - Primary Distribution

Distribution Substation Transformers

Distribution Primary Lines (33 kV to 2.4 kV lines)

Loss Level 5 - Secondary Distribution Transformer

Distribution Line Transformers

Loss Level 6 - Secondary Distribution Lines

¹ Auxiliary busses are distribution busses which provide internal power plant distribution service for internal power

Distribution Secondary and Service Lines

Transmission losses are those at Levels 2 and 3. Losses attributable to distribution facilities are those calculated for levels 4, 5 and 6. In setting loss factors for rate classes, the losses calculated at levels 5 and 6 are combined and a composite loss factor is determined.

The results of the 2016 Loss Evaluation Study are shown in Appendix M and the rate class loss factors derived from the study are in Appendix Q.

1.2 Determination of Actual Losses

Appendix A contains the determination of actual losses measured in MWh for the total transmission and distribution system based on 2016 Study Period operating data. The general definition of losses is the difference between the total resources and total deliveries. Specifically, the Total Resources, shown in Appendix A, are:

Net Generation (line 6) – metered output of SPS's generating plants

Net Metered SPP Interchange and WECC HVDC Interchange (lines 7 & 8) -

metered physical flows at all interchange tie points with the Southwest Power Pool (SPP) and the Western Electric Coordinating Council (WECC). Wherever SPS's transmission system interconnects with transmission systems of other utilities in the SPP or WECC, meters exist and data are captured to determine the energy either flowing into or out of SPS's system. The net flows into or out of the SPS system at these boundaries account for any purchases made from, or sales made to, entities outside the SPS boundary. In addition, if third parties enter into a sale and purchase transaction and SPS's transmission system is used to deliver power, the net metered flows at SPS's boundaries will reflect the

use of the transmission system by recording the inflow and the corresponding outflow. This process of calculating the net flows into or out of SPS's system is referred to as "net metering."

Firm Purchased Power

BEA, LPP (line 11) – SPS purchases energy pursuant to the contracts with Borger Energy Associates and Lea Power Partners, LLC.

LPL Generation (line 12) – SPS has a full requirements sales contract with West Texas Municipal Power Agency (WTMPA), an entity established by the cities of Lubbock, Tulia, Brownfield, and Floydada. SPS also contracts with the City of Lubbock to purchase the output of three Lubbock generating plants that operate only when requested by SPS. This generation is located within the Lubbock Power & Light (LPL) network and no SPS loss is attributable to this power. Line 12 is the total Lubbock generation during the 2016 Study Period.

Others (line 13) – SPS purchases relatively small amounts of energy from a number of other entities located within its system boundary pursuant to firm contracts. The collective purchases under these contracts are reported on this line.

Renewable Energy Purchases (lines 14-21) – these are energy purchases from renewable sources that have firm network transmission service.

Other Generation inside the SPS Boundary

Golden Spread Electric Cooperative (GSEC) owns the Mustang Plant near Denver City, Texas, and Antelope and Elk Stations located near Abernathy, Texas. GSEC has also purchased the output of the Panhandle Wind Ranch. Lines 23-27 show the GSEC resource outputs

for the 2016 Study Period. Since the GSEC generation is within SPS's boundary, its generation must be included in total area resources to prevent an under-statement of resources due to the net metering process described above.

Lea County Electric Cooperative (LCEC) Generation

This is renewable and fossil generation output that is connected to LCEC's 115 kV transmission line from SPS Hobbs Plant to SPS Denver City Substation. This is shown on lines 29-31.

Farmer's Electric Cooperative (FEC) Generation

This renewable generation is connected to FEC's transmission system and the value reported is the excess generation above FEC's load that flows back onto the SPS transmission system. This is shown on lines 33-34.

Export Renewables

The output of these renewable generators is scheduled or purchased by other companies outside of the SPS boundary. These energy values are shown on lines 36-42,

SPS Non-Firm Purchased Power

Lines 44-50 represent the output of various generators that are being purchased by SPS and flow onto the SPS transmission system.

Market Renewables

Lines 52-56 represent generators located within SPS's boundary sending power over SPS's transmission lines into the SPP Energy Market. Like GSEC's generation, this generation must be included in SPS's total

resources to prevent an under-statement of resources due to the net metering process described above.

The sum of these resources is the "Total Resources" (line 58) available on SPS's system for serving customer load within its system boundary.

Total Deliveries (line 64) consists of all retail sales, all full requirements wholesale sales within the system boundary, and all deliveries to Golden Spread load points within the system boundary.

Total Losses (line 66) are the actual losses experienced during the 2016 Study Period. Total Losses are calculated by subtracting the Total Deliveries on line 64 from the Total Resources on line 58. This value of Total Losses is the value that will be used to generate the loss factors by voltage level.

SPS's Total System Loss percentage during the 2016 Study Period is shown on line 67. This value is derived by dividing Total Losses (line 66) by Total Resources (line 58).

The "Net Output to Lines by Load Segment" data (lines 77-89) are simply the sums of monthly values for "Net Output to Lines" (line 74) for the months contained in each segment. The determination of segments is discussed in Section 3.1 and the Net Output to Lines by Load Segment data are used in determining transmission line losses in Section 4.3.

1.3 Distribution Connected Generation Sources

Appendix B contains a list of distribution-connected resources that deliver power directly onto the SPS distribution system at the primary level. These resource values

are used in the calculation of losses on the distribution system, specifically in Appendix J – Distribution Primary Loss.

2.0 Generation Step-Up Transformer Losses

Losses attributable to these transformers are included in station power and are not part of this study.

3.0 System Load Analysis

To determine the transmission line and autotransformer losses, it is necessary to perform powerflow studies at different system load levels throughout the year. The system loading levels must be determined before these studies can be done. For the period under study, the system loads are obtained from the operations center. The load represented in these studies is a composite of SPS retail load, GSEC and other wholesale loads within the SPS system boundary.

Any other sale or purchase of energy that either started in or was received into the SPS boundary, and including any through transactions from the east to west or west to east across the SPS system between the eastern and western grids are included when the powerflow models are developed to capture any transmission losses due to those transactions.

SPS's daily minimum and maximum load are summed to produce a daily average load. Then the corresponding values for tie line flows are obtained and summed for the same hour. This produces a daily minimum and daily maximum load to be analyzed. The results of this procedure are shown in Appendix D – System Load Data 6, Daily Maximum/Minimum Loads graph.

3.1 Segment Derivation

The daily maximum and minimum loads are still too detailed for the powerflow analysis, since there are 366 minimum and 366 maximum values for each load (2016 is a leap year). The next step is to produce a daily average load graph. The Average Value Analysis graph is shown in Appendix D – System Load Data 6. The average load is graphed for the study period. Then an average study value is fit to the graph. The goal of this fit is to minimize the sum of the errors between the average load values to be used in the study and the actual daily average load. Once this has been determined, the year can be broken into load segments which will be modeled in the powerflow program using the values of average load determined here. The load segments will typically be a spring period, summer period, and a fall/winter period. It is required that the segment boundary fall on whole calendar months because the all the data is based on a calendar month, For the 2016 Study Period, the best fit to model the loads for the 12 months was a four segment model. The sum of the errors in the 2016 Study Period is 0.28%. See Appendix D - System Load Data, line 8. The segment values used in this analysis were:

Segment 1:	January - February	3380 MW
Segment 2:	March - May	3323 MW
Segment 3:	June - August	4432 MW
Segment 4:	September - December	3387 MW

The average loads per segment, number of days in each segment and other values used in the analysis are shown on the chart in Appendix D - System Load Data.

3.2 Powerflow Loss Calculations

Once the segment loads have been determined, the powerflow analysis can be performed. The average segment load values determined above are used for the loads in the powerflow studies. Powerflow cases are run on each of the load segments under study. The generation patterns are varied between the segments to better represent

the mix of generators actually on-line at that time of the year. There is also a peak powerflow case prepared to analyze the system losses at the hour of the system peak.

The powerflow program used to perform studies is Power Technologies Inc.'s PSS/E program. Once the powerflows have been completed, the losses are summarized for the SPS system. The loss values for each transmission element and voltage class are tabulated for the peak hour case and for each segment period. The summary tabulations are shown in Appendix N. These losses represent the loss for that element for the segment load used. These values are then used to determine the transmission line and transformer losses.

Excluded from the loss tabulation are transmission systems that are not owned by SPS, but reside inside SPS's boundary and modelled in SPS's powerflow program. These systems are Lea County Electric, Lubbock Power and Light, and Tri-County Electric Cooperative.

4.0 Transmission Line Losses

The losses on transmission lines consist of several parts. Demand and energy losses on the transmission system consist of corona losses, insulator losses, and losses due to power flow through the transmission lines. These losses are tabulated by transmission voltage level in Appendix E.

4.1 Transmission Line Corona and Insulator Losses

Transmission systems have losses due to corona and insulator leakage. Corona loss occurs when the voltage gradient near the conductor surface exceeds the breakdown strength of the surrounding air. Insulator leakage is the small current that flows across the surface of the insulators attached to the electric conductor. The <u>Transmission Line Reference Book</u> published by Electric Power Research Institute contains information on determining the representative losses associated with corona and insulator leakage.

Using that reference, losses per mile for each transmission voltage level were determined and entered in the "KW Loss/mile" column. Transmission line mileage was taken from FERC Form 1 data. The demand loss due to corona and insulator leakage (Appendix E, "Demand Losses" column) is calculated by multiplying the kW loss per mile for a specific voltage level times the miles of transmission operating at that voltage and then dividing that product by 1,000 to yield a MW loss result. The energy loss is simply the demand loss times the number of hours per year. For 345 kV transmission lines, for example, the corona and insulator demand loss of 2.121 MW in Appendix E is the rounded value of this equation: (2.343 kW loss/mile x 905.42 miles) ÷ 1,000. The annual energy loss (18,634 MWH) for these same elements is the product of 2.121 MW (the unrounded value from the previous equation) x 8,784 hours/year.

4.2 Transmission Line Demand Losses

The losses calculated for transmission lines are shown in Appendix E, labeled Transmission Line Demand Loss. The peak demand losses were determined by tabulating the megawatt losses per transmission line as shown in the 2016 Study Period peak powerflow study in Appendix N. These losses are tabulated by voltage class.

4.3 Transmission Line Energy Losses

The energy loss for the transmission lines at each voltage level is determined by using the losses developed in the powerflows for each load segment. The segment loads are listed in Appendix E along with the net output of power to the transmission system during the segment. This value was determined in Appendix A and labeled "Net Output to Lines By Load Segment." The Net Output to Lines by Load Segment is the amount of generated and purchased energy put onto the transmission system to serve load. The determination of the energy losses for transmission lines of a specific voltage in a specific segment is calculated using the following equations.

Segment Loss Factor =
$$\frac{\text{Segment Loss for Transmission Element, MW}}{\text{Segment Load, MW}}$$
(4.3.1)

Segment Losses = Segment Loss Factor
$$\times$$
 Segment Output to Lines, MWH (4.3.2)

Thus, the powerflows provide a determination of the energy loss as a single value for each segment. Dividing the segment loss by the segment load produces a per MW energy loss factor. Multiplying this per MW energy loss factor by the Segment Output to Lines produces the energy loss for that element in that load segment. The energy loss values for the year are simply the sum of the energy loss values for each element in each load segment and appear in Appendix E on lines 37-43 under the column heading "Total Segment Losses, MWH."

5.0 Autotransformer Demand Losses

SPS's transmission system autotransformers reduce voltage from one transmission voltage to a lower transmission voltage. The high side and low side autotransformer voltages are typically written as "345/230," "230/115" and "115/69." See, e.g., Appendix G, column heading "Voltage", lines 2, 11 and 41. Each autotransformer in SPS's transmission system is identified in Appendix G. The load losses related to autotransformers can be separated into demand and energy components.

The demand component was determined in two steps. The first step was to determine the total demand loss for each voltage level of autotransformers from the summer peak powerflow study, summarized in Appendix N. This provided the MW loss due to loading at the peak time of the year. These losses are shown for each of three voltage classes of autotransformers at lines 3, 5 and 7 of Appendix F.

The second component of the autotransformer demand loss was provided by summing the individual transformer no-load demand losses for the different voltage classes of individual transformers in Appendix G in the three columns under column heading "Demand Losses, KW." This component represents the demand loss incurred by simply energizing the transformer, as described below.

5.1 Autotransformer Energy Losses

The energy losses related to autotransformers can also be separated into two parts. The first part is the energy loss associated with no-load operation. This is the energy loss due to the magnetizing currents that exist when a transformer is energized. These losses were determined by multiplying the no-load loss in Watts as shown under column heading "No Load Loss, Watts" in Appendix G by the number of hours in the 2016 Study Period because these autotransformers are assumed to be energized throughout the study period.

The energy losses related to loading were determined using the same methodology as for transmission lines. For each powerflow study, a tabulation of the autotransformer demand losses by voltage level was calculated. A segment loss factor for each segment was calculated by dividing the MW Loss by the Segment Load in Appendix F. The autotransformer energy losses for each segment were calculated by multiplying the segment loss factor by the Segment Output to the Lines for that segment. This produces the average energy losses for each voltage level for each segment. The data needed to make these calculations and the results are shown in Appendix F. The equations used to obtain the energy losses for the autotransformers are the same as Equations 4.3.1 and 4.3.2.

All losses discussed to this point are transmission level losses. The losses discussed in the following sections 6 through 10 are losses at the distribution level.

6.0 Distribution Substation Transformer Losses

Distribution substation transformers are those transformers that reduce the transmission voltage, e.g., 69 kV, to a distribution voltage, such as 33 kV, 22 kV or 12.5 kV. The data for each distribution substation transformer are in Appendix I. Manufacturers' data were used to determine losses. If manufacturers' data were not available for a specific transformer, data for a similar transformer manufactured by another company were used.

Column 9 has a code for verification of data. The codes used in this field mean:

- R ratings were verified from manufacturer's data
- L loss values were verified from manufacturer's data
- E loss values are an estimate

There are many transformers on SPS's system that are either owned by a specific customer or have metering or other arrangements to reflect the billing on the high side of the transformer, *i.e.*, before losses are incurred. These transformers are excluded from the loss calculations in Appendix I, and excluded from Appendix I's list of transformers, because SPS does not incur the losses associated with these transformers (the losses are borne by the customer leasing the transformer). In some situations, only a portion of a transformer's capacity is leased, and thus, only a portion of the losses associated with that transformer should be excluded. These transformers are identified by the letter "E" in column 10 of Appendix I, and the percentage of losses to be excluded is stated in column 15. The letter "I" in column 10 means that all of the transformer's losses are included in the loss calculations.

6.1 Distribution Substation Transformer Demand Losses

The demand losses associated with these transformers have two components. The first component is the magnetizing current losses that are present anytime the transformer is energized. The second component is the full load loss value for the transformer. Manufacturers' test report data was used to determine the no-load loss

and the loss when the distribution transformers were loaded to their nominal MVA ratings (Appendix I, column 4). Loading of transformers at their nominal MVA rating is referred to in Appendix I as "full load" but this label does not mean that the transformers have no additional capacity. The maximum MVA loading for each transformer is listed in Appendix I, column 5. As evidenced by the differences between the values in columns 4 and 5 of Appendix I, many transformers can handle loads in excess of their nominal "full load." The no-load losses and nominal "full load" losses for each transformer are tabulated in Appendix I, columns 6 and 7, and totaled for the entire system near the bottom of Columns 6, 7, and 8 on line 302.

It was assumed for the purposes of this study that the distribution transformers were operating at "full load" (their nominal MVA ratings) at the time of the system peak. This assumption was reasonable, conservative, and necessary. The transmission and distribution system is designed to handle the system's peak load and have additional capacity available in case peak load is greater than forecasted. And, of course, system load has grown since most of these transformers were originally sized and installed. Thus, at the time of system peak, it is likely that many transformers operated somewhere between their nominal and maximum MVA ratings. Thus, basing losses upon only the nominal MVA loading, as SPS has done, is conservative. Using this assumption was necessary since manufacturers typically provide test data only for losses at the nominal MVA rating.

6.2 Distribution Substation Transformer Energy Losses

The energy loss has two components. The first is the no-load loss, which occurs during every hour of the Study Period. Referring to Appendix I, this value was calculated by multiplying the no-load losses derived from manufacturers' test data, column 6, by the number of hours in the Study Period, which results in the energy loss during the Study Period, as shown in column 12.

The full load loss required the determination of the load characteristic of the load being served by a particular transformer. The load factor assigned to each transformer is shown in Appendix I, column 11.

The load factor for a study period is defined as:

Load Factor =
$$\frac{\text{Total Study Period Energy Delivered}}{\text{Max. Demand} \times \text{Hours in Study Period}}$$
(6.2.1)

For the purpose of determining the study period energy losses, the following equation was used:

Losses = Full Load Loss
$$\times$$
 Hours in Period \times Load Factor (6.2.2)

The results of this calculation are shown in Appendix I, column 13.

The "Sum of demands adjusted for Primary Generation" is the estimated load at primary and shown on line 305. The 47.291 MW adjustment shown on line 304 is the coincident wind and solar primary generation from Attachment B at system peak hour and it thus reduces the total flow on the primary feeders. This generation connected to the primary voltage level may all flow into the primary voltage level and never get transformed to the transmission voltage level.

6.3 Calculation of Load at Each Feeder Voltage Level

The load at each feeder voltage level is calculated at lines 312-319 of Appendix I. The loading on 33 kV feeders, for example, is calculated by determining the ratio of the nominal MVA of transformers connected to 33 kV feeders (153.30 MVA on line 314) to the adjusted nominal MVA of all distribution substation transformers (3,026.08 on line 314) and then multiplying that ratio by total loading on all distribution feeders (line 305). Thus, for 33 kV feeders, the calculated loading is: (153.30/3,026.08) x 2,206.35 MW =

111.77 MW. This value appears at line 315, column 2 of Appendix I. From this value, the load on transformers with no feeders (line 316) is subtracted to yield the load on 33 kV feeders, which appears on line 319. Line 317 shows data on total numbers of feeders at each voltage level and line 318 shows the number of feeders after excluding the portions of transformers that are shared with customers.

7.0 Load Factor Derivation

The load factor used to calculate the study period full-load energy losses reflected in Appendix I, column 11, provides a representative load factor for substation loads. However, the load factor is not a pure load factor, such as might be found for a rate class. Rather it represents the composite mix of customer load which occurs on the power system. This load factor is calculated in Appendix H.

The data used in Appendix H comes from rate analysis of each customer class on SPS's system for the Study Period. Using this data, monthly demand peaks and monthly energy deliveries, a composite load is developed which represents the desired substation class load. With the summed energy and demands, a load factor can be calculated. The annual load factor for primary distribution, Loss Level 4 is shown in Appendix H, line 78 under table column heading "Total Loss Level 4."

8.0 Distribution Primary Feeder Losses

The primary distribution system (Level 4 in the loss study) includes the distribution lines (feeders) that transport power from the distribution substation to the distribution line transformers near each customer. The losses associated with these primary distribution feeders are calculated on Appendix J. At the top of Appendix J, the distribution loads and energy are summarized for the Study Period. They are broken into loss levels and they represent the demand and energy for each level of the distribution system. These values shown are derived from Appendix H and they will be

used throughout the distribution loss calculations. On lines 2 and 9, the demand and energy values are offset by the distribution connected generation, obtained from Appendix B.

Losses are calculated for 552.10 feeders operating at 6 nominal voltage levels (33 kV, 22 kV, 13.2 kV, 12.5 kV, 4.16 kV and 2.4 kV). There are 573 feeders connected to the transformers (Appendix I, line 317), but some feeders are connected to transformers whose capacity is shared with customers. Thus, the number of feeders at each voltage level has been reduced in proportion to the nominal MVA of substation transformers at each voltage level leased by customers. The percentage of each transformer's capacity leased to a customer is shown in column 15 of Appendix I. This process produces fractional feeders that are used to calculate primary distribution feeder losses.

8.1 Distribution Primary Feeder Demand Losses

The number of feeders and load at each distribution voltage level are derived from lines 318 and 319, respectively, of Appendix I.

The Feeder Current, in amps, is:

Feeder Current =
$$\frac{\text{Feeder Load}}{(\sqrt{3}) \times \text{Feeder Voltage}}$$
 (8.1.1)

The Feeder Loss, in watts, for a given voltage level is:

Feeder Loss =
$$3 \times (\text{Feeder Current})^2 \times \text{Resistance} \times \text{Average Length}$$
 (8.1.2)

The length of each feeder varies considerably as do the wire sizes (conductors) used in the construction, which affects resistance. The distribution system database consists of 552 feeders ranging in length from zero to 48.6 miles and many different wire sizes and materials. The typical conductor size was determined by summing the feeder lengths

by voltage and by conductor type and size, selecting the most common conductor based on length and conductor material and size. The results of this investigation appear under the column heading "Typical Conductor" in Appendix J.

The average feeder length was determined by sorting the feeders by voltage and dividing the sum of the lengths by the number of feeders in each voltage range. A feeder was counted if the length was greater than 0.05 miles. There were 552 feeders that fit this criterion. The results of this investigation appear under the column heading "Avg. Feeder Length, Miles" in Appendix J.

The total loss for a given voltage level is obtained by multiplying the loss determined above by the number of feeders in the given voltage level.

8.2 Distribution Primary Energy Losses

These losses were calculated by multiplying the demand energy loss for the entire load served via primary distribution line by the hours in the study year and by the loss factor for the entire distribution load. The load factor is determined in Appendix J from the Total Primary Demand and the Total Energy. Note that the Total Primary Demand and Energy have been offset by the distribution primary connected generation from Appendix B. The Loss Factor is determined by the following equation:²

Loss Factor =
$$(0.3 \times Load Factor) + (0.7 \times (Load Factor)^2)$$
 (8.2.1)

Thus, the losses over the year are determined by the following equation:

Loss = Demand Loss
$$\times$$
 8784 hours \times Loss Factor (8.2.2)

9.0 Distribution Line Transformer Losses

² Westinghouse Electric Corporation, <u>Distribution Systems</u>, 1965, page 28.

Appendix K contains the loss calculations for distribution line transformers, which corresponds to Loss Level 5. The number of meters and transformers are actual counts derived from SPS's records. The meters per transformer data is derived by dividing the adjusted meter count by the number of transformers, *e.g.*, 331,812 single phase meters/97,184 transformers equals 3.41427 meters/transformer.

In calculating losses, it is necessary to distinguish between single phase transformers, which serve primarily residential customers, and three phase transformers, which serve primarily commercial customers. The "Adjusted Meters" column on Appendix K performs this function by assigning the single phase commercial meters to the "Residential" category, *i.e.*, Residential Adjusted Meters equals actual residential meters (301,809) plus the difference between all commercial meters and three phase commercial meters (30,003).

It was assumed that one residential customer took service directly from each distribution line transformer and that all other residential customers were served from secondary distribution lines. Secondary lines are the lines that typically run from a pole top transformer to another pole that has no transformer. From that second pole, a service line runs to the customer's premises. Losses on secondary lines and drops are addressed in Appendix L. For three phase commercial customers, the number of transformers essentially equals the number of meters, and thus, each such customer is assumed to be served directly from the transformer.

9.1 Distribution Line Transformer Demand Losses

Based on consultation with distribution system engineers, typical transformer sizes were chosen as 25 KVA (residential) and 100 KVA (commercial). The transformer loss data at no load and "full load" for each size are listed in Appendix K at lines 26 and 27. The average load per customer is developed by taking the demand served and dividing by the number of customers. Then the loss per transformer is developed by taking the load per customer and calculating the losses proportionally to the load served by the

transformer and its full load rating. The total demand loss is determined by multiplying the number of transformers by each no-load and full load loss component. The no-load and loaded losses are shown at Appendix K, lines 35 and 37, and totaled at lines 39 and 41.

9.2 Distribution Line Transformer Energy Losses

These losses were calculated by using the demand energy loss for the distribution line transformers and multiplying by the loss factor of the load served through the distribution transformers and by the number of hours in the Study Period. The load factor is determined from data in Appendix K using the Total Secondary Distribution Transformer Demand and the Total Secondary Distribution Transformer Energy. The Loss Factor is determined from equation 8.2.1. Thus, the losses over the year are determined by the following equation.

Loss = Demand Loss
$$\times$$
 8784 hours \times Loss Factor (9.2.1)

10.0 Distribution Secondary Losses

The distribution secondary losses are determined in Appendix L. To determine the secondary losses, it was estimated that the secondary conductor was 1/0 MCM ACSR conductor and that there was 60 feet of conductor serving each residential meter not served directly from the transformer. The resistance of this secondary was 0.0127 ohms. The typical residential load and current and the commercial load and current were determined in Appendix K. There is no consideration of commercial load on secondary lines, as these customers are usually served directly from transformers.

10.1 Distribution Secondary Demand Losses

There was assumed to be 2 meters per 60 foot of secondary line. The loss, in watts, on the secondary was determined by the following equation:

$$Loss = \left(2 \times I^2 \times R\right) \tag{10.1.1}$$

Multiplying by the number of meters (Appendix K) produces the total loss for the distribution secondary.

10.2 Distribution Service Line Demand Losses

It was estimated that residential service line consisted of 65 feet of #2 Triplex and commercial service line consisted of 30 feet of #1/0 Quadraplex service wire. The resistances for these service lines are 0.02028 ohms and 0.00636 ohms, respectively. The current for each type of customer is calculated and the losses are calculated by the following equations:

Loss =
$$2 \times 1^2 \times R$$
, for residential customers and (10.2.1)

Loss =
$$3 \times I^2 \times R$$
, for commercial customers (10.2.2)

The total loss for each group was determined by multiplying the loss per meter by the number of meters, which are found on Appendix K.

10.3 Distribution Secondary and Service Lines Energy Losses

These losses were calculated by adding the demand loss of both the Secondary and Services and multiplying by the number of hours in the test year and also multiplying by the loss factor of the load that is served by Secondary and Services. The load factor is determined from data in Appendix L using the Total Secondary Distribution Transformer Demand and Total Secondary Distribution Lines demand and their associated energy. The Loss Factor is determined from equation 8.2.1. Thus, the losses over the year are determined by the following equation.

Loss = Demand Loss
$$\times$$
 8784 hours \times Loss Factor (10.3.1)

The results of this calculation are shown in Appendix L.

11.0 Summary of Transmission Loss Study

Appendix M contains the results of all of the calculations discussed previously. The power system elements for which losses are determined are:

Transmission Lines

Autotransformers

Distribution Substation Transformers

Distribution Primary Lines

Distribution Line Transformers

Distribution Secondary and Service Lines

Line 42 shows the total of the loss values obtained by the study, labeled as "Total Determined Losses" or calculated losses. Line 44, labeled "Total Losses," is the actual energy losses determined in Section 1.2 of this report. The difference between the results of this study and the actual losses is shown on line 43 as "Undeterminable Losses". Typically, the results from a loss study will be within a few percent, plus or minus, of the actual losses. For the 2016 Study Period, the Total Determined Losses are over estimated by 1.79% of actual losses. It should be noted that nowhere in this study is the actual loss value used to force the loss study to produce a final answer equal to the actual loss value.

The results of this study are used to determine loss factors for the different rate classes. To do this, the calculated losses must be adjusted to total to the actual losses, and thus, the Undeterminable Losses (Appendix M, line 43) have to be allocated to Loss Levels 2 through 6. Each category of energy losses is allocated a portion of the Undeterminable Losses equal to the ratio of that category's calculated losses to Total Determined Losses in MWh. For example, the "Adjusted Energy MWh" value for Transmission Lines – 345 kV (line 14), which is 80,473 MWh, is determined by: 81,914

MWh (line 14 determined energy loss) x (1,914,545 MWH Total Losses /1,948,829 MWH Total Determined Losses).

The values in Appendix M under the column headings "Demand Total Loss, KW" and "Energy Total Loss, kWh" are used in the development of the rate class loss factors.

12.0 Loss Factor Derivation

Appendices O and P contain the derivation of the rate class loss factors from summary data derived in various sections of the report. The rate class loss factors are determined for the loss levels shown in Appendix O and P.

The method to determine the loss factors is based on starting with the total resource input to the system at Generation Level, Level 1. This value is the starting point for the worksheet. Using Appendix O as an example, from this value, the deliveries for that level and the losses for that level are subtracted, leaving the 'Net KWH into each Loss Level'. This calculation is done for each loss level, with the result that all losses and deliveries have been subtracted from the Total Resources, with a result of zero. This means that all deliveries and losses have been assigned to a loss level and there is no error. Loss factors are calculated at each level as the subtraction progresses to the right through the loss levels. The calculation is shown in the appendices along with the loss factors by rate classification.

The process of calculating the Demand Loss Factor in Appendix O is the same as described for the energy factor calculation. However, rather than redistributing the energy "Undeterminable Losses" among the different loss levels, the Demand MW from line 42 Appendix M is used.

Southwestern Public Service Company Loss Evaluation Study for 2016 Study Period

Appendix Q contains the Demand and Energy Loss Factors by rate class in summarized form, without their respective derivations. The composite loss factors are shown for rate classes in loss levels 5 and 6.

Loss Derivation	Total Resources SPS Net generation (+) Net Metered SPP Interchange WECC HVDC Net Interchange	SPS Firm Purchased Power BEA, Lipe LPL Generation Others (Sid. DeGau)	Removables Caproce Wind (unit 1) San Jum (unit 1) Lian Wund Farm Sprinne Son Wind Widerado (unit 1) Rosenet Wind Project Chaves meter or Chaves & Roswell solar	GSEC Generation Musing Plant - GSEC Modelpe Plant - GSEC Elik Plant GSEC Panhandle Wind Ranch - GSEC(Wildrado 2)	Lea Co Electric Cooperative Wilden Wind-Phase 2- LeaCo WFEC -GAS PLT-LeaCo	Farmers Electric Cooperative Brahms Wind	Export Renewables Buffailo Dumbas Majestic (unit) Majestic (unit) Majestic (unit 2) Gotoshell Wind Captors Solar Bethel Wind	SFS Non-Firm Purchased Power OEO BOVOUS 18 11 Purces showed east load Person Will all allowe SFEC load Pleasant Hill - allowe SFEC load Non-Distant Hill - allowed S	Market Renewables Noble Great Plains (uni 1) Buffia Dunes Wind Milo Wind Surray 3-wind	otal Resources	Total Deliveries Retail/Wholesale Deliveries	WTMPA Sales (FYI -In Total Sales above) Total Deliveries	Total Losses	Net Output To Lines Derivation Total Resources	Net Output To Lines	Net Output to Lines By Load Segment	Load Segment Period 1: Jan Feb.	Load Segment Period 2: Mar May	Load Segment Period 3: Jun Aug.	Load Segment period 4: Sep Dec.	Total Region
2016	1,102,927 199,670 -423	509,996 13,893 10,508	23.013 32.956 14.072 47.188 44.621 86.659 0	84,912 2,099 0 23,416	8,611 2,156	2,222	67,464 22,048 17,606 58,628 0	22,146 815 816 9,614 1,676 16,735 2,577	21.418 3.828 13.172 10.998	2,477,222	2,373,529	2,373,529	103,693	2,477,222	2,477,222		4,685,818	7,256,647	10,175,397	9,640,414	31,758,276
2016	820,336 50,584 -1,633	448,624 5,973 9,778	25,492 36,171 22,934 57,028 52,992 91,296	196,305 2,640 7 24,100	8,711 930	3,352	83,617 29,421 19,620 79,373 0	30,379 1,351 11,380 2,816 22,493 3,747	27,383 8,454 18,153 14,789	2,208,596	2,134,921	2,134,921	73,676	2,208,596	2,208,596						
2016	1,005,873 23,559 -5,255	450,648 13 9,606	29,214 42,787 23,776 63,986 60,731 99,977	144,159 17 1,833 22,800	8,890	3,363	86,867 30,579 18,941 82,278 0	27,293 1,516 13,366 3,072 25,455 3,721	21,697 6,415 19,459 14,484	2,341,644	2,282,910	2,282,910	58,735	2,341,644	2,341,644						
2016	1,256,856 57,215 -6,008	291,067 12 5,700	23.675 34.672 20,004 55,732 51,885 88.515 0	214,115 0 0 19,817	8,729 2,579	1,384	80,792 26,684 23,505 73,437 0	22,754 1,128 13,786 1,781 21,620 2,950	19,939 5,923 17,814 13,308	2,449,370	2,279,558	2,279,558	169,812	2,449,370	2,449,370						
2016	1,203,631 -85,047 -5,176	445,062 923 6,191	29,088 36,017 19,184 62,947 59,531 93,477	223,616 3,491 0 23,085	9,2 <i>57</i> 2,632	1,948	71,729 28,539 28,632 80,913 0	27,837 958 13,682 1,258 22,481 3,013	20,940 3,317 19,459 13,017	2,465,633	2,407,034	2,407,034	58,599	2, 465,633	2,465,633						
2016	1,623,761 4,020 -18,952	357,564 13,841 11,076	20,848 23,933 14,631 46,164 45,626 70,612	312,917 16,767 0 21,859	6,187	545	56,750 21,537 22,408 63,205 0	22,849 626 9,490 751 17,216 2,325	21,497 816 13,803 9,018	2,838,670	2,719,865	2,719,865	118,805	2,838,670	2,838,670						
2016	1,817,540 178,568 -42,457	468,722 21,388 11,953	28,387 32,523 17,772 66,105 59,302 87,868 6,811	373,005 17,922 0 28,918	7,224	186	60,437 26,445 28,520 75,716 0	24,894 512 10,837 20,998 2,053	29,214 1,714 17,540 661,379	4,146,876	3,329,070	3,329,070	817,806	4,146,876	4,146,876						
2016	1,696,692 158,601 -7,626	471,956 18,945 7,739	22,432 20,347 11,723 50,053 44,782 62,711 15,189	338,948 20,531 1,601 21,645	5,197 4,714	154	55,994 17,908 19,874 59,532 0	3285 329 6957 2 12561 2,165	22,334 1,114 12,803 8,658	3,189,851	3,064,511	3,064,511	125,340	3,189,851	3,189,851						
2016	968,319 198,440 -29,311	439,929 17,248 7,663	30,517 30,744 16,465 48,554 62,972 80,179 16,441	212,399 2,699 0 11,163	5,770 5,603	1,956	78,367 20,670 25,461 69,730 0	4,199 959 8,263 2,232 22,745 1,387	9,900 3,036 15,141 11,961	2,401,802	2,310,541	2,310,541	91,260	2,401,802	2,401,802						
2016	1,109,278 32,031 -4,390	454,842 13,148 3,159	33,748 33,117 21,247 74,893 72,573 95,526 30,272	39,520 921 0 26,582	7,571	2,199	82,159 31,097 31,558 87,302 0 1,486	11,438 3,200 12,538 2,905 26,533 1,444	23,483 3,069 17,314 15,619	2,405,024	2,311,025	2,311,025	93,999	2,405,024	2,405,024						
2016	1,288,611 -10,628 0	278,369 3,482 5,292	25,121 32,176 17,196 54,444 51,766 84,507 21,680	97,944 1,922 0 14,727	8,088	2,435	74,680 23,774 23,392 65,663 3,028 25,348	3,195 1,297 10,676 2,190 19,960 1,549	9,694 3,928 17,132 12,946	2,280,188	2,216,346	2,216,346	63,842	2,280,188	2,280,188						
2016	1,118,266 123,598 0	474,668 10,507 7,500	32,706 42,113 21,011 61,516 60,684 104,966 15,104	80,197 4,536 0 19,122	7,699	4,042	73,795 27,591 27,369 65,228 3,278 65,253	889 1,891 9,695 2,658 21,227 1,892	13,428 5,025 19,271 13,845	2,553,401	2,414,422	2,414,422	138,979	2,553,401	2,553,401						
PERIOD	15,012,090 930,611 -121,231	5,091,447 119,373 96,165	324,241 397,556 220,015 686,610 667,465 1,046,293 105,497	2,318,037 73,545 3,441 257,234	91,934 53,952	23,787	872,651 306,293 286,886 861,005 6,306 92,087	201,158 14,672 130,284 21,376 250,024 28,823	240,927 46,639 201,061 800,022	31,758,276	29,843,731	29,843,731	1,914,545 6.0285%	31,758,276	31,758,276						

ne No. 1		Jan 2016	Feb 2016	Mar 2016	Apr 2016	May 2016	Jun 2016	Jul 2016	Aug 2016	Sept 2016	Oct 2016	Nov 2016	Dec 2016	TOTAL PERIOD	MW Output at Peak
က	SPS Distribution Connected Resources at Level 4 - Distribution	urces at Level 4	- Distributio	on Primary											
4 к	Aeolus Wind	∞	ď	r.	ĸ	4	10	9	4	4	4	g	7	67	0 00 No data
9	Sun Edison Dist Solars	6,935	8.788	10.911	11.577	11.126	11.694	12.016	9.154	8.453	8.215	5.199	4.744	108.812	39.62
7	Subtotal DeWind - Pringle	2,902	4,433	3,788	2,971	2,872	2,375	2,531	1,429	934	895	1,864	2,424	29,418	60.0-
80	West Texas A&M University	-	-	-	-	-	-	0	0	0	0	-	-	80	-0.02
6	Suzlon 8 Wind	634	1,489	1,800	1,628	1,265	1,107	1,595	1,205	1,106	1,718	1,381	1,731	16,659	0.79
10	High Plains Wind Farm (Exelon)	2,066	2,822	2,980	2,673	2,668	1,851	2,567	1,620	2,048	2,984	2,413	2,979	29,671	-0.03
7	JD Wind (unit 1) (Exelon)	1,600	768	651	949	1,128	622	572	389	367	752	294	22	8,114	0.22
12	JD Wind (unit 2) (Exelon)	1,706	1,264	1,333	1,275	1,017	265	9//	829	1,064	1,292	836	485	12,474	0.22
13	JD Wind (unit 3)(Exelon)	1,269	623	736	902	1,263	1,018	722	426	393	320	361	176	8,212	0.26
4	JD Wind (unit 5)(Exelon)	1,696	2,956	2,780	2,273	2,383	1,849	2,313	1,590	2,248	2,466	1,360	1,948	25,862	0.03
15	JD Wind (unit 6)(Exelon)	2,216	2,975	3,100	2,692	2,222	2,054	2,563	1,809	2,599	2,768	1,747	2,514	29,259	-0.01
16	JD Wind (unit 7)(Exelon)	2,210	3,148	3,059	2,798	2,645	1,859	2,351	1,598	2,362	2,967	2,661	2,947	30,605	0.54
17	JD Wind (unit 8)(Exelon)	2,154	3,215	3,041	2,718	2,433	1,698	2,298	1,623	2,218	2,977	2,621	2,908	29,904	0.38
18	JD Wind (unit 9)(Exelon)	2,136	3,154	2,904	2,213	2,245	1,775	1,932	1,636	2,197	2,957	2,565	2,831	28,545	0.32
19	JD Wind (unit 10)(Exelon)	2,126	2,897	3,002	2,483	2,128	1,386	2,134	1,443	2,035	2,751	2,569	2,748	27,702	-0.10
20	JD Wind (unit 11)(Exelon)	2,228	2,993	2,744	2,300	2,044	1,443	2,113	1,494	2,006	2,840	2,512	2,876	27,593	0.43
21	Mesalands CC Wind	15	7	7	80	9	10	6	6	22	17	7	1	128	
22	Llano Estacado (Texico)	115	42	52	61	52	99	20	9/	09	40	81	71	764	0.00 No data
23	Ralls Wind Farm	1838	1954	2538	1675	1668	1855	2004	1575	1929	2695	2804	2,954	25,489	4.68
24														439,286 MWH	47.29 MW
25															

Appendix C Generator Step-up Transformer Energy Losses

Appendix C

Not used in this loss evaluation study

٧	В	ပ	О	>	ΑΑ	AB	AC	AD	ΑE	AF AG	AG	AH	AI	Υ	AK	٩٢	AM	AN
										Month		P/EPE	MNd	LAMAR	TNP/EPE PNM LAMAR LPL FLOW	SWPP	WIND SOLAR	SOLAR
					Region	Region Avg Load %Errd	%Error	Start Da	ror Start Da End Day Entry	Entry		Avg	Avg	Avg	Avg	Avg	Avg	Avg
					1	3379.70	%90.0	1	09	60 1			0.12		188.59	-199.84	775.38	
					2	3323.40	0.11%	61	152	92 2			0.12		176.87	29.02 870.39	870.39	
					3	4432.10	%60'0	153	744	92 3			-4.55		240.57	-173.61	-173.61 648.24	
					4	3386.88	0.02%	245	998	122 4	. 4	1.39	99.9	-4.45	188.41	-147.71 788.83	788.83	34.22
						Total Error 0.28%	0.28%			366								

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	٧	В	၁	Q	Е	F	ტ	т	_	٦	メ	7	Σ
10					Hr @	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	# bəs	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	SWPP	Tbr	MIND	SOLAR
12											TIE FLOW		
13	-	Jan	1	2016	17	3244	0	0	0	-252	199	299	_
14	7	Jan	2	2016	16	3130	0	0	0	-558	186	41	4
15	က	Jan	3	2016	17	3006	0	0	0		164	34	15
16	4	Jan	4	2016	_	3235	34	0	0	-342	185	129	3
17	2	Jan	2	2016	3	3360	0	0	0	-198	163	1101	3
18	9	Jan	9	2016	3	3323	0	0	0	-2	150	1396	3
19	7	Jan	7	2016	3	3240	0	0	0	-103	144	1243	3
20	∞	Jan	∞	2016	4	3240	0	0	0	-708	138	374	က
21	စ	Jan	6	2016	3	3422	0	0	0	-718	178	464	3
22	10	Jan	10	2016	4	3469	0	0	0	-331	194	355	က
23	7	Jan	11	2016	16	3340	0	0	0	-612		39	24
24	12	Jan	12	2016	17	3263	0	0	0	-441	177	116	17
25	13	Jan	13	2016	17	3224	0	0	0	-594	175	45	18
26	14	Jan	14	2016	16	3210	0	0	0	-580	164	629	19
27	15	Jan	15	2016	3	3231	0	0	0	-571	178	672	0
28	16	Jan	16	2016	2	3205	0	0	0	-131	173	618	0
29	17	Jan	17	2016	16	3294	0	0	0	-367	179	360	28
30	18	Jan	18	2016	17	3388	0	0	0	-187	189	966	18
31	19	Jan	19	2016	3	3266	0	0	0	-168	160	1147	0
32	20	Jan	70	2016	16	3235	0	0	0	41	174	1143	28
33	21	Jan	21	2016	3	3181	0	0	0	349	142	1368	0
34	22	Jan	22	2016	17	3207	0	0	0	-327			22
35	23	Jan	23	2016	16	3122	0	0	0	-473	176	689	30
36	24	Jan	24	2016	17	3066	0	0	0	320	169	1570	22
37	25	Jan	22	2016	2	3058	0	0	0	214	156	1371	0
38	26	Jan	56	2016	3	3191	0	0	0	-514	153	358	0
39	27	Jan	27	2016	17	3216	0	0	0	-611	153	139	24
40	28	Jan	28	2016	0	3143	0	0	0	394	170	1436	0
41	29	Jan	29	2016	18	3113	0	0	0	-315	174		3
42	30	Jan	30	2016	0	2997	0	0	0	436	149		0
43	31	Jan	31	2016	3	2913	0	0	0	147	135	1257	0

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				Hr @	Min Sys	TOTAL	TOTAL	TOTAL		TOTAL	TOTAL	TOTAL
ged #	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	ddMS	LPL	MIND	SOLAR
										TIE FLOW		
	Feb	1	2016	2	2980	0	0	0	-190	156	664	0
	Feb	7	2016	2	3272	0	0	0	244	175	_	7
	Feb	3	2016	16	3334	0	0	0	-458	216	290	21
	Feb	4	2016	17	3240	0	0	0	-349	161	148	27
	Feb	2	2016	က	3329	0	0	0	233	165	1282	0
	Feb	9	2016	17	3040	0	0	0	896-	154	414	27
	Feb	7	2016	18	3069	0	0	0	6	152	921	2
	Feb	∞	2016	2	3157	0	0	0	148	151	1162	0
	Feb	6	2016	17	3163	0	0	0	-38	190	474	33
	Feb	10	2016	0	3090	0	0	0	170	156	748	0
	Feb	11	2016	2	3016	0	0	0	482	148	1151	0
43	Feb	12	2016	2	3067	0	0	0	-453	159	393	0
44	Feb	13	2016	0	3049	0	0	0	-114	146	1191	0
	Feb	14	2016	17	2975	0	0	09	-263	167	251	34
46	Feb	15	2016	1	3020	0	0	0	717	159	373	0
	Feb	16	2016	7	3053	0	0	0	0	146	1269	0
48	Feb	17	2016	0	3080	0	0	0	142	154	1457	0
49	Feb	18	2016	3	2944	0	0	0	132	135		0
	Feb	19	2016	4	2882	0	0	0	37	125	1253	0
	Feb	20	2016	2	2869	0	0	0	99-	132	1071	0
52	Feb	21	2016	က	2837	0	0	0	299-	129	533	0
53	Feb	22	2016	3	2971	0	0	0	194-	119	490	0
54	Feb	23	2016	7	3119	0	0	0	-987	144	115	0
22	Feb	24	2016	18	3153	0	0	0	7 1-	165	698	15
26	Feb	52	2016	2	3180	0	0	0	-208	147	1071	0
22	Feb	56	2016	18	3122	0	0	0	692-	180	45	14
28	Feb	27	2016	0	2995	0	0	-26	262	144	1407	0
29	Feb	28	2016	4	2906	0	0	-20	420	135	1167	0
09	Feb	53	2016	2	2914	0	0	0	283	140	1320	0

Exhibit No. SPS-0005_2016 Loss Study-FINAL.xlsx App. D - System Load Data

	¥	В	С	٥	В	F	ŋ	I	-	٦	¥	٦	Σ
10					Hr @	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	# bes	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	SWPP	TaT	MIND	SOLAR
12											TIE FLOW		
73	61	Mar	T	2016	က	2893	0	0	-24	29	127	1164	0
74	62	Mar	2	2016	0	3046	0	0	0	-91	150	089	0
75	63	Mar	3	2016	2	2956	0	0	-20	227	136	1068	0
9/	64	Mar	4	2016	က	3057	0	0	0	462	138	1480	0
77	92	Mar	2	2016	က	2983	0	0	0	-229	138	797	0
78	99	Mar	9	2016	4	2936	0	0	-114	257	124	1314	0
79	29	Mar	7	2016	3	2887	0	0	-49	-51	131	1155	0
80	89	Mar	8	2016	4	2954	0	0	0	-336	135	591	0
8	69	Mar	6	2016	2	2959	0	0	0		135		0
82	20	Mar	10	2016	က	3025	0	0	0	-300	143	230	0
83	71	Mar	11	2016	3	3076	0	0	0	-154	140	899	0
84	72	Mar	12	2016	0	3032	0	0	-63	34	139	1067	0
82	73	Mar	13	2016	4	2933	0	0	0	-254	122	572	0
98	74	Mar	14	2016	4	2884	0	0	0		128	985	0
87	75	Mar	15	2016	4	2942	0	0	0	-275	122	762	0
88	9/	Mar	16	2016	3	3001	0	0	0	-437		551	0
88	77	Mar	17	2016	4	3057	0	0	0	-617	129	269	0
90	78	Mar	18	2016	4	3070	0	0	0	260	130	1381	0
91	79	Mar	19	2016	19	3187	0	0	0		158	352	17
92	80	Mar	20	2016	18	3109	0	0	0	-79	165	293	32
93	81	Mar	21	2016	3	3137	0	0	0	228	143	`	0
94	82	Mar	22	2016	3	3022	0	0	-124	503			0
92	83	Mar	23	2016	4	3017	0	0	-37	98	129	1322	0
96	84	Mar	24	2016	2	3167	0	0	0	8	150	1228	0
97	82	Mar	25	2016	က	3204	0	0	0	259	146	1375	0
86	98	Mar	56	2016	3	3097	0	0	0	227	134	1087	0
66	87	Mar	27	2016	17	3070	0	0	81	42	151	41	34
100	88	Mar	28	2016	2	3079	0	0	0	73	139	1448	0
101	88	Mar	53	2016	4	3049	0	0	-100	26	124	1282	0
102		Mar	30	2016	4	3078	0	0	-86	51	134	1162	0
103	9	Mar	31	2016	3	3138	0	0	-20	136	133	1235	0

Exhibit No. SPS-0005_2016 Loss Study-FINAL.xlsx App. D - System Load Data

Π_	با م		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0 0	000	000	0000	00000	00000
≥ F	SOLAR																																
TOTAL	WIND		593	1091	1419	424	1416	1301	1228	869	1047	1372	942	53	573	1283	1331	1273	1254	1223	247	73	265	368	1578			1318	1318 886	1318	1318 886 1125	1318 886 1125 1211	1318 886 1125 1211 728
¥ 10+		TIE FLOW	136	152	135	125	129	131	127	131	128	120	131	135	141	132	126	131	123	132	135	132	134	134	131	120	120	001	135	135	135	138	136 138 130 130
\ TOT			-513	-188	112	-158	291	-20	385	-18	-32	36	-92	-619	-299	190	212	419	157	411	-232	-275	-453	-79	278	145	145		238	238	238	238 85 219	238 85 219 -307
_ TOT	LAMAR		0	0	68-	0	-26	0	0	0	0	-101	-26	0	0	-26	-20	0	0	0	0	0	0	0	-20	-50	-20	•	0	0	0	0 0	0 0 0
± 10±			0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	<u> </u>	•	>	0	000	000
9 TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	39	42	41	41	0			0	0	0 0
Min Cyc			3202.00	3274.00	3186.00	3016.00	3080.00	3100.00	3133.00	3151.00	3155.00	3118.00	3039.00	3199.00	3216.00	3076.00	3033.00	2971.00	2941.00	2981.00	3033.00	2972.00	2940.00	2957.00	2982.00	2971.00	2971.00	2932.00			3064.00	3064.00	3064.00 3023.00 3051.00
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Δ	Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016			2016	2016	2016 2016 2016
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В	Month		Apr			Apr	Apr	Apr Apr Apr																									
∢	Sed #	-	92	93	94	92	96	26	86	66	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	115	116		!	117	117	118
Ş	1	12	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	127	128			129	129 130	129 130

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Σ	TOTAL	SOLAR)			1)					,		1						,		11))
Γ	TOTAL	MIND		124	181	26	332	38	593	614	1100	1329	792	1071	806	902	297	1348	1526	1351	748	267	1075	1254	1625	471	727	1245	151	339	415	906	462
¥	TOTAL		TIE FLOW	141	135	139	142	141	149	156	153	160	165	167	155	186	154	208	168	206	206	190	181	178	182	200	190	156	185	176	175	170	190
ſ	TOTAL .	SWPP		-409	-481	-269	-444	-655	-232	-144	348	538	41	-226	267	237	-765	-38	314	-183	-164	-394	-334	-234	177	-398	-227	-297	-351	-247	-332	-20	-764
-	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-92	0	0	0	0	0
I	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	TOTAL	EDDY		0	0	0	0	0	0	52	20	20	20	09	0	0	40	40	40	40	39	40	40	40	40	40	40	40	0	0	0	0	40
F	Min Sys	Net Load EDDY		2881.00	2804.00	2860.00	2904.00	2858.00	2954.00	3085.00	3122.00	3246.00	3146.00	3323.00	3145.00	3360.00	3342.00	3500.00	3370.00	3634.00	3643.00	3622.00	3583.00	3661.00	3805.00	3872.00	3865.00	3833.00	3719.00	3615.00	3748.00	3806.00	3854.00
Э	Hr @	Min		5	5	4	5	8	5	5	5	5	5	7	8	5	5	5	2	9	8	8	5	2	2	9	2	7	8	5	2	2	5
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		1	7	3	4	2	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	22	56	27	28	58	30
В		Month		Jun	lun	Jun	Jun																										
A		# bəs		153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182
	10	11	12	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194

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L	TOTAL	WIND		708	989	373	286	641	1215	1562	1147	1035	1283	1421	800	1481	1117	314	564	1523	1324	984	1505	1504	1318	1332	762	26	291	401	291	950	430	1204
¥	LAL		TIE FLOW	182	176	186	167	220	194	170	206	159	175	209	221	228	215	178	172	186	187	195	198	205	202	193	191	212	198	145	183	193	188	188
٦		SWPP		-304	-688	-169	-479	-627	91	-184	-589	72	-20	-124	-659	-83	-549	-547	-443	178	-299	-189	-20	-20	-53	244	-119	-956	-1129	-1172	-1339	-559	-526	-103
_		LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	74	0	0	0
I		BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-16	-17	13	-16	91-	-16	-23	-25	-107
Э	TOTAL	EDDY		40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	49	0	0	40	40	40	40	40	40	40	40	40	0	20	0
F	Min Sys	Net Load		3789.00	3834.00	3738.00	3701.00	3934.00	3997.00	4054.00	4220.00	3958.00	4091.00	4245.00	4309.00	4366.00	4373.00	4061.00	3881.00	4035.00	4085.00	4168.00	4226.00	4325.00	4299.00	4207.00	4172.00	4223.00	4209.00	4197.00	4100.00	4217.00	4032.00	4066.00
Е	Hr @	Min		5	9	8	7	9	9	2	2	8	8	5	9	9	9	5	7	∞	5	9	5	9	9	∞	8	9	5	2	5	5	8	8
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		T	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	53	30	31
В		Month		Jul	Jul	Jul	Ju	Jul	Jul	Jul	Jul	Jul	Ju	Inf	Inf	Jul	Ju	Inf	Ju	Jul	Inf	Jul	Jul	Jul	Inf	Ju	Ju	Jul	Inf	Jul	Inf	Jul	Ju	Jul
Α		Seq#		183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213
	10	11	12	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225

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10					Hr @	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	Sed #	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	SWPP	LPL	MIND	SOLAR
12											TIE FLOW		
226	214	Aug	1	2016	5	4145.00	0		0	-146	202	1401	7
227	215	Aug	2	2016	5	4275.00	40	-21	0	-1099	208	220	7
228	216	Aug	3	2016	5	4098.00	45	-91	0	-1018	207	192	7
529	217	Aug	4	2016	5	4229.00	0	-21	0	-571	205	1258	0
230	218	Aug	2	2016	5	4220.00	0		0	-564		218	0
231	219	Aug	9	2016	8	4165.00	0	-16	0	-588	200	251	21
232	220	Aug	7	2016	8	4106.00	0	-20	0	-771	191	355	21
233	221	Aug	∞	2016	5	4096.00	0		0	-956	205	617	0
234	222	Aug	6	2016	5	3994.00	40	14	0	-746		739	0
235	223	Aug	10	2016	5	4030.00	40	-94	0	-151	194	1229	0
236	224	Aug	11	2016	5	4096.00	40	-182	0		196	822	0
237	225	Aug	12	2016	5	3967.00	40	-21	0	-828	202	149	0
238	226	Aug	13	2016	9	3787.00	40		0	-734	148	149	0
239	227	Aug	14	2016	8	3704.00	40	-21	0	-553	157	62	_
240	228	Aug	15	2016	5	3683.00	40	14	0	-195	158	589	0
241	229	Aug	16	2016	5	3869.00	40	14	0	-317	168	1188	0
242	230	Aug	17	2016	2	3911.00	40	14	0	-543	165	815	0
243	231	Aug	18	2016	2	3999.00	40	-21	0	969-		899	0
244	232	Aug	19	2016	5	4024.00	40	-16	0	006-		316	0
245	233	Aug	70	2016	5	3867.00	0	-20	0	-532	180	1011	0
246	234	Aug	21	2016	8	3646.00	0	13	0	-818	151	299	2
247	235	Aug	22	2016	5	3616.00	0	14	0	-258	158	1097	0
248	236	Aug	23	2016	2	3850.00	40	14	0	9	175	1392	0
249	237	Aug	24	2016	5	3675.00	75	-16	0	-348	171	1095	0
250	238	Aug	52	2016	2	3552.00	92	-20	0	-646	168	110	0
251	239	Aug	56	2016	2	3426.00	0	-21	0	-219	158	250	0
252	240	Aug	22	2016	2	3393.00	0	15	0	-114	155	1103	0
253	241	Aug	28	2016	9	3284.00	0	14	0	-145	162	460	0
254	242	Aug	53	2016	2	3157.00	0	14	0	-105	166	193	0
255	243	Aug	30	2016	5	3086.00	0		0	-205	159	24	0
256	244	Aug	31	2016	5	2977.00	0	-21	0	-167	•		0

Exhibit No. SPS-0005_2016 Loss Study-FINAL.xlsx App. D - System Load Data

	Α	В	၁	Q	3	Ь	9	I	-	ſ	X	٦	Σ
10					Hr @	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	# beS	Month	Day	Year	Min	Net Load EDDY	EDDY	BLKW	LAMAR	SWPP	LPL	MIND	SOLAR
12											TIE FLOW		
257	245	Sep	1	2016	4	2918.00	0	08-	0	-220	155	98	0
258	246	Sep	7	2016	4	2962.00	0	14	0	-544	160	377	0
259	247	Sep	3	2016	5	3034.00	0	108	0	-366	159	1027	0
260	248	Sep	4	2016	9	3028.00	0	114	-20	-118	165	1043	0
261	249	Sep	2	2016	5	3017.00	0	19	-9	-33	162	1251	0
262	250	Sep	9	2016	5	3036.00	0	191	0	-147	173	1140	0
263	251	Sep	7	2016	5	3047.00	0	-16	7	29	173	1000	0
264	252	Sep	∞	2016	5	3078.00	0	14	0	-516	179	860	0
265	253	Sep	6	2016	5	3062.00	0	64	-49	199-	175	651	0
266	254	Sep	10	2016	9	2921.00	0	161	-124	-671	161	878	0
267	255	Sep	11	2016	5	2838.00	0	155	-129	-232	139	1176	0
268	256	Sep	12	2016	4	2933.00	0	180	-183	-273	154	1298	0
269	257	Sep	13	2016	5	2979.00	0	29	-106	-639	162	443	0
270	258	Sep	14	2016	4	2952.00	0	-16	0	-544	163	149	0
271	259	Sep	15	2016	4	2980.00	0	180	0	-516	160	813	0
272	260	Sep	16	2016	2	2776.00	0	27	0	-461	130	262	0
273	261	Sep	17	2016	5	2840.00	0	-16	0	-433	150	152	0
274	262	Sep	18	2016	5	2825.00	0	170	0	-431	147	1089	0
275	263	Sep	19	2016	5	2882.00	0	180	-39	-671	168	832	0
276	264	Sep	70	2016	5	2981.00	0	-16	66-	-82	171	928	4
277	265	Sep	21	2016	2	3049.00	0	06	-110	-239	168	1072	4
278	566	Sep	22	2016	5	3008.00	0	-16	69-	-181	168	696	0
279	267	Sep	23	2016	5	3000.00	0	-16	0	-105	162	1153	0
280	268	Sep	24	2016	9	3061.00	0	-13	0	096-	173	369	0
281	569	Sep	25	2016	5	2915.00	0	08-	32		152	341	0
282	270	Sep	56	2016	4	2763.00	0	-16	0	-737	133	208	0
283	271	Sep	27	2016	4	2867.00	0	-60	0	-23	132	562	0
284		Sep	28	2016	5	2885.00	0	-16	0	-209	137	492	0
285		Sep	29	2016	5	2931.00	0	-71	0	1			0
286	274	Sep	30	2016	5	2966.00	0	-16	0	-92	138	1051	0

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	Y	В	၁	Q	Е	F	9	Н	-	ſ	У	٦	Σ
10					@ JH	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	# bəS	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	SWPP	Tbr	QNIM	SOLAR
12											TIE FLOW		
318	306	Nov	1	2016	4	2995.00	0	0	0	-123	143	852	0
319	307	Nov	7	2016	4	3009.00	0	0	0	-453	144	458	0
320	308	Nov	3	2016	3	2872.00	0	0	0	06-	136	295	0
321	309	Nov	4	2016	5	2959.00	0	0	0	-159	140	49	0
322	310	Nov	2	2016	5	2936.00	0	0	0	98-	134	431	0
323	311	Nov	9	2016	4	2802.00	0	0	0	-260	129	288	0
324	312	Nov	7	2016	3	2788.00	0	0	0	159	136	318	0
325	313	Nov	∞	2016	3	2860.00	0	0	0	133	135	945	0
326	314	Nov	6	2016	3	2965.00	0	0	0	-204	144	185	0
327	315	Nov	10	2016	4	3023.00	0	0	0	-175	143	842	0
328	316	Nov	11	2016	3	2990.00	0	0	0	-160	141	752	0
329	317	Nov	12	2016	3	3001.00	0	0	0	-552	143	115	0
330	318	Nov	13	2016	0	2999.00	0	0	0	-210	153	282	0
331	319	Nov	14	2016	3	2893.00	0	0	0	-197	136	482	0
332	320	Nov	15	2016	3	2949.00	0	0	0	-211	138	141	0
333	321	Nov	16	2016	4	2941.00	0	0	0		133	1225	0
334	322	Nov	17	2016	3	2926.00	0	0	0	278	135	1407	0
335	323	Nov	18	2016	3	3026.00	0	0	0	-115	140	1021	0
336	324	Nov	19	2016	17	3249.00	0	0	0	320	177	1573	89
337	325	Nov	20	2016	0	3056.00	0	0	0	166	159	069	0
338	326	Nov	21	2016	2	2980.00	0	0	0	39	148	999	0
339	327	Nov	22	2016	3	3040.00	0	0	0	159	140	1422	0
340	328	Nov	23	2016	33	3162.00	0	0	0	-13	151	1108	0
341	329	Nov	25	2016	17	3023.00	0	0	0	43	146	1231	35
342	330	Nov	25	2016	33	3071.00	0	0	0	-351	124	673	0
343	331	Nov	56	2016	4	3138.00	0	0	0	-113	149	806	0
344	332	Nov	27	2016	5	3008.00	0	0	0	230	134	1418	0
345		Nov	28	2016	3	3033.00	0	0	0	78		1349	0
346		Nov	29	2016	3	3171.00	0	0	0		_	_	0
347	335	Nov	30	2016	16	3328.00	0	0	0	-344	199	765	172

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10					H @	Min Sys	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL
11	# bes	Month	Day	Year	Min	Net Load	EDDY	BLKW	LAMAR	SWPP	LPL	MIND	SOLAR
12											TIE FLOW		
348	336	Dec	1	2016	16	3296.00	0	0	0	-116	199	29	150
349	337	Dec	2	2016	2	3278.00	0	0	0	-102	179	167	0
350	338	Dec	3	2016	4	3289.00	0	0	0	-519	175	415	0
351	339	Dec	4	2016	16	3190.00	0	0	0	-227	186	28	158
352	340	Dec	2	2016	17	3289.00	0	0	0	-255	141	938	27
353	341	Dec	9	2016	2	3273.00	0	0	0	-220	173	1161	0
354	342	Dec	7	2016	3	3516.00	0	0	0	-85	202	1330	0
322	343	Dec	∞	2016	2	3614.00	0	0	0	-339	223	111	0
356	344	Dec	6	2016	17	3633.00	0	0	0	165	240	752	58
357	345	Dec	10	2016	17	3276.00	0	0	0	207	192	1331	13
358	346	Dec	11	2016	17	3253.00	0	0	0	·	185	029	25
329	347	Dec	12	2016	2	3274.00	0	0	0	-48	138	423	0
360	348	Dec	13	2016	3	3239.00	0	0	0	ſ	167	299	0
361	349	Dec	14	2016	3	3435.00	0	0	0	276	161	1086	0
362	320	Dec	15	2016	Н	3540.00	0	0	0	-32	165	377	0
363	351	Dec	16	2016	0	3291.00	0	0	0	519	173	1577	0
364	352	Dec	17	2016	3	3175.00	0	0	0	459	157	1534	0
365	353	Dec	18	2016	16	3409.00	0	0	0		197	349	72
366	354	Dec	19	2016	16	3436.00	0	0	0	24	231	1166	143
367	355	Dec	20	2016	17	3263.00	0	0	0	-267	201	23	29
368	326	Dec	21	2016	3	3341.00	0	0	0	-454	186	1252	0
369	357	Dec	22	2016	3	3310.00	0	0	0	906-	182	928	0
370	358	Dec	23	2016	17	3174.00	0	0	0	-242	177	282	63
371	329	Dec	24	2016	16	3036.00	0	0	0		191	1414	47
372	360	Dec	22	2016	2	2860.00	0	0	0	217	134	1521	0
373	361	Dec	56	2016	16	3113.00	0	0	0	-393	168	320	147
374	362	Dec	27	2016	2	3244.00	0	0	0	-635	175	734	0
375	363	Dec	28	2016	3	3202.00	0	0	0	-48	159	1488	0
376	364	Dec	53	2016	3	3274.00	0	0	0	-278	151	1115	0
377		Dec	30	2016	3	3476.00	0	0	0		186	1618	0
378	366	Dec	31	2016	17	3256.00	0	0	0		178	7 7	21

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AE	%	Error		-0.32%	-2.20%	-3.88%	3.12%	6.62%	4.00%	2.63%	2.54%	5.72%	7.24%	8.04%	6.36%	2.08%	3.88%	3.26%	0.07%	2.60%	7.52%	3.49%	3.57%	1.84%	4.73%	0.01%	-4.18%	-1.32%	1.49%	5.28%	2.33%	-0.36%	-6.89%	-9.05%
AD	Study	Value		3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7
AC	Average	Load		3369	3306	3249	3485	3604	3515	3469	3466	3573	3625	3652	3595	3552	3511	3490	3382	3468	3634	3498	3501	3442	3540	3380	3239	3335	3430	3558	3459	3368	3147	3074
AB	Total	Max		3494	3481	3491	3735	3847	3707	3697	3691	3724	3780	3963	3926	3879	3812	3749	3559	3641	3880	3729	3766	3703	3872	3638	3411	3612	3669	3900	3774	3622	3297	3235
AA																																		
\	TOTAL	SOLAR		0	0	0	3	3	3	3	3	16	3	3	3	3	3	0	28	0	11	0	0	0	0	13	26	0	0	0	0	0	0	7
×	TOTAL	WIND		474	82	396	301	1512	968	783	504	339	278	160	515	785	1202	185	82	96	172	1254	1439	1462	157	1128	1227	1294	272	545	150	1116	1184	791
W	TOTAL	LPL	TIE FLOW	224	242	206	235	220	206	196	213	220	235	242	232	225	215	246	229	228	230	224	221	208	236	204	206	228	215	242	248	223	181	198
^	TOTAL	SWPP		-373	-431	-441	-124	-104	-557	-244	-673	-899	-859	999-	-512	-322	-252	-738	-472	-447	-35	263	244	603	-516	-53	-181	-18	-556	-256	-723	-161	-24	-18
n	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Τ	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
R	Max Sys	Net Load		3494	3481	3491	3735	3847	3707	3697	3691	3724	3780	3963	3926	3879	3812	3749	3228	3641	3880	3729	3766	3703	3872	3638	3411	3612	3669	3900	3774	3622	3297	3235
Ö	Hr @	Мах		20	21	8	8	20	8	8	19	10	21	8	8	8	8	8	11	21	10	8	8	8	8	6	10	8	8	8	8	8	8	21
Ь	Total	Min		3244	3130	3006	3235	3360	3323	3240	3240	3422	3469	3340	3263	3224	3210	3231	3205	3294	3388	3266	3235	3181	3207	3122	3066	3058	3191	3216	3143	3113	2997	2913
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		1	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31
В		Month		Jan																														
Α		Sed#		_	7	က	4	2	9	7	80	6	10	7	12	13	4	15	16	17	18	19	20	21	22	23	24	22	26	27	28	59	30	31
	10	1	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	8	35	36	37	38	39	40	41	42	43

AF																																
ΑE	%	Error		-3.13%	3.75%	%98.9	6.19%	5.31%	-0.97%	-4.18%	7.35%	2.41%	0.11%	-2.98%	-1.81%	-4.33%	%29'2-	-3.84%	-5.62%	-1.80%	-6.19%	-8.41%	-9.89%	%59'6-	-4.92%	0.79%	2.17%	0.72%	0.91%	-6.40%	-9.58%	-6.40%
AD	Study	Value		3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7	3379.7
AC	Average	Load		3274	3507	3612	3589	3228	3347	3239	3459	3461	3384	3279	3319	3234	3121	3250	3291	3319	3171	3096	3046	3054	3214	3407	3453	3404	3411	3164	3056	3164
AB	Total	Max		3568	3741	3889	3938	3789	3654	3408	3761	3759	3677	3542	3570	3418	3266	3480	3529	3558	3397	3309	3222	3270	3456	3694	3753	3628	3699	3332	3206	3413
AA																																
\	TOTAL	SOLAR		0	7	0	0	0	1	19	0	1	1	1	1	27	15	2	2	3	2	0	0	0	0	0	9	5	9	9	0	9
×	TOTAL	WIND		1265	1507	341	852	920	216	857	626	950	1318	443	746	1296	624	356	950	1045	1608	953	478	445	472	1159	835	522	1522	1311	343	1375
W	TOTAL	LPL	TIE FLOW	227	240	268	234	229	211	176	226	245	226	214	223	193	176	218	208	206	187	199	199	176	197	219	214	205	206	183	194	195
>	TOTAL T	SWPP		259	140	-448	127	40	-451	-382	-75	-117	561	6-	-61	620	24	-770	-665	-532	09	-308	-220	-420	-381	-279	-334	-626	-11	-16	-53	339
n	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
⊢	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ĸ	Max Sys	Net Load		3568	3741	3889	3938	3789	3654	3408	3761	3759	3677	3542	3570	3418	3266	3480	3529	3228	3397	3309	3222	3270	3456	3694	3753	3628	3699	3332	3206	3413
Ø	Hr @	Мах		8	8	80	8	8	8	6	8	8	8	8	8	6	10	8	8	8	8	20	20	20	20	20	8	80	ω	8	20	8
Д	Total	Min		2980	3272	3334	3240	3329	3040	3069	3157	3163	3090	3016	3067	3049	2975	3020	3053	3080	2944	2882	2869	2837	2971	3119	3153	3180	3122	2995	2906	2914
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		П	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	22	56	27	28	59
В		Month		Feb																												
٧		Sed#		32	33	34	32	36	37	38	39	40	41	42	43	44	45	46	47	48	49	20	21	25	53	24	22	26	22	28	29	09
	10	7	12	4	45	46	47	48	49	20	51	52	53	54	22	99	22	28	29	09	61	62	63	64	65	99	29	89	69	70	71	72

AF																																		
AE	%	Error		-5.94%	-1.67%	-4.69%	-1.98%	-6.24%	-6.63%	-5.76%	-4.78%	-4.77%	-3.08%	-1.49%	-5.35%	-7.19%	-5.53%	-4.77%	-3.46%	-2.25%	-0.07%	0.85%	-2.55%	2.30%	-1.49%	-2.58%	2.17%	1.72%	-2.48%	-2.74%	-0.46%	-0.15%	-0.31%	1.24%
AD	Study	Value		3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4
AC	Average	Load		3126	3268	3168	3258	3116	3103	3132	3165	3165	3221	3274	3146	3085	3140	3165	3209	3249	3321	3352	3239	3400	3274	3238	3396	3381	3241	3233	3308	3319	3313	3365
AB	Total	Max		3359	3490	3379	3458	3249	3270	3377	3375	3371	3417	3472	3259	3236	3395	3388	3416	3440	3572	3516	3368	3663	3493	3458	3624	3557	3385	3395	3537	3588	3548	3591
AA																																		
>	TOTAL	SOLAR		7	3	0	2	0	0	0	0	0	6	13	43	0	0	0	13	6	32	33	15	0	0	0	0	21	34	34	0	0	45	~
×	TOTAL	WIND		1193	1522	287	1462	1347	1387	666	379	294	206	116	1047	367	1601	269	919	91	1361	236	45	1578	1408	1278	855	1117	915	334	1491	1618	1316	612
Μ	TOTAL	۱ Tbr	TIE FLOW	188	199	201	190	181	195	206	206	202	189	190	171	187	196	135	168	174	179	190	169	205	190	189	212	189	169	175	189	209	214	182
>	TOTAL T	SWPP L		121	338	340	336	157	37	-218	-78	-310	-163	-306	374	152	223	-183	174	-84	-146	-875	-420	75	456	-273	-243	63	96	-63	6	343	151	-382
О	TOTAL	LAMAR		0	0	0	0	-55	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
_	TOTAL	BLKW		0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	43 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0
S	TOTAL	EDDY					(
ĸ	Max Sys	Net Load		3359	3490	3379	3458	3249	3270	3377	3375	3371	3417	3472	3259	3236	3335	3388	3416	3440	3572	3516	3368	3663	3493	3458	3624	3557	3385	3395	3537	3588	3548	3591
Ø	Hr @	Max		8	80	19	8	20	20	20	20	21	8	80	11	21	21	21	6	6	12	11	6	8	8	22	∞	10	10	10	8	21	17	8
Ь	Total	Min		2893	3046	2956	3057	2983	2936		2954	2959	3025		3032	2933	2884	2942	3001	3057	3070	3187	3109	3137	3022	3017	3167	3204	3097	3070	3079	3049	3078	3138
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	2	3	4	2	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
В		Month		Mar																														
٧	-	# bes			62	93		. 65		29	89	69		71	72	73	74		92	77		79			85		84		98			1 89		91
	10	11	12	73	74	75	9/	77	78	79	80	81	82	83	84	85	98	87	88	88	90	91	92	93	94	92	96	97	86	66	100	101	102	103

П																																	
AF																																	
AE	%	Error		3.48%	3.84%	-0.58%	0.09%	1.72%	1.27%	1.24%	0.89%	0.48%	0.41%	0.15%	2.80%	1.90%	0.44%	-1.86%	-4.71%	-5.35%	-3.34%	-2.87%	-3.01%	-3.20%	-1.10%	-1.43%	-0.57%	3.09%	1.15%	0.94%	2.40%	%09:0-	-3.83%
AD	Study	Value		3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4
AC	Average	Load		3439	3451	3304	3327	3381	3366	3365	3353	3340	3337	3329	3417	3387	3338	3262	3167	3146	3213	3228	3224	3217	3287	3276	3305	3426	3362	3355	3403	3304	3196
AB	Total	Max		3676	3628	3422	3637	3681	3631	3596	3555	3524	3556	3618	3634	3557	3600	3490	3363	3350	3444	3423	3475	3494	3617	3570	3638	3920	3659	3686	3755	3531	3374
AA																																	
>	TOTAL	SOLAR		2	1	0	0	18	26	0	6	39	0	0	0	0	43	42	44	0	0	19	40	40	39	34	31	41	38	14	41	35	35
×	TOTAL	WIND		809	339	397	1142	1541	226	554	493	1235	879	439	619	911	1185	1413	1125	206	554	44	349	212	545	1559	1127	1001	885	176	1377	450	434
M	TOTAL		TIE FLOW	197	185	183	221	216	213	200	185	183	215	200	192	194	214	185	214	188	189	190	215	219	235	224	246	271	238	239	242	228	202
>	TOTAL	SWPP		-343	-548	-481	248	-104	-737	-128	109	-57	-304	-352	-292	156	181	292	159	18	193	289	429	-320	406	187	227	256	647	-200	920	31	112
n		LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	-26	0	0	0	0	0	0	0	-	0	0	0	0	0	0	0	0
⊥	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	41	42	-41	0	0	0	0	0	0
ĸ	Max Sys	Net Load		3676.00	3628.00	3422.00	3637.00	3681.00	3631.00	3596.00	3555.00	3524.00	3556.00	3618.00	3634.00	3557.00	3600.00	3490.00	3363.00	3350.00	3444.00	3423.00	3475.00	3494.00	3617.00	3570.00	3638.00	3920.00	3659.00	3686.00	3755.00	3531.00	3374.00
Ø	Hr @	Мах		11	8	22	21	19	18	21	11	18	21	21	22	22	17	16	17	22	22	12	18	18	18	18	19	18	15	18	18	17	18
Ь	Total	Min		3202	3274	3186	3016	3080	3100	3133	3151	3155	3118	3039	3199	3216	3076	3033	2971	2941	2981	3033	2972	2940	2957	2982	2971	2932	3064	3023	3051	3076	3018
۵		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		1	2	8	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	70	21	22	23	24	25	56	27	28	59	30
В		Month		Apr																													
Α		Sed#		95	93	94	92	96	97	86	66	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121
	10	7	12	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133

AF																																		
AE	%	Error		-3.44%	-2.74%	-3.95%	-0.13%	4.25%	5.61%	7.28%	3.28%	4.19%	11.86%	11.78%	7.33%	12.20%	-0.78%	-4.19%	1.03%	-3.80%	-6.42%	-8.42%	-5.01%	-0.93%	0.38%	2.60%	9.48%	11.11%	12.01%	6.38%	7.51%	2.83%	0.89%	1.24%
AD	Study	Value		3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4	3323.4
AC	Average	Load		3209	3233	3192	3319	3465	3510	9958	3433	3463	3718	3715	3567	3729	3298	3184	3358	3197	3110	3044	3157	3293	3336	3510	3639	3693	3723	3536	3573	3418	3353	3365
AB	Total	Max		3430	3419	3392	3691	3943	3940	4001	3786	3882	4313	4194	3947	4232	3436	3388	3736	3384	3283	3210	3497	3718	3795	4159	4222	4327	4300	3970	4069	3756	3831	3790
AA																																		
Υ	TOTAL	SOLAR		0	2	36	32	39	33	34	32	33	40	17	26	40	0	0	26	9	4	11	31	37	35	36	20	37	33	38	38	15	11	28
×	TOTAL	WIND		467	37	931	4-	444	1614	1560	1521	473	1173	238	95	452	1099	902	1051	1350	173	303	1148	1488	1229	457	1031	1022	1568	734	118	1145	772	189
W	TOTAL	LPL	TIE FLOW	183	194	191	240	282	256	278	260	254	298	304	251	299	170	183	264	189	193	190	211	262	288	310	324	332	302	265	284	268	275	269
>	TOTAL	SWPP		333	324	172	-19	216	482	347	245	-3	702	-41	371	-428	-75	127	484	129	-30	-182	308	162	121	-432	-42	614	153	51	232	209	207	-83
n	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	-110	0	0	0	0	0	0	0	-126	0	0	0	0	0	26	0	0	0
	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ĸ	Max Sys	Net Load		3430.00	3419.00	3392.00	3691.00	3943.00	3940.00	4001.00	3786.00	3882.00	4313.00	4194.00	3947.00	4232.00	3436.00	3388.00	3736.00	3384.00	3283.00	3210.00	3497.00	3718.00	3795.00	4159.00	4222.00	4327.00	4300.00	3970.00	4069.00	3756.00	3831.00	3790.00
Ø	Hr @	Мах		22	22	17	19	18	18	18	18	19	18	18	19	17	1	22	19	12	11	12	19	18	18	18	17	18	18	18	18	16	18	17
Ь	Total	Min		2988	3046	2992	2947	2986	3080	3130	3079	3043	3122	3236	3187	3226	3159	2980	2979	3010	2937	2877	2817	2867	2877	2860	3022	3058	3145	3101	3077	3079	2875	2939
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31
В		Month		May	Мау	May	Мау	May																										
Α		Sed#		122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152
Ī	10	1	12	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164

AF																																	
AE	%	Error		-29.45%	-28.78%	-23.87%	-24.14%	-22.61%	-18.28%	-15.75%	-14.02%	-11.23%	-12.57%	-12.45%	-13.88%	-7.68%	-7.81%	-3.47%	-4.72%	-0.13%	-2.44%	-6.14%	-2.94%	-1.01%	4.39%	4.42%	2.63%	0.92%	-5.95%	-2.52%	1.15%	2.77%	2.45%
AD.	Study	Value		4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1
AC	Average	Load		3127	3157	3374	3362	3430	3622	3734	3811	3935	3875	3881	3817	4092	4086	4279	4223	4427	4324	4160	4302	4388	4627	4628	4549	4473	4169	4321	4483	4555	4541
AD	Total	Max		3373	3209	3888	3820	4002	4290	4383	4499	4623	4604	4438	4489	4823	4830	2002	5076	5219	2002	4698	5021	5114	5448	5384	5232	5113	4618	5026	5218	5304	5227
AA																																	
Υ	TOTAL	SOLAR		31	18	37	17	36	20	41	39	40	38	22	30	22	30	13	32	31	29	24	29	25	29	32	30	30	27	18	39	35	48
<	TOTAL	WIND		482	314	104	484	75	285	1015	1416	1232	824	783	353	403	343	735	696	145	269	410	202	803	218	337	1315	1283	252	139	53	129	553
۸۸	TOTAL .	LPL	TIE FLOW	190	222	265	261	298	310	269	320	327	280	267	262	300	310	333	309	354	324	307	297	276	335	319	277	264	250	284	355	298	276
^	TOTAL	SWPP L		130	152	-160	-418	287	252	888	426	420	409	298	320	29	25	398	470	-293	-160	-300	-545	131	-393	28	362	19	623	94	-181	3	141
0	TOTAL	LAMAR		0	0	0	0	49	98	101	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	0	0	0	0
	TOTAL	BLKW		0 0	0 0	0 0	0 0	0	0	0	0	0 (0 (0	0 (0	0 (0 (0 (0 (0 (0	0 ,	0	0 (0	0	0 (0 (0	0	0	0
o	TOTAL	EDDY						0	51	40	20	90	92	0	0	40	40	40	40	40	40	40	47	81	40	70	70	40	0	0	0	40	40
¥	Max Sys	Net Load		3373.00	3509.00	3888.00	3820.00	4002.00	4290.00	4383.00	4499.00	4623.00	4604.00	4438.00	4489.00	4823.00	4830.00	5057.00	5076.00	5219.00	5005.00	4698.00	5021.00	5114.00	5448.00	5384.00	5232.00	5113.00	4618.00	5026.00	5218.00	5304.00	5227.00
3	Hr @	Мах		16	17	18	18	18	17	17	18	17	17	17	18	17	18	17	17	17	18	18	17	18	18	17	18	18	16	17	17	18	17
L	Total	Min		2881	2804	2860	2904	2858	2954	3085	3122	3246	3146	3323	3145	3360	3342	3500	3370	3634	3643	3622	3583	3661	3805	3872	3865	3833	3719	3615	3748	3806	3854
ם		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ر		ı Day		1	2	3	4	2	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Я		Month		Jun																													
A		Sed #		153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182
	10	11	12	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194

AF																																		
AE	%	Error		0.02%	-0.37%	-1.15%	1.28%	7.60%	8.80%	10.43%	2.55%	%69.9	8.58%	13.87%	15.36%	16.98%	14.45%	9.26%	4.81%	7.20%	9.87%	10.59%	12.50%	14.70%	14.07%	11.75%	10.97%	12.24%	11.10%	8.72%	10.00%	6.50%	6.25%	6.36%
AD	Study	Value		4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1
AC	Average	Load		4433	4416	4381	4489	4769	4822	4895	4678	4729	4813	5047	5113	5185	5073	4843	4646	4751	4870	4902	4986	5084	2056	4953	4919	4975	4924	4819	4876	4853	4709	4714
AB	Total	Max		2077	4997	5024	5277	5604	5647	5735	5136	5499	5534	5849	5917	6003	5772	5624	5410	5467	5654	5635	5746	5842	5812	2699	5665	5726	5639	5440	5651	5489	5386	5362
AA																																		
Υ	TOTAL	SOLAR		30	33	33	25	26	23	10	32	29	46	36	49	42	38	22	26	25	09	69	22	09	89	69	9/	28	24	78	09	88	88	27
×	TOTAL	WIND		1023	865	33	49	318	446	180	994	460	1043	1021	148	105	501	739	1241	1220	269	682	863	634	752	069	476	230	133	282	172	837	196	1265
Μ	TOTAL	LPL	TIE FLOW	276	292	284	309	326	328	348	277	294	295	345	322	367	333	305	328	303	302	338	337	385	307	320	310	339	324	363	310	325	311	327
>	TOTAL T	SWPP L		8	-199	-721	-349	-291	-498	-722	307	-25	208	149	-557	-654	-772	-181	-122	167	400	113	-20	-156	277	111	159	-81	-250	-30	-303	414	7	255
Ω	TOTAL	LAMAR		0	0	27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
⊥	TOTAL	BLKW		0 (0 (0	0 (0	0 (0	0 (0 (0 (0 (0 (0 (0 (0 (0	0 (0 (0 1	0 (0 (91-	91-	16	91-	3116	89	194	0 153	0 13	0 -24
S	TOTAL	EDDY		40	40	40	40	70	100	70	02	40	02	100	100	100	100	100	100	100	0	34	100	0	100	22	40	22	133	133	133			
ď	Max Sys	Net Load		5077.00	4997.00	5024.00	5277.00	5604.00	5647.00	5735.00	5136.00	5499.00	5534.00	5849.00	5917.00	6003.00	5772.00	5624.00	5410.00	5467.00	5654.00	5635.00	5746.00	5842.00	5812.00	2699.00	5665.00	5726.00	2639.00	5440.00	5651.00	5489.00	5386.00	5362.00
Ø	Hr @	Max		17	19	18	18	17	16	17	18	18	17	17	18	17	16	17	18	18	17	18	18	17	18	18	18	16	17	16	18	17	18	18
Ь	Total	Min		3789	3834	3738	3701	3934	3997	4054	4220	3958	4091	4245	4309	4366	4373	4061	3881	4035	4085	4168	4226	4325	4299	4207	4172	4223	4209	4197	4100	4217	4032	4066
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ن د		Day		1	2	33	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	53	30	31
В		Month		Jul	Jul	Jn	Jul	Jn	Jul	Jn	Jul	Jn	Jul	Inc	Jul	Jul	Jul	Jul	Jul	Jul	Inf													
٧		# bəs		183	184	185	186	187	188	189	190	191	192	193	194	195	196		198	199	500	201		503	204		3 206	207	208	209	210	211	212	213
	10	11	12	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225

AF																																		
AE	%	Error		11.11%	13.67%	9.53%	13.03%	11.65%	9.25%	7.43%	8.37%	5.14%	%26.9	8.30%	3.37%	-2.79%	-7.82%	%00:0	3.93%	4.19%	2.80%	5.81%	-6.68%	-9.37%	-4.99%	1.16%	-7.31%	%69.8-	-10.87%	-11.15%	-14.07%	-20.62%	-23.59%	-25.55%
AD	Study	Value		4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1	4432.1
AC	Average	Load		4925	5038	4855	5010	4949	4842	4762	4803	4660	4741	4800	4582	4309	4086	4432	4607	4618	4689	4690	4136	4017	4211	4484	4108	4047	3951	3938	3809	3518	3387	3300
AD	Total	Max		5704	5801	5611	2190	242	5519	5417	5510	5326	5452	5504	5196	4830	4467	5181	5344	5325	5379	5355	4405	4388	4806	5117	4541	4542	4475	4483	4333	3879	3687	3622
AA																																		
٨	TOTAL	SOLAR		43	95	93	105	106	52	107	9	35	78	20	69	17	25	88	93	98	92	40	61	53	36	27	83	25	4	86	81	74	43	22
×	TOTAL	MIND		993	238	818	749	224	651	407	683	298	675	258	786	326	130	186	174	263	183	160	41	289	1154	927	744	212	226	441	271	225	20	39
M	TOTAL	LPL	TIE FLOW	323	336	336	329	360	334	301	318	328	306	330	326	275	205	294	298	298	303	363	203	232	265	293	248	239	251	288	287	229	235	238
^	TOTAL	SWPP		72	210	400	-117	-352	-18	37	-43	98	-260	-93	101	-322	-177	-325	-307	-166	-191	-830	-627	-158	-201	-72	472	457	-36	299	154	489	946	425
O	TOTAL	LAMAR		0	0	0	0	0	0	0	0	174	0	100	0	0	0	0	0	0	0	0	26	0	0	0	26	51	0	0	76	0	0	C
-	TOTAL .	BLKW		-21	-32	14	13	14	-16	-21	-22	14	13	14	-22	-22	-14	54	-14	19	-22	-16	-21	13	14	14	-16	-21	-21	-41	-125	-46	-43	02-
n	TOTAL	EDDY		40	92	0	0	0	0	0	38	40	40	40	40	40	40	40	40	40	40	40	0	0	0	40	22	92	0	0	0	0	0	0
Y	Max Sys	Net Load		5704.00	5801.00	5611.00	5790.00	5677.00	5519.00	5417.00	5510.00	5326.00	5452.00	5504.00	5196.00	4830.00	4467.00	5181.00	5344.00	5325.00	5379.00	5355.00	4405.00	4388.00	4806.00	5117.00	4541.00	4542.00	4475.00	4483.00	4333.00	3879.00	3687.00	3622.00
3	@ JH	Мах		17	17	17	17	17	18	16	16	17	16	16	17	17	18	18	17	17	17	17	18	18	18	17	17	17	17	17	17	15	16	15
Ь	Total	Min		4145	4275	4098	4229	4220	4165	4106	4096	3994	4030	4096	3967	3787	3704	3683	3869	3911	3999	4054	3867	3646	3616	3850	3675	3552	3426	3393	3284	3157	3086	2427
D		/ Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ر		ر Day		1	2	æ	4	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31
מ		Month		Aug	Ang	Aug	Ang	Aug	Aug	Aug	Ang	Aug	Aug	Aug	Aug	Ang	Ang	Aug	Ang	Aug	Aug	Aug	Aug	Aug	Ang	Ang	Aug	Aug	Aug	Aug	Aug	Aug	Ang	Allø
¥		Sed#		5 214	7 215	3 216	9 217	218	1 219	220	3 221	4 222	5 223	5 224	7 225	3 226			1 229	2 230		4 232	5 233	3 234	7 235	3 236	9 237	238	1 239	2 240	3 241			244
	10	11	12	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256

П																																	
AF																																	
AE	%	Error		0.03%	1.89%	3.28%	3.61%	2.50%	7.25%	4.83%	9.22%	11.33%	-3.98%	-1.16%	4.90%	1.57%	-0.84%	0.59%	-4.20%	-4.22%	1.98%	%28.9	7.21%	7.05%	6.31%	2.66%	1.02%	-8.47%	-9.08%	-2.51%	0.89%	-1.87%	-1.87%
AD	Study	Value		3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9
AC	Average	Load		3388	3451	3498	3509	3573	3633	3551	3711	3771	3252	3348	3553	3440	3329	3407	3245	3244	3454	3620	3631	3626	3601	3579	3422	3100	3080	3302	3417	3324	3324
AB	Total	Max		3858	3940	3962	3990	4129	4229	4054	4344	4479	3583	3857	4173	3901	3765	3834	3713	3648	4083	4357	4281	4202	4193	4157	3782	3285	3396	3737	3949	3716	3681
AA																																	
>	TOTAL	SOLAR		88	96	36	66	88	16	71	101	88	91	78	43	102	28	18	98	53	87	87	96	33	94	107	105	0	14	126	122	126	146
×	TOTAL	WIND		144	395	1141	1388	1387	987	1110	385	99	70	106	524	133	400	704	108	999	157	172	549	1056	1038	1313	395	289	30	2	100	88	911
M	TOTAL		TIE FLOW	299	293	277	209	245	270	230	283	293	259	232	311	304	269	250	218	196	253	294	290	275	268	281	210	156	160	204	285	207	199
^	TOTAL	SWPP		-498	-143	-368	-133	-147	-488	-196	-597	-820	-106	-619	-387	-141	-40	-432	-130	161	153	367	-220	-127	-71	-173	-383	-511	-517	-414	-589	-231	63
n	TOTAL	LAMAR (0	0	-20	-50	-75	0	0	0	0	84	-119	0	26	119	0	25	22	114	103	-131	-191	0	0	0	0	0	0	0	0	0
Τ	TOTAL	BLKW		166	150	14	72	-30	-15	-30	-15	-16	-64	-16	26	-17	-48	-16	-16	-16	-29	-16	-16	06	96	-16	-16	33	-15	14	-16	-15	-16
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ĸ	Max Sys	Net Load		3858.00	3940.00	3962.00	3990.00	4129.00	4229.00	4054.00	4344.00	4479.00	3583.00	3857.00	4173.00	3901.00	3765.00	3834.00	3713.00	3648.00	4083.00	4357.00	4281.00	4202.00	4193.00	4157.00	3782.00	3285.00	3396.00	3737.00	3949.00	3716.00	3681.00
Ø	Hr @	Мах		18	17	17	17	18	17	18	17	17	18	18	17	17	17	18	18	18	18	17	17	17	17	17	18	21	18	18	18	17	17
Ь	Total	Min		2918	2962	3034	3028	3017	3036	3047	3078	3062	2921	2838	2933	2979	2952	2980	2776	2840	2825	2882	2981	3049	3008	3000	3061	2915	2763	2867	2885	2931	2966
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		1	7	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	22	56	27	28	29	30
В		Month		Sep																													
Α		Sed#		245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274
	10	7	12	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286

AF																																		
AE	%	Error		0.83%	2.20%	3.64%	3.27%	-0.16%	3.74%	-6.85%	-7.50%	-7.57%	-1.96%	2.97%	-4.22%	-7.78%	-5.12%	-0.38%	-0.48%	2.23%	-2.48%	-1.89%	-6.03%	-5.77%	-4.32%	-3.60%	-1.12%	0.22%	%89.0	0.92%	1.18%	1.73%	-3.38%	0.34%
AD	Study	Value		3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9
AC	Average	Load		3415	3462	3510	3498	3382	3514	3155	3133	3131	3321	3488	3244	3124	3214	3374	3371	3463	8088	3323	3183	3192	3241	3265	3349	3395	3410	3418	3427	3446	3273	6688
AB	Total	Max		3826	3946	4019	3909	3849	4026	3364	3322	3365	3814	4036	3490	3365	3527	3817	3876	4048	3697	3748	3446	3439	3549	3639	3806	3764	3816	3817	3829	3863	3571	3856
AA																																		
>	TOTAL	SOLAR		82	102	104	147	146	164	40	0	0	123	155	170	0	103	128	126	85	159	158	148	170	112	101	138	96	158	161	49	93	85	142
×	TOTAL	WIND		636	985	1593	810	615	206	41	099	1196	250	726	289	1065	1245	392	1286	1206	28	922	17	399	1011	228	172	777	256	617	1380	163	136	1226
W	TOTAL		TIE FLOW	222	283	224	220	191	237	143	143	167	213	247	176	199	225	224	273	222	228	275	170	203	216	207	225	238	198	258	257	250	199	264
^	TOTAL	SWPP		-279	28	-34	314	591	181	-483	-391	-243	-829	-349	-671	206	-106	-404	-191	-141	522	420	-262	-371	-561	30	234	-642	341	275	-141	-780	-138	-561
Ω	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
⊢	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	39	39	39	40	40	0	0	0	0	0	0	0	0	0	0
٣	Max Sys	Net Load		3826.00	3946.00	4019.00	3909.00	3849.00	4026.00	3364.00	3322.00	3365.00	3814.00	4036.00	3490.00	3365.00	3527.00	3817.00	3876.00	4048.00	3697.00	3748.00	3446.00	3439.00	3549.00	3639.00	3806.00	3764.00	3816.00	3817.00	3829.00	3863.00	3571.00	3856.00
Ø	H @	Мах		18	18	18	17	18	17	17	21	21	18	17	17	21	17	18	18	18	17	17	17	17	18	18	17	18	17	17	17	18	18	17
Ь	Total	Min		3004	2977	3001	3086	2914	3001	2946	2944	2896	2827	2939	2998	2882	2900	2931	2865	2877	2909	2898	2919	2944	2932	2891	2892	3025	3004	3019	3025	3028	2974	2941
О	_	Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	7	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31
В		Month		Oct	0ct	Oct																												
Α		%ed		275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305
	10	1	12	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317

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AF																																	
AE	%	Error		0.68%	-4.10%	-6.92%	-6.70%	-8.28%	-10.18%	-8.62%	-7.78%	-5.56%	-5.22%	-6.64%	-7.38%	-7.35%	-6.45%	-5.13%	-5.47%	-5.62%	-3.60%	0.03%	-5.30%	-4.10%	-3.52%	-1.41%	-5.65%	-4.60%	-3.35%	-5.36%	-1.72%	1.05%	5.48%
AD	Study	Value		3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9
AC	Average	Load		3410	3248	3153	3160	3107	3042	3095	3124	3199	3210	3162	3137	3138	3169	3213	3202	3197	3265	3388	3208	3248	3268	3339	3196	3231	3274	3206	3329	3423	3573
AB	Total	Max		3825	3487	3433	3361	3277	3282	3402	3387	3432	3397	3334	3273	3277	3444	3477	3462	3467	3504	3527	3359	3516	3495	3516	3368	3391	3409	3403	3624	3674	3817
AA																																	
\	TOTAL	SOLAR		147	0	0	2	0	0	0	0	0	0	19	0	0	0	0	0	0	150	153	153	0	0	147	118	0	0	0	0	0	2
×	TOTAL	WIND		113	482	99	173	1013	436	488	892	259	437	955	616	233	463	515	1383	1404	1067	721	983	1376	1374	218	493	856	1337	1347	1249	296	288
M	TOTAL	LPL	TIE FLOW	236	210	209	189	185	210	218	211	214	208	191	187	195	203	218	219	216	203	204	182	211	185	200	184	165	191	164	206	155	194
^	TOTAL TO	SWPP LI		10	82	40	-16	172	-205	819	117	304	-270	-233	109	-561	604	282	275	-298	-272	837	-289	-187	-240	-543	-304	16	-120	129	193	-747	-1023
n	TOTAL 1	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
⊥	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
æ	Max Sys	Net Load		3825.00	3487.00	3433.00	3361.00	3277.00	3282.00	3402.00	3387.00	3432.00	3397.00	3334.00	3273.00	3277.00	3444.00	3477.00	3462.00	3467.00	3504.00	3527.00	3359.00	3516.00	3495.00	3516.00	3368.00	3391.00	3409.00	3403.00	3624.00	3674.00	3817.00
Ø	Hr @	Мах		17	20	20	6	20	19	19	19	19	19	10	19	20	19	19	19	19	6	6	6	19	19	6	10	21	19	19	19	21	∞
Ь	Total	Min		2995	3009	2872	2959	2936	2802	2788		2962	3023	2990	3001	2999	2893	2949	2941	2926	3026	3249	3056	2980	3040	3162	3023	3071	3138	3008	3033	3171	3328
О		/ Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016		2016
၁		ر Day		1	2	3	4	5	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	25	25	26	27	28	29	30
В		Month		Nov																													
А	I =	Sed#			9 307	308	1 309	310	3 311	312	5 313	314	7 315	316	9 317	318	1 319			4 322	5 323	924	7 325	8 326	9 327	0 328	1 329	330		4 332	5 333		7 335
	10	11	12	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347

AF																																		
AE	%	Error		4.08%	3.50%	2.60%	0.18%	4.40%	2.57%	11.31%	14.26%	13.53%	4.54%	0.37%	4.90%	3.34%	8.20%	11.83%	4.42%	8.68%	8.43%	8.96%	4.58%	3.22%	4.51%	1.44%	-5.15%	-9.46%	-2.95%	2.01%	-0.13%	3.71%	7.38%	0.01%
AD	Study	Value		3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.9	3386.2
AC	Average	Load		3525	3506	3475	3393	3536	3226	3770	3870	3845	3541	3400	3553	3500	3665	3788	3537	3681	3673	3691	3542	3496	3540	3436	3213	3067	3287	3455	3383	3513	3637	3387
AB	Total	Max		3754	3733	3661	3596	3783	3878	4024	4126	4057	3805	3546	3832	3761	3894	4035	3782	4187	3936	3945	3821	3651	3769	3697	3389	3273	3461	3666	3563	3751	3798	3517
AA																																		
>	TOTAL	SOLAR		1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	3	0	0	0	5	17	0	0	0	64	66	0	21	131
×	TOTAL	WIND		375	808	74	1000	1399	1282	1229	135	1205	696	311	1364	1015	653	1281	1732	1015	168	069	826	1343	201	1449	450	1266	533	614	1111	1183	1564	1294
M	TOTAL	LPL	TIE FLOW	177	245	236	230	203	214	273	248	276	238	201	204	196	208	220	234	268	253	248	259	179	194	136	198	179	204	222	204	181	223	190
^	TOTAL	SWPP 1		-391	-238	-442	48	-236	-38	-419	-26	439	-374	-502	969	908	477	309	22	09	167	-199	-421	-128	-414	-344	-479	-307	-541	-418	-469	387	-631	-530
Ω	TOTAL	LAMAR		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
⊥	TOTAL	BLKW		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	TOTAL	EDDY		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ĸ	Max Sys	Net Load		3754.00	3733.00	3661.00	3596.00	3783.00	3878.00	4024.00	4126.00	4057.00	3805.00	3546.00	3832.00	3761.00	3894.00	4035.00	3782.00	4187.00	3936.00	3945.00	3821.00	3651.00	3769.00	3697.00	3389.00	3273.00	3461.00	3666.00	3563.00	3751.00	3798.00	3517.00
Ø	Hr @	Max		8	19	19	21	8	21	20	19	8	8	20	8	21	8	8	8	21	8	8	8	8	19	6	8	77	21	6	10	21	6	10
Ь	Total	Min		3296	3278	3289	3190	3289	3273	3516	3614	3633	3276	3253	3274	3239	3435	3540	3291	3175	3409	3436	3263	3341	3310	3174	3036	2860	3113	3244	3202	3274	3476	3256
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		n Day		1	2	3	4	2	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31
В		Month		Dec																														
Α		# bəs		336	337	338	339	340	341	342	343	344	345	346	347	348	349	320	351	352	353	354	355	356	357	358	329	360	361	362	363	364	365	366
	10	1	12	348	349	350	351	352	353	354	322	356	357	358	329	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378

5 5)	כ	ב	Š	Ę	7	3	ΥΥ	٩٢	ΑM	A
11						ЕРБУ СО	PNM	LAMAR	LPL	SWPP	MIND	SOLAR
=	% Sed	Month	Day	Year		Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
12												
13	1	Jan	1	2016		0	0	0	211	-313	288	1
14	2	Jan	2	2016		0	0	0	214	-495	63	7
15	က	Jan	3	2016		0	0	0	185	-384	215	7
16	4	Jan	4	2016		37	0	0	210	-233	215	8
17	2	Jan	2	2016		0	0	0	191	-151	1,306	3
18	9	Jan	9	2016		0	0	0	178	-279	1,182	ε
19	7	Jan	7	2016		0	0	0	170	-174	1,013	3
20	8	Jan	8	2016		0	0	0	176	069-	439	ε
21	6	Jan	6	2016		0	0	0	199	608-	401	10
22	10	Jan	10	2016		0	0	0	215	969-	316	ε
23	7	Jan	11	2016		0	0	0	215	-639	66	14
24	12	Jan	12	2016		0	0	0	205	<i>L</i> 2477	316	01
25	13	Jan	13	2016		0	0	0	200	-475	415	01
26	14	Jan	14	2016		0	0	0	190	-416	912	11
27	15	Jan	15	2016		0	0	0	212	-654	429	0
28	16	Jan	16	2016		0	0	0	201	-302	352	14
29	17	Jan	17	2016		0	0	0	203	-407	228	14
30	18	Jan	18	2016		0	0	0	210	-111	584	15
31	19	Jan	19	2016		0	0	0	192	48	1,201	0
32	20	Jan	20	2016		0	0	0	161	142	1,291	14
33	21	Jan	21	2016		0	0	0	175	476	1,415	0
34	22	Jan	22	2016		0	0	0	205	-422	16	11
35	23	Jan	23	2016		0	0	0	190	-263	908	21
36	24	Jan	24	2016		0	0	0	187	69	1,399	24
37	25	Jan	25	2016		0	0	0	192	98	1,332	0
38	56	Jan	56	2016		0	0	0	184	-535	315	0
39	27	Jan	27	2016		0	0	0	198	-433	341	12
40	28	Jan	28	2016		0	0	0	209	-165	262	0
41	29	Jan	59	2016		0	0	0	198	-238	1,017	1
42	30	Jan	30	2016		0	0	0	165	206	1,376	0
43	31	Jan	31	2016		0	0	0	167	92	1,024	4

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Exhibit No.

A B	Н		ပ	۵	ΑG	АН	ΑI	AJ	AK	AL	AM	AN
			E	E	Ш	ЕDDY СО	PNM	LAMAR	LPL	SWPP	WIND	SOLAR
Seq# Month Day Year Av	Day Year	Year		Á	á	Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
Feb 1	1 2016	2016		0	0		0	0	192	35	965	0
Feb 2	2 2016	2016		0	0		0	0	208	192	1,583	7
34 Feb 3 2016 0	3 2016	2016		0	0		0	0	242	-453	315	11
35 Feb 4 2016 0	4 2016	2016		0	0		0	0	197	-111	200	13
36 Feb 5 2016 0	5 2016	2016		0	0		0	0	197	137	1,101	0
Feb 6	6 2016	2016		0	0		0	0	182	-410	315	14
38 Feb 7 2016 0	7 2016	2016		0	0		0	0	164	-186	889	10
Feb 8	8 2016	2016		0	0		0	0	188	36	1,051	0
40 Feb 9 2016 0	9 2016	2016		0	0		0	0	218	-78	712	17
Feb 10	10 2016	2016		0	0		0	0	191	396	1,033	0
42 Feb 11 2016 0	11 2016	2016		0	0		0	0	181	237	797	1
Feb 12	12 2016	2016		0	0		0	0	191	-242	699	1
Feb 13	13 2016	2016		0	0		0	0	170	253	1,243	14
Feb 14	14 2016	2016		0	0		0	25	171	-120	437	24
Feb 15	15 2016	2016		0	0		0	0	188	-592	365	-
47 Feb 16 2016 0	16 2016	2016		0	0		0	0	177	-333	1,109	1
Feb 17	17 2016	2016		0	0		0	0	180	-195	1,251	-
Feb 18	18 2016	2016		0	0		0	0	161	96	1,534	1
Feb 19	19 2016	2016		0	0		0	0	162	-135	1,103	0
Feb 20	20 2016	2016		0	0		0	0	165	-143	774	0
Feb 21	21 2016	2016		0	0		0	0	153	-543	489	0
Feb 22	22 2016	2016		0	0		0	0	158	-566	481	0
54 Feb 23 2016 0	23 2016	2016		0	0		0	0	182	-633	637	0
55 Feb 24 2016 0	24 2016	2016		0	0		0	0	190	-174	852	10
56 Feb 25 2016 0	25 2016	2016		0	0		0	0	176	-417	962	3
57 Feb 26 2016 0	26 2016	2016		0	0		0	0	193	-390	783	10
Feb 27	27 2016	2016		0	0		0	-13	163	289	1,359	3
59 Feb 28 2016 0	28 2016	2016		0))	0	-25	165	183	755	0
60 Feb 29 2016 C	29 2016	2016)		0	0	0	167	461	1,348	3

	Α	В	C	Q	AG	AH	ΑI	۲Y	AK	AL	AM	AN
10						ЕРБУ СО	MNd	LAMAR	LPL	SWPP	WIND	SOLAR
11	Sed#	Month	Day	Year		Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
12												
73	61	Mar	1	2016		0	0	-12	158	94	1,179	4
74	62	Mar	7	2016		0	0	0	175	124	1,101	2
75	63	Mar	3	2016		0	0	-25	168	284	229	0
92	64	Mar	4	2016		0	0	0	164	430	1,471	3
77	92	Mar	2	2016		0	0	-28	160	-36	1,057	0
78	99	Mar	9	2016		0	0	-27	160	147	1,350	0
79	29	Mar	7	2016		0	0	-25	168	-134	1,077	0
80	89	Mar	∞	2016		0	0	0	171	-207	485	0
81	69	Mar	6	2016		0	0	0	168	-266	334	0
82	20	Mar	10	2016		0	0	0	166	-231	218	4
83	7.1	Mar	11	2016		0	0	0	165	-230	392	7
84	72	Mar	12	2016		0	0	-31	155	204	1,057	22
85	73	Mar	13	2016		0	0	0	155	-51	469	0
98	74	Mar	14	2016		0	0	0	162	72	1,291	0
87	75	Mar	15	2016		0	0	0	128	-229	999	0
88	9/	Mar	16	2016		0	0	0	126	-132	735	9
89	77	Mar	17	2016		0	0	0	152	-350	180	4
90	78	Mar	18	2016		22	0	0	155	25	1,371	18
91	79	Mar	19	2016		0	0	0	174	-857	294	25
92	80	Mar	70	2016		0	0	0	167	-249	169	23
93	81	Mar	21	2016		0	0	0	174	151	1,500	0
94	82	Mar	22	2016		0	0	-62	162	479	1,415	0
92	83	Mar	23	2016		0	0	-18	159	-94	1,300	0
96	84	Mar	24	2016		0	0	0	181	-117	1,041	0
97	82	Mar	22	2016		0	0	0	167	161	1,246	11
98	98	Mar	26	2016		0	0	0	151	162	1,001	17
66	87	Mar	27	2016		0	0	41	163	-11	187	34
100	88	Mar	28	2016		0	0	0	164	85	1,469	0
101	83	Mar	53	2016		0	0	-50	166	220	1,450	0
102	6	Mar	30	2016		0	0	-43	174	101	1,239	22
103	91	Mar	31	2016		0	0	-25	158	-123	923	0

	٧	В	Э	D	AG	HY	ΑI	AJ	AK	AL	AM	AN
10						EDDY CO	PNM	LAMAR	LPL	SWPP	WIND	SOLAR
11	Sed#	Month	Day	Year		Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
12												
104	92	Apr	1	2016		0	0	0	166	-428	601	~
105	93	Apr	7	2016		0	0	0	168	-368	715	0
106	94	Apr	3	2016		0	0	-44	159	-185	806	0
107	92	Apr	4	2016		0	0	0	173	45	783	0
108	96	Apr	2	2016		0	0	-13	173	94	1,478	6
109	97	Apr	9	2016		0	0	0	172	-379	764	13
110	86	Apr	7	2016		0	0	0	163	129	891	0
111	66	Apr	8	2016		0	0	0	158	46	296	5
112	100	Apr	6	2016		0	0	0	155	-45	1,141	20
113	101	Apr	10	2016		0	0	-20	191	-134	1,126	0
114	102	Apr	11	2016		0	0	-13	165	-222	692	0
115	103	Apr	12	2016		0	0	0	164	-455	336	0
116	104	Apr	13	2016		0	0	0	167	-72	742	0
117	105	Apr	14	2016		0	0	-26	173	185	1,234	22
118	106	Apr	15	2016		0	0	-25	155	252	1,372	21
119	107	Apr	16	2016		0	0	0	172	289	1,199	22
120	108	Apr	17	2016		0	0	0	155	387	1,080	0
121	109	Apr	18	2016		0	0	0	160	302	688	0
122	110	Apr	19	2016		0	0	0	163	29	145	6
123	111	Apr	70	2016		0	0	0	173	22	211	20
124	112	Apr	21	2016		0	0	0	921	-387	238	20
125	113	Apr	22	2016		40	0	-1	185	164	455	20
126	114	Apr	23	2016		42	0	-25	178	232	1,568	17
127	115	Apr	24	2016		0	0	-25	188	186	1,222	15
128	116	Apr	25	2016		0	0	0	203	597	974	21
129	117	Apr	56	2016		0	0	0	188	366	1,005	19
130	118	Apr	27	2016		0	0	0	183	10	693	20
131	119	Apr	78	2016		0	0	0	186	172	1,052	20
132	120	Apr	53	2016		0	0	0	187	6-	869	17
133	121	Apr	30	2016		0	0	0	166	-52	378	18

	A	В	ပ	Ω	AG	AH	ΙΑ	Υ	AK	AL	AM	NA
10						EDDY CO	PNM	LAMAR	LPL	SWPP	QNIM	SOLAR
11	Seq#	Month	Day	Year		Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
12												
134	122	Мау	1	2016		0	0	0	150	436	966	0
135	123	May	2	2016		0	0	0	167	2	142	1
136	124	Мау	3	2016		0	0	0	161	233	864	18
137	125	Мау	4	2016		0	0	0	187	-222	82	17
138	126	Мау	2	2016		0	0	0	207	396	502	20
139	127	Мау	9	2016		0	0	0	196	208	1,588	16
140	128	Мау	4	2016		0	0	0	207	298	1,454	17
141	129	Мау	8	2016		0	0	0	200	96	966	16
142	130	Мау	6	2016		0	0	0	198	-132	111	17
143	131	Мау	10	2016		0	0	0	221	296	962	20
144	132	Мау	11	2016		0	0	0	222	32	929	6
145	133	Мау	12	2016		0	0	0	197	9-	374	13
146	134	Мау	13	2016		0	0	-26	221	-65	913	20
147	135	Мау	14	2016		0	0	-110	157	-150	1,159	0
148	136	Мау	15	2016		0	0	0	155	-35	089	0
149	137	Мау	16	2016		0	0	0	199	179	286	13
150	138	Мау	11	2016		0	0	0	164	203	1,371	4
151	139	Мау	18	2016		0	0	0	164	-171	301	2
152	140	Мау	19	2016		0	0	0	162	-237	249	5
153	141	Мау	20	2016		0	0	0	171	267	1,264	16
154	142	Мау	21	2016		0	0	-50	201	140	1,462	19
155	143	May	22	2016		0	0	-122	219	175	1,181	21
156	144	Мау	23	2016		0	0	0	233	-53	790	18
157	145	Мау	24	2016		0	0	0	245	117	1,239	10
158	146	Мау	25	2016		0	0	0	245	260	1,071	19
159	147	May	26	2016		0	0	0	234	227	1,509	16
160	148	Мау	27	2016		0	0	0	205	-228	639	19
161	149	Мау	28	2016		0	0	13	212	-142	285	19
162	150	Мау	29	2016		0	0	0	204	177	1,068	7
163	151	Мау	30	2016		0	0	0	201	-48	627	7
164	152	Мау	31	2016		0	0	-13	208	-158	573	15

Seq# Month Ag Ag Avg LAMAR LLOL 153 Jun 1 Ag Avg FLOWAvg 153 Jun 2 2016 0 0 168 154 Jun 3 2016 0 0 178 155 Jun 3 2016 0 0 178 155 Jun 4 2016 0 0 201 156 Jun 4 2016 0 0 201 159 Jun 5 2016 0 0 202 160 Jun 5 2016 0 0 203 161 Jun 10 2016 6 0 203 203 165 Jun 11 2016 50 0 203 203 166 Jun 12 2016 40 0 223 167 Jun 13		Α	В	ပ	Q	ΑG	AH	ΑI	Υ	AK	AL	AM	AN
Seq# Month Day Year Avg Avg Avg 153 Jun 1 2016 0 0 0 154 Jun 2 2016 0 0 0 155 Jun 3 2016 0 0 0 155 Jun 4 2016 0 0 0 156 Jun 5 2016 0 0 0 167 Jun 1 2016 0 0 0 167 Jun 1 2016 0 0 0 168 Jun 1 2016 0 0 0 167 Jun 1 2016 40 0 0 168 Jun 1 2016 40 0 0 169 Jun 1 2016 40 0 0 169 Jun 1 2016 40 <t< th=""><th>10</th><th></th><th></th><th></th><th></th><th></th><th>Ерру со</th><th>PNM</th><th>LAMAR</th><th>LPL</th><th>SWPP</th><th>WIND</th><th>SOLAR</th></t<>	10						Ерру со	PNM	LAMAR	LPL	SWPP	WIND	SOLAR
153 Jun 1 2016 0 0 0 0 0 1 154 Jun 2 2016 0	11	%ed	Month	Day	Year		Avg	Avg	Avg	FLOW Avg	Avg	Avg	Avg
153 Jun 1 2016 0 0 0 0 0 1 154 Jun 2 2016 0	12												
154 Jun 2 2016 0 0 0 0 1 1 1 1 1 2 2016 0 <th< th=""><th>165</th><th>153</th><th>Jun</th><th>1</th><th>2016</th><th></th><th>0</th><th>0</th><th>0</th><th>166</th><th>-139</th><th>303</th><th>16</th></th<>	165	153	Jun	1	2016		0	0	0	166	-139	303	16
155 Jun 3 2016 0 0 0 0 1<	166	154	Jun	2	2016		0	0	0	178	-165	248	6
156 Jun 4 2016 0 0 0 0 10 15 10 15 10 15 2016 0 0 0 25 10 <th>167</th> <th>155</th> <th>Jun</th> <th>3</th> <th>2016</th> <th></th> <th>0</th> <th>0</th> <th>0</th> <th>202</th> <th>-364</th> <th>92</th> <th>18</th>	167	155	Jun	3	2016		0	0	0	202	-364	92	18
157 Jun 5 2016 0 0 25 158 Jun 6 2016 26 0 43 159 Jun 7 2016 26 0 60 160 Jun 8 2016 50 0 0 161 Jun 10 2016 50 0 0 162 Jun 11 2016 0 0 0 163 Jun 12 2016 0 0 0 164 Jun 13 2016 40 0 0 165 Jun 13 2016 40 0 0 165 Jun 15 2016 40 0 0 170 Jun 18 2016 40 0 0 172 Jun 2016 40 0 0 0 173 Jun 2016 40 0	168	156	Jun	4	2016		0	0	0	201	-431	409	6
158 Jun 6 2016 26 0 43 159 Jun 7 2016 46 0 50 160 Jun 8 2016 50 0 0 161 Jun 10 2016 50 0 0 162 Jun 11 2016 50 0 0 163 Jun 12 2016 0 0 0 164 Jun 13 2016 0 0 0 165 Jun 13 2016 40 0 0 165 Jun 15 2016 40 0 0 169 Jun 15 2016 40 0 0 170 Jun 16 40 0 0 0 173 Jun 17 2016 40 0 0 174 Jun 10 20 0	169	157	Jun	2	2016		0	0	25	220	-184	26	26
159 Jun 7 2016 46 0 50 160 Jun 8 2016 50 0 0 161 Jun 9 2016 50 0 0 162 Jun 10 2016 50 0 0 163 Jun 11 2016 0 0 0 164 Jun 12 2016 0 0 0 165 Jun 13 2016 40 0 0 165 Jun 14 2016 40 0 0 169 Jun 15 2016 40 0 0 170 Jun 17 2016 40 0 0 172 Jun 18 2016 40 0 0 173 Jun 21 2016 40 0 0 174 Jun 22 2016 0	170	158	Jun	9	2016		26	0	43	229	10	439	10
160 Jun 8 2016 50 0 0 161 Jun 9 2016 50 0 0 162 Jun 10 2016 50 0 0 163 Jun 11 2016 25 0 0 164 Jun 12 2016 0 0 0 165 Jun 13 2016 40 0 0 165 Jun 14 2016 40 0 0 165 Jun 15 2016 40 0 0 169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 172 Jun 20 2016 40 0 0 173 Jun 22 2016 40 0 0 174 Jun 22 2016 0	171	159	Jun	7	2016		46	0	50	212	372	814	24
161 Jun 9 2016 50 0 0 162 Jun 10 2016 50 0 0 163 Jun 11 2016 25 0 0 164 Jun 12 2016 0 0 0 165 Jun 13 2016 40 0 0 165 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 171 Jun 2016 40 0 0 0 173 Jun 20 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 40	172	160	Jun	8	2016		90	0	0	236	387	1,258	19
162 Jun 10 2016 50 0 0 163 Jun 11 2016 25 0 0 164 Jun 12 2016 0 0 0 165 Jun 13 2016 40 0 0 166 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 171 Jun 19 2016 40 0 0 172 Jun 20 2016 60 0 0 173 Jun 22 2016 40 0 0 174 Jun 23 2016 60 0 0 175 Jun 22 2016 0	173	161	Jun	6	2016		90	0	0	243	479	1,281	20
163 Jun 11 2016 25 0 0 164 Jun 12 2016 0 0 0 165 Jun 13 2016 0 0 0 166 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 171 Jun 20 2016 40 0 0 172 Jun 20 2016 40 0 0 173 Jun 20 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 40 0 0 175 Jun 25 2016 0	174	162	Jun	10	2016		90	0	0	222	225	808	19
164 Jun 12 2016 0 0 165 Jun 13 2016 20 0 166 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 168 Jun 16 2016 40 0 0 170 Jun 17 2016 40 0 0 171 Jun 18 2016 40 0 0 172 Jun 20 2016 40 0 0 173 Jun 20 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 175 Jun 25 2016 0 0 0 177 Jun 25 2016 0 0 0	175	163	Jun	11	2016		25	0	0	217	186	927	11
165 Jun 13 2016 20 0 0 166 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 168 Jun 16 2016 40 0 0 170 Jun 17 2016 40 0 0 171 Jun 18 2016 40 0 0 172 Jun 20 2016 40 0 0 173 Jun 20 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 0 175 Jun 25 2016 40 0 0 0 175 Jun 25 2016 0 0 0 0 180 Jun	176	164	Jun	12	2016		0	0	0	209	294	930	18
166 Jun 14 2016 40 0 0 167 Jun 15 2016 40 0 0 168 Jun 16 2016 40 0 0 170 Jun 17 2016 40 0 0 171 Jun 18 2016 40 0 0 172 Jun 20 2016 44 0 0 173 Jun 21 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 40 0 0 175 Jun 23 2016 55 0 0 177 Jun 25 2016 0 0 0 178 Jun 25 2016 0 0 0 181 Jun 29 2016 0	177	165	Jun	13	2016		20	0	0	243	133	654	11
167 Jun 15 2016 40 0 0 168 Jun 16 2016 40 0 0 170 Jun 17 2016 40 0 0 171 Jun 18 2016 40 0 0 172 Jun 20 2016 44 0 0 173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 175 Jun 25 2016 40 0 0 177 Jun 25 2016 0 0 0 178 Jun 25 2016 0 0 0 180 Jun 28 2016 0 0 0 181 Jun 29 2016 0	178	166	Jun	14	2016		40	0	0	232	-354	320	15
168 Jun 16 2016 40 0 0 169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 171 Jun 20 2016 44 0 0 172 Jun 20 2016 40 0 0 173 Jun 22 2016 40 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 177 Jun 25 2016 40 0 0 178 Jun 25 2016 0 0 0 180 Jun 27 2016 0 0 0 181 Jun 29 2016 0 0 0	179	167	Jun	15	2016		40	0	0	271	180	1,041	7
169 Jun 17 2016 40 0 0 170 Jun 18 2016 40 0 0 171 Jun 19 2016 40 0 0 172 Jun 20 2016 44 0 0 173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 177 Jun 25 2016 40 0 46 177 Jun 25 2016 0 0 25 178 Jun 27 2016 0 0 0 0 181 Jun 29 2016 0 0 0 0 182 Jun 29 2016 0 0 0 0	180	168	Jun	16	2016		40	0	0	238	392	1,248	16
170 Jun 18 2016 40 0 0 171 Jun 19 2016 40 0 0 172 Jun 20 2016 44 0 0 173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 177 Jun 25 2016 40 0 46 178 Jun 25 2016 0 0 25 180 Jun 27 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0	181	169	Jun	17	2016		40	0	0	280	-238	748	16
171 Jun 19 2016 40 0 0 172 Jun 20 2016 44 0 0 173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 0 176 Jun 24 2016 40 0 46 1 177 Jun 25 2016 0 0 46 1 178 Jun 25 2016 0 0 0 0 180 Jun 27 2016 0 0 0 0 181 Jun 29 2016 0 0 0 0	182	170	Jun	18	2016		40	0	0	265	-162	508	21
172 Jun 20 2016 44 0 0 173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 177 Jun 25 2016 40 0 -46 178 Jun 25 2016 0 0 0 0 180 Jun 27 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0	183	171	Jun	19	2016		40	0	0	248	-347	338	15
173 Jun 21 2016 60 0 0 174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 176 Jun 24 2016 40 0 -46 177 Jun 25 2016 0 0 -46 178 Jun 26 2016 0 0 0 0 180 Jun 27 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0 182 Jun 29 2016 20 0 0 0	184	172	Jun	70	2016		44	0	0	239	-440	791	15
174 Jun 22 2016 40 0 0 175 Jun 23 2016 55 0 0 176 Jun 24 2016 40 0 -46 177 Jun 25 2016 0 0 -46 178 Jun 27 2016 0 0 0 0 180 Jun 28 2016 0 0 0 0 181 Jun 29 2016 40 0 0 0	185	173	Jun	21	2016		09	0	0	227	-51	1,028	13
175 Jun 23 2016 55 0 0 176 Jun 24 2016 55 0 0 177 Jun 25 2016 40 0 -46 178 Jun 26 2016 0 0 25 180 Jun 27 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0 182 Jun 30 2016 40 0 0 0	186	174	Jun	22	2016		40	0	0	259	-108	921	15
176 Jun 24 2016 55 0 0 177 Jun 25 2016 40 0 -46 178 Jun 26 2016 0 0 25 179 Jun 27 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0 182 Jun 30 2016 40 0 0 0	187	175	Jun	23	2016		55	0	0	260	-185	404	16
177 Jun 25 2016 40 0 -46 178 Jun 26 2016 0 0 25 179 Jun 27 2016 0 0 0 180 Jun 28 2016 0 0 0 181 Jun 29 2016 20 0 0 182 Jun 30 2016 40 0 0	188	176	Jun	24	2016		55	0	0	234	68	1,021	15
178 Jun 26 2016 0 0 25 179 Jun 27 2016 0 0 0 180 Jun 28 2016 0 0 0 181 Jun 29 2016 20 0 0 182 Jun 30 2016 40 0 0	189	177	Jun	25	2016		40	0	-46	210	-139	1,264	16
179 Jun 27 2016 0 0 0 180 Jun 28 2016 0 0 0 181 Jun 29 2016 20 0 0 182 Jun 30 2016 40 0 0	190	178	Jun	56	2016		0	0	25	218	136	202	19
180 Jun 28 2016 0 0 0 0 181 Jun 29 2016 20 0 0 0 182 Jun 30 2016 40 0 0	191	179	Jun	27	2016		0	0	0	230	-76	239	6
181 Jun 29 2016 20 0 0 0	192	180	Jun	28	2016		0	0	0	265	-257	234	20
182 1.15 30 2016 40 0	193	181	Jun	59	2016		20	0	0	234	-8	517	17
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	194	182	Jun	30	2016		40	0	0	233	-312	507	24

AN SOLAR Avg

	٧	В	Э	/ Q	AG	АН	ΙV	ſΥ	AK	٦V	AM
9						ЕРБУ СО	PNM	LAMAR	LPL	SWPP	WIND
1	Sed#	Month	Day	Year	H	Avg	Avg	Avg	FLOW Avg	Avg	Avg
12											
195	183	Jnf	1	2016		40	0	0	229	-148	998
196	184	Jul	2	2016		40	0	0	234	-443	927
197	185	Jnf	æ	2016		40	0	14	235	-445	203
198	186	Jul	4	2016		40	0	0	238	-414	168
199	187	Jul	2	2016		22	0	0	273	-459	479
200	188	Jul	9	2016		20	0	0	261	-203	831
201	189	Jul	7	2016		22	0	0	259	-453	871
202	190	Jul	∞	2016		55	0	0	241	-141	1,070
203	191	Jul	6	2016		40	0	0	526	54	748
204	192	Jul	10	2016		22	0	0	235	329	1,163
205	193	Juf	11	2016		02	0	0	277	13	1,221
206	194	Jul	12	2016		20	0	0	288	809-	474
207	195	Jul	13	2016		20	0	0	298	896-	262
208	196	Jul	14	2016		20	0	0	274	099-	608
209	197	Jul	15	2016		20	0	0	241	-364	526
210	198	Jul	16	2016		70	0	0	250	-283	902
211	199	Jul	17	2016		75	0	0	244	173	1,371
212	200	Jul	18	2016		0	0	0	246	12	1,010
213	201	Juf	19	2016		17	0	0	266	86-	833
214	202	luſ	70	2016		70	0	0	268	02-	1,184
215	203	Juf	21	2016		20	0	0	295	-113	1,069
216	204	Jul	22	2016		02	8-	0	255	112	1,035
217	205	Jul	23	2016		28	-16	0	256	178	1,011
218	206	Jul	24	2016		40	-16	0	250	20	619
219	207	Jul	22	2016		58	7	0	275	-503	154
220	208	Jul	56	2016		98	-16	0	261	689-	212
221	209	Jul	27	2016		98	37	0	254	-601	493
222	210	Jul	28	2016		98	68	37	247	-821	231
223	211	Jul	59	2016		0	65	0	259	-73	894
224	212	Jul	30	2016		25	9-	0	249	-259	969
225	213	Juf	31	2016		0	-65	0	257	9/	1,235

		0)			i			,
Ŋ	22	Aug	6	2016	40	14	87	258	-330
7	223	Ang	10	2016	40	-40	0	250	-206
236 2	24	Aug	11	2016	40	-84	20	263	-380
	25	Aug	12	2016	40	-21	0	264	-363
238 2	226	Aug	13	2016	40	-21	0	212	-528
	27	Ang	14	2016	40	-18	0	181	-365
	28	Aug	15	2016	40	34	0	226	-260
241 2	229	Aug	16	2016	40	0	0	233	-312
242 2:	30	Aug	17	2016	40	38	0	232	-355
	231	Aug	18	2016	40	-21	0	244	-443
244	232	Aug	19	2016	40	-16	0	273	-865
	33	Aug	20	2016	0	-21	13	192	-580
246 2	34	Aug	21	2016	0	13	0	191	-488
	35	Aug	22	2016	0	4	0	212	-229
	236	Aug	23	2016	40	4	0	234	4
249 2	237	Aug	24	2016	75	-16	13	210	62
	238	Ang	25	2016	75	-21	25	204	-95
	39	Aug	56	2016	0	-21	0	204	-128
252 2.	240	Aug	27	2016	0	-13	0	222	243
	241	Aug	28	2016	0	-55	38	225	2
254 2	242	Aug	29	2016	0	-16	0	198	192
255 2	243	Aug	30	2016	0	-32	0	197	372
256 2	244	Aug	31	2016	0	-45	0	198	129

17 39 10 35

25 50 50

1,197 544 505

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23 23

214 215 216

226

-37 -445 -309 -344 -458 -303 -367 -500

263 272 271 271 284 284 267 267 266 266

0

-21 -26 -39 -39 -4 -4 -16 -21 -21

2016 2016 2016 2016 2016 2016 2016 2016

4

217 218 219 220 221

0

0 0 0 0 8

0

AN SOLAR Avg

WIND AM

AL SWPP

AK LPL

LAMAR

PNM Avg

EDDY CO Avg

Year

Day

Month

% bes

ΑH

Avg

Avg

FLOW Avg

52 53 37 64 64 46 20 31 27

18 14 41

1,126 1,159 920 920 161 772 366 209 37 24

AN	SOLAR	Avg		44	48	18	49	45	8	35	50	45	46	39	22	51	29	6	43	26	44	43	50	19	47	54	53	0	7	63	19	63	73
AM	MIND	Avg		06	386	1,084	1,216	1,319	1,063	1,055	622	358	474	1,038	911	288	275	838	352	409	623	205	753	1,064	1,000	1,233	382	465	119	284	596	225	981
AL	SWPP	Avg		-524	-343	-367	-126	06-	-318	-83	-556	-743	-389	-426	-330	-390	-292	-474	-295	-136	-139	-152	-151	-183	-126	-139	999-	-338	-627	-219	-549	161-	-15
AK	LPL	FLOW Avg		227	226	218	187	204	221	201	231	234	210	185	232	233	216	205	174	173	200	231	230	221	218	222	192	154	147	168	211	174	169
Υ	LAMAR	Avg		0	0	-25	-50	-83	0	7	0	-25	-20	-124	-91	-40	09	0	13	38	22	32	-115	-150	-35	0	0	16	0	0	0	0	0
ΙΑ	PNM	Avg		89	82	61	93	9	73	-23	7	24	48	69	138	9	-32	82	9	-16	71	82	-16	06	40	-16	-15	2	-15	-23	-16	-43	-16
АН	EDDY CO	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ВA																																	
Ω		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	59	30
В		Month		Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep	Sep
A		Sed#		245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274
	10	11	12	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286

AM	WIND	Avg		878	885	1,445	915	514	856	646	839	723	721	985	745	585	1,181	888	1,238	1,362	929	1,027	448	875	1,245	689	162	1,020	583	725	1,389	840	396	1.316
AL	SWPP	Avg		-168	-142	5	40	242	28	-249	-142	-280	-504	-278	-599	-232	83	-188	-221	-84	251	325	-133	-73	-248	-49	99	-281	443	347	-36	-266	-143	-263
AK	LPL	FLOW Avg		182	213	188	188	162	191	138	137	149	174	197	164	166	180	182	207	186	186	205	152	168	173	167	182	192	166	200	200	194	167	201
Υ	LAMAR	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ΙΑ	PNM	Avg		7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	C
AH	EDDY CO	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	40	40	40	40	0	0	0	0	0	0	0	0	0	C
AG																																		
۵		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	70	21	22	23	24	22	56	27	28	29	30	31
В		Month		Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct	Oct
Α		# bəS		275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305
	10	11	12	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317
_								_																								_		

51 52 74 73 82 20

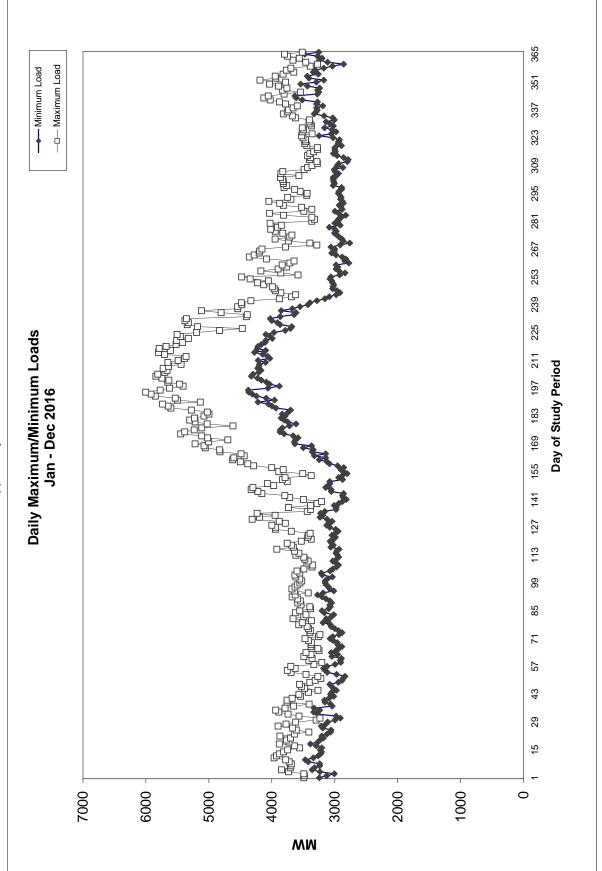
AN SOLAR Avg 62 78 85

AN	Š	Avg																				1											
AM	WIND	Avg		483	470	181	111	722	661	403	918	222	629	854	366	258	473	628	1,304	1,405	1,044	1,147	836	996	1,398	663	862	765	1,120	1,383	1,299	691	100
AL	SWPP	Avg		-57	-186	-25	-88	43	-233	489	125	20	-223	-197	24	-386	204	187	339	-10	-194	294	-61	-74	-41	-278	-131	-168	-116	179	136	-496	700
AK	TH	FLOW Avg		190	177	172	165	159	170	177	173	179	176	166	165	174	170	178	176	176	172	191	121	179	163	175	165	145	170	149	175	154	107
AJ	LAMAR	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	ď
ΑI	PNM	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	c
AH	ЕББҮ СО	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
ΑG																																	Ī
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
၁		Day		Н	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	25	25	56	27	28	59	00
В		Month		Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Nov	Non															
٧		Sed#		306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335
	10	11	12	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	476

AN SOLAR Avg

AM	WIND	Avg		217	550	245	514	1,169	1,221	1,280	456	626	1,147	491	894	841	870	829	1,655	1,274	259	928	490	1,297	279	1,018	932	1,393	427	674	1,300	1,149	1.591
_																																	
AL	SWPP	Avg		-253	-170	-481	-255	-245	-129	-252	-182	302	-83	-386	274	167	377	138	271	259	349	-87	-344	-291	099-	-293	-139	-45	-467	-526	-259	-95	-461
AK	LPL	FLOW Avg		188	212	205	208	172	193	238	235	258	215	193	171	181	202	193	204	213	225	239	230	183	188	157	179	157	186	199	182	169	205
AJ	LAMAR	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
ΑI	PNM	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
AH	EDDY CO	Avg		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
AG																																	
D		Year		2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016	2016
ပ		Day		1	7	8	4	2	9		8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	22	56	27	28	59	30
В		Month		Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec	Dec
А		% bes		336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	329	360	361	362	363	364	365
	10	11	12	348	349	350	351	352	353	354	355	356	357	358	329	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377

40



App. D - System Load Data 6

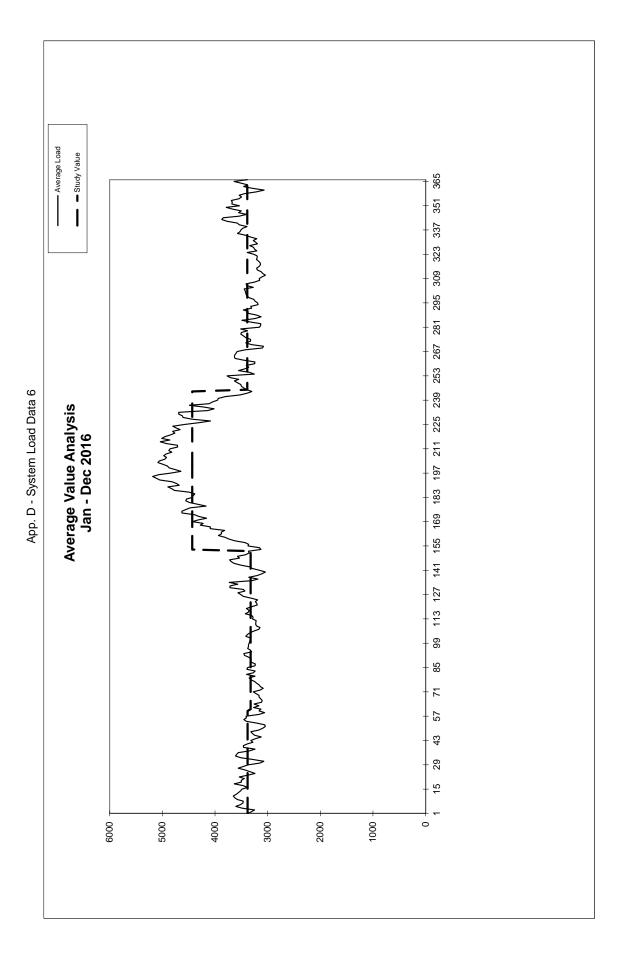


Exhibit No. SPS-0005_2016 Loss Study-FINAL.xlsx App. D - System Load Data 6

Demand Losses MW

Energy Losses MWH

Line No. 1 Corona & Insulator Leakage Demand and Energy Losses

2.12 2.21 1.27

18,634

2.343 1.185

905.42

345 kV Line

1,862.03

230 kV Line 115 Kv Line

KW Loss/mile

51,811 MWH 2,678 11,116 19,382

0.403 0.197

3,140.28

69 kV Line 1,547.58 7,455.31 Anni Transmission Line Demand Loss	0 197		2.678		0.30								
55.31 Anr	5		î										
nand Loss	7,455.31 Annual Losses		51,811 MWH	WH.	5.90 MW	MW							
					WW								
This	This data comes from	n the peak			8.26								
nou	nour powernow case.	. App. R			47.35								
					66.32								
					19.19								
Transmission Line Energy Loss													
	Segr	Segment 1 So	Segment 2 Segment 3		Segment 4								
	8	3379.7	3323.4	4432.1	3386.9								
Segment Output to Lines, MWH	4	,685,818	7,256,647	10,175,397	9,640,414								
	Segr MW Loss F	Segment 1 Factor		MW Loss	Segment 2 Factor		MW Loss	Segment 3 Factor I	MWH Loss MW Loss		Segment 4 Factor	MWH Loss	MWH Loss Losses, MWH
	0.960	0.0027	37 801	9.032	0.0030	105,858	40.522	0.00	16,991	10.007	0.0032	30,363	364.668
	29.519	0.0087	40,927	41.440	0.0125	90,484	43.111	0.0097	98,975	44.789	0.0132	127,488	357,874
	6.118	0.0018	8,482	9.090	0.0018	13,298	10.916	0.0025	25,061	5.294	0.0016	15,068	61,909

Appendix F Autotransformer Losses Under Load

Line No.

Autonalisionillei Eille Delland Eoss	Dellially E03	2			M								
345/230 kV Autos	This data come:	This data comes from the peak hour powerflow.	eak		0.80								
230/115 kV Autos	_				7.40								
115/69 Kv Autos					4.36								
Autotransformer Energy Loss	rgy Loss												
Segment Name		Segment 1 Segment 2	Segment 2	Segment 3 Segment 4	Segment 4								
Segment Load, MW		3379.7	3323.4	4432.1	3386.9								
Segment Output to Lines, MWH	ines, MWH	4,685,818	7,256,647	10,175,397	9,640,414								
345/230 KV Autos	MW Loss 0.674	Segment 1 Factor 0.0002	MWH Loss 934	8 MW Loss 0.764	Segment 2 Factor 0.0002	MWH Loss 1,669	8 MW Loss 0.853	Segment 3 Factor 0.0002	egment 3 Factor MWH Loss 0.0002 1,959	S MW Loss 0.734	Segment 4 Factor 0.0002	MWH Loss 2,089	Total Segment MWH Loss Losses, MWH 2,089 6,651
230/115 kV Autos	4.880	0.0014	6,766	4.626	0.0014	10,101	5.503	0.0012	12,634	4.827	0.0014	13,740	43,241
115/69 Kv Autos	2.564	0.0008	3,555	2.541	0.0008	5,548	3.202	0.0007	7,350	2.384	0.0007	6,785	23,239

Appendix G Autotransformer No-Load Losses

Line No.	Location	Voltage	Nominal Rating MVA	Max Rating MVA	No Load Loss, Watts	Energy Losses, MWH 345 Kv 230 kV 115 kV	Demand Losses, KW 345 Kv 230 kV 115 kV
1	AMA_SOUTH	230/120	135	252	55,500	487.51	55.50
2	ARTESIA	115/69	23.77	39.6	15,268	134.11	15.27
3	ARTESIA	115/69	23.77	39.6	15,268	134.11	15.27
4	ATOKA	115/69	23.77	39.62	21,060	184.99	21.06
5 6	BAILEYCO BAILEYCO	115/69 115/69	50 50	84 84	17,540 18,460	154.07 162.15	17.54 18.46
7	BLACKHAWK	115/69	45	75	14,249	125.16	14.25
8	BLACKHAWK	115/69	45	75	14,335	125.92	14.34
9	BOWERS	120/69	45	84	14,340	125.96	14.34
10	BOWERS	115/69	50	84	20,615	181.08	20.62
11 12	BUSHLAND CARLISLE	230/115 230/115	90 90	150 150	86,001 57,968	755.43 509.19	86.00 57.97
13	CARLISLE	115/69	23.77	39.62	18,380	161.45	18.38
14	CARLSBAD	115/69	23.77	39.62	22,450	197.20	22.45
15	CARLSBAD	115/69	23.77	39.62	16,900	148.45	16.90
16	CASTRO_N	120/69	45	84	14,901	130.89	14.90
17 18	CASTRO_S CHAVES CO INT E	120/69 230/120	45 150	84 288	14,917 50,458	131.03 443.22	14.92 50.46
19	CHAVES CO INT W	230/120	135	252	61,380	539.16	61.38
20	CHAVES INT	115/69	23.77	39.62	18,700	164.26	18.70
21	COCHRAN	115/69	50	84	25,750	226.19	25.75
22	COCHRAN	115/69	50	84	26,050	228.82	26.05
23	COULTER	115/69	45	75	25,659	225.39	25.66
24 25	COX CROSBY	120/69 115/69	45 50	84 84	17,390 18,920	152.75 166.19	17.39 18.92
26	CROSBY	115/69	50.4	84	19,647	172.58	19.65
27	CUNNINHAM	230/115	90	150	84,128	738.98	84.13
28	CURRY	115/69	23.77	39.62	18,205	159.91	18.21
29	CURRY	115/69	23.77	39.62	20,110	176.65	20.11
30 31	DALHART DALLAM	115/69 115/69	23.77 23.77	39.62 39.6	20,200 17,840	177.44 156.71	20.20 17.84
32	DEAFSMITH	230/120	150	250	39,230	344.60	39.23
33	DEAFSMITH	230/120	150	250	39,520	347.14	39.52
34	DENVER_N	115/69	50	84	18,660	163.91	18.66
35	DENVER_S	115/69	50	84	18,860	165.67	18.86
36 37	DOSS EAGLE_CREEK	115/69 115/69	50 23.77	84 39.6	17,000 18,205	149.33 159.91	17.00 18.21
38	EAST_PLANT	230/120	135	252	71,492	627.99	71.49
39	EAST_PLANT	115/69	50	84	18,200	159.87	18.20
40	EAST_PLANT	115/69	50	84	17,340	152.31	17.34
41	EDDY_CNTY	345/230	300	560	75,788	665.72	75.79
42 43	EDDY_NORTH EDDY_SOUTH	230/115 230/115	150 150	250 250	37,500 40,891	329.40 359.19	37.50 40.89
44	FLOYD_CNTY	115/69	50	84	26,300	231.02	26.30
45	FLOYD_CNTY	120/69	45	84	13,970	122.71	13.97
46	GAINES	115/69	23.77	39.6	10,900	95.75	10.90
47	GAINES	115/69	23.77	39.6	27,500	241.56	27.50
48 49	GEORGIA GRAHAM	115/69 115/69	45 50	75 84	20,602 21,581	180.97 189.57	20.60 21.58
50	GRAPEVINE	230/115	150	250	38,500	338.18	38.50
51	GRASSLAND	230/115	150	250	41,860	367.70	41.86
52	GRAY_CNTY	115/69	45	75	24,519	215.37	24.52
53	HALE_CNTY	115/69	50	84	23,520	206.60	23.52
54 55	HALE_CNTY HAPPY_INT	115/69 115/69	50 50	84 84	23,910 20,982	210.03 184.31	23.91 20.98
56	HAPPY_INT	115/69	50	84	22,351	196.33	20.96
57	HEREFORD	115/66	23.77	39.6	21,030	184.73	21.03
58	HEREFORD	115/69	23.77	39.6	23,340	205.02	23.34
59	HITCHLAND	345/230	336	560	86,954	763.80	86.95
60	HITCHLAND	230/115	150	250	62,938	552.85	62.94
61 62	HITCHLAND HOCKLEY	345/230 115/69	336 50	560 84	74,704 25,080	656.20 220.30	74.70
63	HOCKLEY	115/69	50	84	23,650	207.74	23.65
64	HOWARD	115/69	50	84	24,939	219.06	24.94
65	HUTCH_S	115/69	45	75	28,199	247.70	28.20
66	HUTCHISON	230/115	90	150	84,172	739.37	84.17
67 68	HUTCHISON KINGSMILL	230/115 115/69	90 50	150 84	90,549 18,560	795.38 163.03	90.55 18.56
69	KINGSMILL	115/69	45	75	33,190	291.54	33.19
70	KRESS_INT	115/69	50	84	24,100	211.69	24.10
71	LAMB_CNTY	230/120	135	252	69,698	612.23	69.70
72	LAMB_CNTY	120/69	45	84	17,020	149.50	17.02
73	LAMB_CNTY	120/69	45 45	84	17,600	154.60	17.60
74 75	LAMTON LEGACY	115/69 115/69	45 50	75 84	14,230 25,140	125.00 220.83	14.23 25.14
75 76	LUBBCK_EST	230/115	150	250	65,770	577.72	65.77
77	LUBBCK_EST	115/69	50	84	26,330	231.28	26.33
78	LUBBCK_EST	115/69	50	84	25,300	222.24	25.30
79	LUBBCK_STH	120/69	45 125	84	15,020	131.94	15.02
80 81	LUBBCK_STH LUBBCK_STH	230/120 230/115	135 150	225 288	60,232 40,980	529.08 529.08 359.97	60.23 40.98
U I	_35550K_0111	200/110	100	200	-10,500	353.31	70.30

Appendix G Autotransformer No-Load Losses

	Location	Voltage	Nominal Rating	Max Rating	No Load Loss,	Energy 345 Kv	Losses, M\ 230 kV	WH 115 kV	Demar 345 Kv	nd Losses, 230 kV	KW 115 kV
Line No.			MVA	MVA	Watts						
82	LYNN_CNTY	115/69	23.77	39.52	16,670			146.43			16.67
83	LYNN_CNTY	115/69	27	45	10,100			88.72			10.10
84	MOORE_CNTY	230/120	150	250	67,370		591.78			67.37	
85	MUSTANG	230/115	150	250	66,670		585.63	400.00		66.67	40.00
86 87	NE_HEREFORD NE_HEREFORD	120/69 115/69	50 50	84 84	19,000 18,840			166.90 165.49			19.00 18.84
88	NEWHART	230/120	150	250	37,900			332.91			37.90
89	NICHOLS	230/120	150	250	65,000		570.96	332.91		65.00	37.30
90	NICHOLS	230/120	150	250	66,200		581.50			66.20	
91	NORTHWEST	120/69	45	84	14,390			126.40			14.39
92	OASIS	230/115	135	225	53,021		465.74			53.02	
93	OCHILTREE	230/115	100	168	51,758		454.64			51.76	
94	PCA	115/69	50	84	19,040			167.25			19.04
95	PECOS	230/115	90	150	50,428		442.96			50.43	
96	PERRYTON	115/66	15	18.75	6,708			58.92		74.70	6.71
97	PLANT_X	230/120	135	225	71,721		630.00	00.00		71.72	44.47
98 99	PORTALES PORTALES	115/69 115/69	45 45	70 70	11,167 14,894			98.09 130.83			11.17 14.89
100	POTASH_JCT	230/120	150	250	40,070		351.97	130.63		40.07	14.09
101	POTASH_JCT	115/69	50	84	20,961	184.12	331.37	184.12		40.07	20.96
102	POTASH JCT	115/69	23.77	39.62	25,320	2		222.41			25.32
103	POTTER_CO	345/230	150	250	65,980	579.57			65.98		
104	PRINGLE	230/120	100	168	37,390		328.43			37.39	
105	RANDALL	230/115	150	250	37,900		332.91			37.90	
106	RANDALL	230/115	135	225	99,620		875.06			99.62	
107	RDRUNNER	230/120	150	288	41,000		360.14			41.00	
108	RIVERVIEW	115/69	23.77	39.63	24,770		450.40	217.58		50.07	24.77
109 110	ROSEVELT_N	230/115	135	225	52,272		459.16	104.04		52.27	18.74
110	ROSWLL_INT ROSWLL INT	115/69 115/69	23.77 23.77	39.62 44.37	18,740 17,400		152.84	164.61 152.84			17.40
112	SEAGRAVES	120/69	23.77 45	44.37 75	14,103		132.04	123.88			14.10
113	SEMINOLE	230/115	90	150	63,300		556.03	556.03		63.30	14.10
114	SEMINOLE	230/115	90	150	58,700		515.62	000.00		58.70	
115	SEVEN_RIVERS	115/69	90	150	58,220			511.40			58.22
116	SEVEN_RIVERS	230/115	23.77	39.62	15,520		136.33			15.52	
117	SPEARMAN	115/69	50	84	24,620			216.26			24.62
118	SULPHUR	120/69	24	44.8	6,280			55.16			6.28
119	SULPHUR	120/69	24	44.8	8,900		500.05	78.18			8.90
120	SUNDOWN	230/118	100	166.66	60,604		532.35			60.60	
121 122	SWISHER TERRY_CNTY	230/115 115/69	150 50	288 84	40,270 24,480		353.73	215.03		40.27	24.48
123	TERRY_CNTY	115/69	50	84	24,460			211.26			24.46
124	TOLK	345/230	300	560	80,850	710.19		211.20	80.85		24.00
125	TUCO_INT	230/115	135	252	54,435			478.16			54.44
126	TUCO_INT	230/115	150	250	66,740			586.24			66.74
127	TUCO_INT	120/69	45	84	14,980			131.58			14.98
128	TUCO_INT	120/69	45	84	14,950			131.32			14.95
129	TUCO_INT	345/230	336	560	75,800	665.83			75.80		
130	TUCO_INT	345/230	300	560	58,730	515.88		400 75	58.73		40.00
131	TUCO_INT	115/69	50	84 150	18,300		242.27	160.75		39.09	18.30
132 133	TUCO_SVC WHEELER	230/13 230/120	90 150	250	39,090 62,631		343.37 550.15			62.63	
134	WOLFFORTH	230/120	90	150	80,106		703.65			80.11	
135	YOAKUM	230/115	90	150	69,850		613.56			69.85	
136	YOAKUM	230/115	90	150	69,990		614.79			69.99	
						Total Ene	ergy Losses	s, MWH	Total Den	nand Losse	es, KW
						345 Kv	230 kV	115 kV	345 Kv	230 kV	115 kV
	Hours in Period	8784				4,741	21,905	17,276	519	2,539	1,755

APPENDIX H USE BY LOSS LEVEL

SOUTHWESTERN PUBLIC SERVICE COMPANY SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS

TOTAL SYSTEM FOR THE YEAR ENDED: DECEMBER 31, 2016

KWH ENER	KWH ENERGY DELIVERED AT THE METER	T THE METER	,								(754,595,533)	
	Total Loss Level 6	Total Loss Level 5	Total Loss Level 4	Total Loss Level 3	Total Loss Level 2	Total Retail	Wholesale 4	Wholesale 3	Wholesale 2	Wholesale "@generator	Total Wholesale	Total System Energy
JANUARY 16	411,818,678	239,445,487	290,019,002	112,669,984	575,096,269	1,629,049,420	6,119,318	212,667,734	524,698,747	994,014	744,479,813	2,373,529,233
FEBRUARY	306,426,002	215,233,752	284,345,595	106,304,866	536,379,707	1,448,689,922	5,703,770	197,239,396	482,072,342	1,215,180	686,230,688	2,134,920,610
APRIL	253,608,063	236,825,335	295,917,648	109,790,407	556,075,883	1,452,217,336	5,705,558	296,724,173	523,645,813	1,265,402	827,340,946	2,279,558,282
MAY	298,475,419	256,989,020	299,289,662	109,428,376	578,306,297	1,542,488,774	6,046,872	289,265,841	568,654,679	577,605	864,544,997	2,407,033,771
# N	406,851,507	300,650,169	296,223,566	107,902,611	579,057,304	1,690,685,157	8,904,907	353,598,849	666,014,213	029'199	1,029,179,589	2,719,864,746
ALIGHST	307,096,036	329 159 595	310,909,040	114 821 152	610.492.1,193	1,903,332,703	10,781,338	516 345 423	740.498.309	830 898	1 267 721 184	3,329,069,760
SEPTEMBER	321,160,706	262,516,234	301,336,391	111.072.247	580,209,111	1.576,294,689	7,429,123	187,514,928	538,853,371	449.071	734.246.493	2,310,541,182
OCTOBER	272,553,649	259,186,166	314,376,279	107,582,599	594,932,988	1,548,631,681	6,546,395	245,790,726	509,808,761	247,567	762,393,449	2,311,025,130
NOVEMBER DECEMBER	289,834,829 390,432,501	249,034,387 257,837.374	297,597,740 300.794.911	105,655,493 106,053,432	574,825,618 576,070,355	1,516,948,067	6,160,347 6,585,523	222,508,772 253,521,253	470,704,438 523.090,845	24,434 35,450	699,397,991 783,233,071	2,216,346,058 2.414,421,644
TOTAL YEAR	4.161,409,160	3.205.486.688	3.618.157.286	1.318,901,280	6.940.287.923	19,244,242,337	86,637,128	3.623,599,836	6.880.956.843	8.295.082	10,599,488,889	29.843.731.226
SOUTHWES SCHEDULE TOTAL	SOUTHWESTERN PUBLIC SERVICE COMPANY SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLAS: TOTAL SYSTEM	RVICE COMPAN T YEAR DATA B	NY IY RATE CLAS:	S			3,704,794,414	4,942,501,116	13,821,244,766			
FOR THE YI	ADDOSTED CLASS CONSIDER I FEAN CHIMAND FOR THE YEAR ENDED: DECEMBERS IS THE METER HOME EVICTING FOR EACH DOS	EMBER 31, 201	9	CHILDING	0 TO VE 000 C	ģ						
	Total Loss Level	Total Loss Level 5	Total Loss Level	Total Loss Level	Total Loss Level	Total Retail	Total Wholesale 4	Total Wholesale 3	Total Wholesale 2	Total Wholesale "@generator	Total Wholesale	Total System Demand
SALIAN VA	330 937	336 206	440 755	160 405	753 704	0 404 979	0 465	323 420	024 020	120	24.42	039.0
JANOAR TO	740,564	387,350	412,735	162,423	753,761	2,484,573	0,403	323,429	070,470	1/0	1,136,142	3,608,60
MADELLA	749,364	360 847	424,336	162,962	712,650	2,432,301	9,210	366 249	76.5 24.2	132	1,136,301	3,000,002
NOW O	563.608	301,017	410,030	141 457	789 852	2 320 700	102.0 088.8	300,240	900.313	- 00°, c	1,142,149	9 683 6
MAY	757 242	450 157	453,700	138 811	766 302	2,520,103	12 785	430,421	1 054 747	חססיים -	1 408 245	4,002,00
	242,161	450,137	404,321	150,011	063 300	2,077,123	16,783	700,002	1,400,47	03760	2,000,243	4,073,366
Z >	1,009,093	640,746	437,103	155 553	834 859	3,165,282	17.363	034 032	1,409,556	604,7	2,009,111	5,007,43
AUGUST	1.059.316	609.767	467.850	170.214	851.140	3.158.287	16.535	935.031	1.315.108	422	2.267.096	5.425.383
SEPTEMBER	854.761	498.727	409,245	164,359	850,193	2,777,286	14,873	333,502	1,005,683	984	1.355,042	4,132,32
OCTOBER	613,085	446,605	480,798	145,216	785,718	2,471,422	10,345	384,042	824,450	189	1,219,026	3,690,448
NOVEMBER DECEMBER	440,239 823,122	463,422 354,194	436,073 380,230	144,537 156,220	829,025 723,397	2,313,297 2,437,162	11,136 11,398	393,490 398,065	808,463 857,860	42 334	1,213,131 1,267,657	3,526,428 3,704,819
AT Peak Hour	1,114,734	640,746	419,391	155,553	834,859	3,165,282	17,363	934,932	1,409,556	• }	2,361,851	5,527,133
MAX PEAK		1,755,480	480,798	1/0,214	853,290	3,165,282	17,363	935,031	1,409,556	4,381	2,361,851	5,527,13
SOUTHWES	SOUTHWESTERN PUBLIC SERVICE COMPANY	RVICE COMPAN	>									
SCHEDULE	SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLAS:	T YEAR DATA B	3Y RATE CLAS	S								
LOAD FACT	LOAD FACTOR USING KWH DELIVERED AND MAX KW ATT	ELIVERED AND	MAX KW AT T	'HE METER								
FOR THE Y	FOR THE YEAR ENDED: DECEMBER 31, 2016	EMBER 31, 201	9									
	i i											

	AN LINDED. DE	TON THE LEAN ENDED. DECEMBER 31, 2010	2									
ADJUSTED C	OINCIDENT PE	ADJUSTED COINCIDENT PEAK DEMAND AT THE METER USIN	THE METER L	JSING EXISTING	IG EXISTING LOSS FACTORS	S						
	Total Loss Level 6	Total Loss Level 5	Total Loss Level 4	Total Loss Level 3	Total Loss Level 2	Total Retail	Total Wholesale 4	Total Wholesale 3	Total Wholesale 2	Total Wholesale "@generator	Total Wholesale	Total System Demand
JANUARY 16	768.056	397.356	412.755	162,425	753.781	2.494.373	8.465	323.429	824.078	170	1.156.142	3.650,515
FEBRUARY	749,564	361,951	424,358	162,962	753,466	2,452,301	8,210	324.735	823,204	152	1,156,301	3,608,602
MARCH	540,750	360,817	416,098	162,601	712,659	2,192,925	9,207	366,248	762,313	4,381	1,142,149	3,335,074
APRIL	263,698	391,933	433,768	141,457	789,852	2,320,709	8,880	449,421	900,314	3,558	1,362,173	3,682,882
MAY	757,242	450,157	464,521	138,811	766,392	2,577,123	12,785	430,713	1,054,747		1,498,245	4,075,368
JUNE	1,069,093	541,535	457,105	157,320	853,290	3,078,342	16,599	700,985	1,289,058	2,469	2,009,111	5,087,453
JULY	1,114,734	640,746	419,391	155,553	834,859	3,165,282	17,363	934,932	1,409,556		2,361,851	5,527,133
AUGUST	1,059,316	29,767	467,850	170,214	851,140	3,158,287	16,535	935,031	1,315,108	422	2,267,096	5,425,383
SEPTEMBER	854,761	498,727	409,245	164,359	850,193	2,777,286	14,873	333,502	1,005,683	984	1,355,042	4,132,328
OCTOBER	613,085	446,605	480,798	145,216	785,718	2,471,422	10,345	384,042	824,450	189	1,219,026	3,690,448
NOVEMBER	440,239	463,422	436,073	144,537	829,025	2,313,297	11,136	393,490	808,463	42	1,213,131	3,526,428
DECEMBER	823,122	354,194	380,230	156,220	723,397	2,437,162	11,398	398,065	857,860	334	1,267,657	3,704,819
AT Peak Hour	1,114,734	640,746	419,391	155,553	834,859	3,165,282	17,363	934,932	1,409,556		2,361,851	5,527,133
MAX PEAK	1,114,734	640,746	480,798	170,214	853,290	3,165,282	17,363	935,031	1,409,556	4,381	2,361,851	5,527,133

LOAD FACTOR AT THE LOSS LEVEL	RA	r the Loss	LEVEL						
Total	Tot	<u></u>	Total	Total	Total	Total	Total	Total	
Loss	Loss	loss Level	System						
9	9		5	4	3	2	1	Demand	HOURS
JANUARY 16 0.	0	.720676	0.751112	0.802575	0.825421	0.873586	0.873912	0.873912	744
FEBRUARY 0.	Ö	.587364	0.674315	0.755302	0.788656	0.849581	0.850029	0.850029	696 29 days
U	Ö	.681163	0.759563	0.834074	0.862280	0.920747	0.920048	0.920048	744
APRIL 0	0	.624862	0.712783	0.786737	0.836878	0.860021	0.859667	0.859667	720
	0	0.529786	0.618347	0.686761	0.750975	0.793667	0.793857	0.793857	744
_	0	.528552	0.610098	0.674764	0.695772	0.742710	0.742531	0.742531	720
JULY 0	0	.612397	0.666931	0.734996	0.781101	0.809385	0.809562	0.809562	744
AUGUST	_	.543443	0.609974	0.675032	0.706414	0.759056	0.759203	0.759203	744
SEPTEMBER (_	0.521849	0.598943	0.697288	0.726975	0.776614	0.776580	0.776580	720
OCTOBER (_	0.597528	0.674446	0.738991	0.779300	0.841644	0.841691	0.841691	744
NOVEMBER		0.914387	0.828219	0.866342	0.860872	0.872912	0.872911	0.872911	720
DECEMBER	_	0.637542	0.740099	0.818689	0.832588	0.876004	0.875938	0.875938	744
ANNUAL LF		0.424988	0.477745	0.559290	0.542772	0.604185	0.614697	0.614697 0.614697	8784

USE BY LOSS LEVEL APPENDIX H

SOUTHWESTERN PUBLIC SERVICE COMPANY SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS Line No.

TOTAL SYSTEM

FOR THE YEAR ENDED: DECEMBER 31, 2016

KWH ENERGY DELIVERED AT THE METER
Residential - NM Residential

	Residential - NM	Residential	Residential	Total	NM & TX	NM & TX	NM & TX	NM & TX		Total
	Water	RTX & RLNM	RHTX & RHNM	Residential	Small General	Street	Area	Small Muni and	Larg	Loss Level
	Heating				Service	Lighting	Lighting	School Service	Service	9
JANUARY 16		206,412,082	145,317,508	351,729,590	37,790,297	3,996,739	3,431,824	.,	11,784,993	411,818,678
FEBRUARY		154,814,527	99,594,841	254,409,369	30,777,989	3,738,885	3,210,416	.,	11,831,628	306,426,002
MARCH		140,862,410	80,070,342	220,932,752	30,501,449	3,996,739	3,431,824	•	12,851,485	274,044,235
APRIL		133,520,374	68,171,570	201,691,944	30,508,950	3,867,812	3,321,120	•	12,045,938	253,608,063
MAY		166,311,838	75,982,323	242,294,161	33,743,022	3,996,739	3,431,824	.,	12,760,096	298,475,419
JUNE		240,357,451	100,559,271	340,916,722	41,867,532	3,867,812	3,321,120	•	14,371,957	406,851,507
JULY		303,377,266	122,396,782	425,774,048	55,311,750	4,010,381	3,437,253	.,	16,340,435	507,898,858
AUGUST		253,154,894	101,177,980	354,332,874	48,855,990	4,010,381	3,437,253	.,	14,881,545	428,304,713
SEPTEMBER		188,659,155	76,249,227	264,908,382	34,491,249	3,881,014	3,326,374	•	12,202,398	321,160,706
OCTOBER		154,662,037	65,113,598	219,775,634	30,642,944	4,010,381	3,437,253	2,281,667	12,405,769	272,553,649
NOVEMBER		158,701,686	80,634,409	239,336,094	29,814,985	3,881,014	3,326,374	•	11,124,126	289,834,825
DECEMBER		211,189,576	121,593,034	332,782,610	35,957,942	4,010,381	3,437,253	•	11,275,985	390,432,501

SOUTHWESTERN PUBLIC SERVICE COMPANY

TOTAL YEAR

SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS

TOTAL SYSTEM

ADJUSTED CLASS COINCIDENT PEAK DEMAND FOR THE YEAR ENDED: DECEMBER 31, 2016

768,056 749,564 540,750 563,698 757,242 1,069,093 1,114,734 1,059,316 854,761 613,039 823,122 1,114,734 1,114,734 Total Loss Level TX Large Municipal Service 19,642 16,500 17,412 20,501 20,738 21,565 28,234 23,196 18,411 17,571 18,302 18,823 28,234 28,234 Small Muni and School Series 5,193 4,601 4,169 2,736 3,748 3,748 4,501 4,501 4,282 3,410 5,160 4,804 5,194 NM & TX Area Lighting 5,390 NM & TX Street Lighting ADJUSTED COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS FACTORS
Residential NM Residential NM 8 TX
Water RTX & RLNM RHTX & RHNM Residential Small General
Heafing 61,122 56,988 45,250 49,912 76,323 75,393 108,913 101,620 66,990 47,173 43,941 62,090 682,099 671,475 473,919 490,549 657,081 968,386 972,784 929,99 765,078 544,783 374,587 972,784 972,784 296,647 312,555 205,400 192,169 211,003 289,848 282,008 271,598 271,598 163,983 163,983 104,300 282,008 312,555 385,452 358,920 268,519 298,379 446,078 678,538 690,776 658,402 541,825 380,801 270,287 APRIL MAY JUNE JULY AUGUST SEPTEMBER OCTOBER NOVEMBER DECEMBER AT Peak Hour MAX PEAK JANUARY 16 FEBRUARY MARCH

USE BY LOSS LEVEL APPENDIX H

SOUTHWESTERN PUBLIC SERVICE COMPANY SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS Line No.

TOTAL SYSTEM

FOR THE YEAR ENDED: DECEMBER 31, 2016

290,019,002 284,345,595 307,275,100 295,917,648 299,289,662 296,223,566 316,969,540 314,011,852 301,336,391 314,376,279 297,597,740 Total Loss Level NM & TX Primary General Service 277,931,882 274,472,103 295,498,694 278,492,154 281,056,957 278,195,721 293,755,140 292,795,512 282,849,387 281,738,408 101,005 13,772 115,790 16,759 134,799 16,769 11,591 12,976 12,976 12,976 12,978 12,837 759,389 Primary Low Load 190,911 97,754 117,964 118,459 97,208 122,308 111,565 111,852 107,382 130,046 TX Primary QF Stand F ,493,607 TX Primary LGS SAS-8 3,683,994 3,662,443 3,853,127 3,030,499 3,499,170 3,792,823 3,948,912 3,948,912 3,948,912 3,948,912 2,917,433 2,977,433 15,374,283 207,572 209,398 214,908 229,256 241,853 253,817 291,553 315,884 300,147 262,614 262,614 187,880 TX LSSTX - Pri 2,612,153 TX LMSTX - Pri arge Munich 2,188,310 2,854,454 2,633,848 2,759,627 3,435,884 4,027,282 3,100,136 2,594,945 1,917,392 1,735,944 31,397,184 6,124,991 3,701,815 4,620,164 11,396,673 11,406,244 10,406,244 14,826,497 11,776,750 11,776,750 12,282,909 11,222,207 8,865,380 CRMWA TX Interruptible SAS-4 119,535,151 239,445,487 215,233,752 236,445,146 226,899,020 300,650,169 363,164,023 329,169,595 229,189,595 229,186,166 249,034,387 257,887,374 3,205,486,687 Total Loss Level 14,702,014 13,697,862 12,820,539 13,066,966 13,066,967 12,891,103 14,752,879 16,945,248 16,945,248 16,188,967 14,406,732 14,406,732 12,367,162 TX LSSTX 214,991,258 190,782,740 207,692,632 207,302,890 224,789,925 226,246,677 226,246,37,385 230,852,242 230,852,242 230,871,985 230,871,985 226,302,665 236,515,551 NM & TX Sec General KWH ENERGY DELIVERED AT THE METER NM NM Inrigation Municipal and Schot 8,774,453 8,207,735 8,561,678 8,883,421 10,006,879 10,549,468 12,461,836 12,461,836 12,461,836 12,461,836 12,60,621 8,226,042 8,226,042 8,266,621 8,266,621 116,206,036 977,762 2,545,415 6,370,296 7,572,058 10,962,920 14,315,816 9,913,819 4,932,125 4,932,125 1,874,033 1,085,803 73,323,473 Irrigation Service JANUARY 16
FEBRUARY
MARCH
MAY
JUNE
JUNE
JUNE
JUNE
SEPTEMBER
OCTOBER
NOVEMBER
DECEMBER **FOTAL YEAR**

SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS SOUTHWESTERN PUBLIC SERVICE COMPANY

TOTAL SYSTEM

ADJUSTED CLASS COINCIDENT PEAK DEMAND FOR THE YEAR ENDED: DECEMBER 31, 2016

Total Loss Level NM & TX Primary General Service 389,511 405,684 390,044 406,543 423,579 425,482 392,123 432,892 381,256 451,328 407,649 392,123 451,328 26 Primary Low Load 325 168 140 32 34 34 146 459 459 459 140 83 TX Primary QF Stand by 5,172 6,612 5,419 5,650 3,580 3,580 5,129 5,172 5,172 5,172 5,172 5,120 5,612 5,612 Primary LGS 519 456 524 388 388 425 604 579 680 488 496 604 Ę. TX LSSTX - F Large Sch TX LMSTX - Pri Large Municipal 2,964 3,052 3,867 4,483 5,156 6,958 6,958 3,577 3,577 3,155 2,898 6,958 13,999 9,929 15,853 18,727 20,888 20,795 14,425 24,255 18,612 18,646 17,903 14,425 24,255 FOR THE YEAR ENDED: DECEMBER 31, 2010
FOR THE YEAR ENDED: DECEMBER 31, 2010
ADJUSTED COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS FACTORS
ADJUSTED COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS LEVEL INFORMUTION AT THE METER USING EXIST CRAWATX

INFORMATION AND THE METER USING EXIST CRAWATX

INFORMATION AND THE METER USING EXISTING LOSS FACTORS

ORDER TO THE METER USING EXISTING LOSS FACTORS

ORDER TO THE METER USING EXISTING LOSS FACTORS

ORDER TO THE METER USING EXISTING FACTORS

ORDER TO THE METER USING FACTORS

ORDER TO THE METER USING EXISTING FACTORS

ORDER TO THE METER USING FACTORS

ORDER TO T 397,356 361,951 360,817 391,933 450,157 541,535 640,746 609,767 446,605 463,422 354,194 640,746 36,774 29,832 31,267 22,094 22,111 21,575 30,572 31,042 36,704 36,704 36,704 36,704 36,704 36,704 36,704 36,704 30,572 TX LSSTX Large School 345,139 316,391 310,004 342,863 393,826 480,501 567,327 537,148 427,904 396,008 406,768 567,327 14,731 14,450 12,863 15,724 18,062 21,400 23,942 23,425 24,697 18,583 22,268 712 1,279 6,684 11,252 16,159 18,059 18,059 18,059 18,152 9,423 6,366 6,366 5,352 1,629 18,905 18,905 APRIL MAY JUNE JULY AUGUST SEPTEMBER OCTOBER NOVEMBER DECEMBER JANUARY 16 FEBRUARY MARCH AT Peak Hour MAX PEAK

412,755 424,358 416,098 433,768 464,521 457,105 467,850 409,245 480,798 436,073 380,230

419,391 480,798

APPENDIX H USE BY LOSS LEVEL

Line No. SOUTHWESTERN PUBLIC SERVICE COMPANY
1 SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS

TOTAL SYSTEM FOR THE YEAR ENDED: DECEMBER 31, 2016

		Sub-Trans.	Sub-Trans.	Total	Transmission	Transmission	Transmission	Total
		res	Standby	Loss Level	res	Ŗ	res	Loss Level
		Standard		3	Standard		Generation	2
_								
0	JANUARY 16	112,596,022	73,962	112,669,984	560,475,226	14,621,043		575,096,269
_	FEBRUARY	106,006,863	298,003	106,304,866	522,815,224	13,564,483		536,379,707
~	MARCH	114,132,955	1,108,069	115,241,024	562,528,780	13,391,812		575,920,592
m	APRIL	106,475,977	3,314,430	109,790,407	542,216,069	13,859,814		556,075,883
*	MAY	109,373,566	54,810	109,428,376	564,665,497	13,640,800		578,306,297
10	JUNE	107,859,487	43,124	107,902,611	564,136,895	14,920,409		579,057,304
'n	JULY	112,184,602	194,487	112,379,089	586,728,435	16,192,758		602,921,193
_	AUGUST	112,493,510	2,327,642	114,821,152	595,004,183	15,488,423		610,492,606
m	SEPTEMBER	111,067,837	4,410	111,072,247	567,338,569	12,870,542		580,209,111
6	OCTOBER	107,552,453	30,146	107,582,599	580,964,046	13,968,942		594,932,988
0	NOVEMBER	102,284,646	3,370,847	105,655,493	560,571,541	14,254,077		574,825,618
_	DECEMBER	105,685,021	368,411	106,053,432	562,708,759	13,361,596		576,070,355
<u>~</u>								
~	TOTAL YEAR	1,307,712,939	11,188,341	1,318,901,280	6,770,153,224	170,134,699		6,940,287,923

Sub-Times Sub-Times Sub-Times Class	KWH ENERG	iY DELIVERED A	T THE METER					
1,12,096,022 1,09,004 1,09,		Sub-Trans. LGS Standard	Sub-Trans. Standby	Total Loss Level 3	Transmission LGS Standard	Transmission QF	Transmission LGS Generation	Total Loss Level 2
114, 122, 894 (1974) (1	JANUARY 16	112,596,022	73,962	112,669,984	560,475,226	14,621,043	,	575,096,269
107, 108, 478 108,	FEBRUARY	106,006,863	298,003	106,304,866	522,815,224	13,564,483		536,379,70
107,559,487 43,187 104,082 71,580,489 43,020,489 14,920,489 14,920,489 14,920,489 14,920,489 14,920,489 11,448,521 14,4487 11,273,780 99,6278,483 14,680,423 14,680,423 14,480,433 14,480,433 14,480,433 14,480,433 14,480,433 14,480,433 14,480,433 14,480,433	APRIL	114,132,955	3.314.430	115,241,024	542.216.069	13,391,812		556.075.883
10,1286.28	MAY	109,373,566	54,810	109,428,376	564,665,497	13,640,800		578,306,297
11.06F 287 2.776	# > I	107,859,487	43,124	107,902,611	586 728 435	14,920,409		602 921 19
11,007,123, 4410 11,02,247 58,738,589 580,954,06 19,805,522 17,526,584 580,954,06 19,805,522 17,526,584 580,954,06 19,805,523 17,526,584 19,805,738,702 13,815,996 1,815,599 1,815	AUGUST	112,493,510	2,327,642	114,821,152	595,004,183	15,488,423		610,492,60
102.284.646 3.970.847 106.655.483 580.571.547 10.50.655.483 580.571.547 10.50.5427	SEPTEMBER	111,067,837	4,410	111,072,247	567,338,569	12,870,542		580,209,117
1307/12.299	NOVEMBER DECEMBER	102,284,646	3,370,847 3,88.411	105,655,493 106,053,432	560,571,541 562,708,759	14,254,077		574,825,618 576,070,355
SYSTEM CLASS COINCIDENT PEAK DEMAND CLASS COINCIDENT PEAK DEMAND CLASS COINCIDENT PEAK DEMAND CLASS COINCIDENT PEAK DEMAND CONCIDENT PEAK DEMAND COINCIDENT PEAK	TOTAL YEAR	1,307,712,939	11,188.341	1.318.901.280	6.770.153.224	170.134.699		6.940.287.923
CLASS COINCIDENT PEAK DEMAND SAR ENDED: DECEMBER 31, 2016 COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS FACTORS COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS FACTORS Sub-Trans. Sub-Trans. LOSS Connection LOSS Connection LOSS Connection Transmission Transm	SOUTHWEST SCHEDULE:	TERN PUBLIC SE ADJUSTED TES	RVICE COMPA	NY BY RATE CLASS	l			
COINCIDENT PEAK DEMAND AT THE METER USING EASS FACTORS Sub-Trare. Sub-Trare. Total Loss Level Transmission	ADJUSTED C FOR THE YE	CLASS COINCIDE AR ENDED: DEC	ENT PEAK DEM SEMBER 31, 20	AND 16				
Sub-Trans. Total Transmission Transmission Transmission Transmission Tr	ADJUSTED C	COINCIDENT PEA	K DEMAND AT	THE METER US	ING EXISTING L	OSS FACTORS		
162,425		Sub-Trans. LGS Standard	Sub-Trans. Generation QF	Total Loss Level 3	Transmission LGS Standard	Transmission Standby QF		Total Loss Level 2
162,662	25	160 405		169 495	350 575	902.9		7697
161 694 907 142 601 706 154 6 656 141 457 159 503 10 349 159 503 10 349 159 503 10 349 159 503 10 349 159 503 10 349 159 503 10 349 159 503	FEBRUARY	162,962		162.962	745,561	7,904		753,46
14,457 - 14,457 779,503 10,349 - 15,520	MARCH	161,694	206	162,601	706,154	6,505		712,65
155,320	APRIL	141,457		141,457	779,503	10,349		789,85
165,653	ENI.	157.320		158,811	844.372	6,075		766,38 853,29
164,389 164,389 164,389 22,601	JULY	155,553		155,553	805,486	29,373		834,85
145.35	AUGUST	163,977	6,237	170,214	828,539	22,601		851,14
144.537 804.178 24.847 - 144.537 804.178 24.847 - 144.537 804.178 - 145.069 - 165.069	OCTOBER	145,216		145,216	763,667	22,051		785,71
165,563	NOVEMBER	144,537	1.548	144,537	804,178	24,847		829,02
166.553								
	AT Peak Hour MAX PEAK	155,553 164,359	6,237	155,553 170,214	805,486 844,372	29,373 29,373		834,85 853,29

APPENDIX H USE BY LOSS LEVEL

SOUTHWESTERN PUBLIC SERVICE COMPANY SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS Line No.

TOTAL SYSTEM

FOR THE YEAR ENDED: DECEMBER 31, 2016

744,479,814 686,230,688 774,983,603 827,340,946 864,544,996 14,023,179,589 14,025,770,05 1,267,721,184 734,246,492 734,246,492 734,246,492 734,246,492 734,246,492 734,246,492 734,246,492 734,249,699,397,991 994,014 1,215,180 1,265,837 1,265,402 577,605 661,620 728,004 830,898 449,071 247,567 24,434 35,450 524,698,747 482,072,342 523,645,813 568,654,679 666,014,213 817,704,745 740,488,309 538,853,371 470,704,438 523,090,945 Total Wholesale KWH ENERGY DELIVERED AT THE METER
Total
Wholesale Wholesale
Loss Level LL3 212,667,734 197,239,396 251,879,163 296,724,173 289,265,841 355,598,849 596,542,978 516,345,423 187,514,928 2245,790,726 222,508,772 223,508,772 6,119,318 6,627,423 6,627,423 6,705,558 6,04,607 10,761,338 10,046,554 7,429,123 6,566,395 6,160,347 6,585,523 JANUARY 16
FEBRUARY
MARCH
APRIL
MAY
JUNE
JUNE
JUNE
AUGUST
SEPTEMBER
OCTOBER
DCCEMBER
DECEMBER

SCHEDULE: ADJUSTED TEST YEAR DATA BY RATE CLASS SOUTHWESTERN PUBLIC SERVICE COMPANY

10,599,488,890

492,134,601

344,822,539

147,312,062

TOTAL YEAR

TOTAL SYSTEM

ADJUSTED CLASS COINCIDENT PEAK DEMAND FOR THE YEAR ENDED: DECEMBER 31, 2016

ADJUSTED COINCIDENT PEAK DEMAND AT THE METER USING EXISTING LOSS FACTORS

	Total	Total	Total	@ Generation	Total	
		Wholesale	Wholesale	Wholesale	Wholesale	
	Loss Level 4	LL3	LL2	LL1		
JANUARY 16	8,465	323,429	824,078	170	1,156,142	
FEBRUARY	8,210	324,735	823,204	152	1,156,300	
MARCH	9,207	366,248	762,313	4,381	1,142,149	
APRIL	8,880	449,421	900,314	3,558	1,362,173	
MAY	12,785	430,713	1,054,747		1,498,245	
JUNE	16,599	700,985	1,289,058	2,469	2,009,111	
JULY	17,363	934,932	1,409,556		2,361,850	
AUGUST	16,535	935,031	1,315,108	422	2,267,095	
SEPTEMBER	14,873	333,502	1,005,683	984	1,355,042	
OCTOBER	10,345	384,042	824,450	189	1,219,027	
NOVEMBER	11,136	393,490	808,463	42	1,213,131	
DECEMBER	11,398	398,065	857,860	334	1,267,657	
AT Peak Hour	17,363	934,932	1,409,556		2,361,850	
MAX PEAK	17,363	935,031	1,409,556	4,381	2,361,850	

Line No.	1	Voltage High Side, kV 2	Low Side, kV 3	Ratings Nominal MVA 4	Max MVA 5	No Load Losses WATTS 6	Full Load Losses WATTS 7	Low Side Class 8	Verify Flag R,L,E 9	Exclude Flag 10	Primary Load Factor 11	No Load Losses MWH 12	Full Load Losses MWH 13	Number of Feeder Circuits 14	Percent Transf. Excluded 15
1	34TH STREET	115	13.2	22.4	37.3	19,005	64,617	13.2	R,L	!	0.5592897 0.55929	166.94	317.45	4	
2 3	ADAIR AIKEN RURAL	68.8 67	13.09 12.5	10 2.5	14 2.5	12,573 4,608	25,896 13,940	12.5 12.5	R,E R,E	i	0.55929 0.55929	110.44 40.48	127.22 68.48	1 1	
4 5	ALLMON ALLRED	67 115	12.5 12.5	7.5 12	9.38 20	10,895 19,630	43,006 57,040	12.5 12.5	R,L R,L	I E	0.55929 0.55929	95.70 34.49	211.28 56.05	1 2	80
6 7	AM-FRAC AMHERST	115 67	2.4 2.4	5.6 3.75	7 4.687	5,677 7,840	24,595 28,640	2.4 2.4	R,L R.L	1	0.55929 0.55929	49.87 68.87	120.83 140.70	0 2	
8	ARROWHEAD	115	13.2	15	25	12,450	55,570	13.2	R,L	i	0.55929	109.36	273.00	2	
9 10	ARTESIA COUNTRY CLUB ARTESIA S RURAL	67 69	12.5 13.2	7.5 11.2	9.38 14	12,000 8,663	40,000 46,721	12.5 13.2	R,E R,L	- 1	0.55929 0.55929	105.41 76.10	196.51 229.53	2	
11 12	ARTESIA TOWN ARTESIA WEST 13th St.	66 67	4.16 4.16	5 7.5	5 11.26	10,526 9,800	32,485 55,797	4.16 4.16	R,E R.L	1	0.55929 0.55929	92.46 86.08	159.59 274.12	3 2	
13	BAILEY PUMP	67	12.5	5	5.6	11,000	35,000	12.5	R,E	į	0.55929	96.62	171.95	1	
14 15	BAINER BARWISE	66 68.8	4.16 13.09	5 3.75	5 4.2	10,526 7,760	32,485 27,560	4.16 12.5	R,E R,L	i	0.55929 0.55929	92.46 68.16	159.59 135.40	1 2	
16 17	BATTLE AXE T1 BATTLE AXE T2	115 115	22.86 22.86	30 30	50 50	19,900 19,600	89,300 88,400	22 22	R,L R.L	-	0.55929 0.55929	174.80 172.17	438.71 434.29	3 3	
18 19	BENNETT BENSING	115 118	13.2 13.2	16.8 17.5	28 29.5	11,770 11,700	55,780 67,500	12.5 12.5	R,L R,L	1	0.55929 0.55929	103.39 102.77	274.04 331.61	3	
20	BOARDMAN	69	13.2	12	20	9,410	45,960	12.5	R,L	Ė	0.55929	67.78	185.15	2	18
21 22	BOOKER 4.16 KV BOWERS	69 67	4.2 13.8	3.75 7.5	3.75 9.375	7,900 19,800	24,500 56,515	4.16 13.2	R,E R,L	- 1	0.55929 0.55929	69.39 173.92	120.36 277.65	3 3	
23 24	BRASHER BRISCOE	115 66	13.2 22	15 3	25 3.92	13,500 5,697	57,700 15,131	13.2 22	R,L R,E		0.55929 0.55929	118.58 50.04	283.47 74.33	3 2	
25 26	BROWNFIELD SWITCH STATION BUCKEYE	67 115	22.9 12.5	5 7.5	5 10.5	13,410 20,620	31,360 74,550	22 12.5	R,L R,L	į	0.55929 0.55929	117.79 181.13	154.07 366.25	1 3	
27	BUFFALO	69	13.2	5	6.25	4,595	22,296	13.2	R,L	į	0.55929	40.36	109.54	2	
28 29	BURNETT BUSH	69 115	13.2 13.8	11.2 15	14 25	8,110 24,880	45,840 60,701	13.2 13.2	R,L R,L	!	0.55929 0.55929	71.24 218.55	225.20 298.21	2	
30 31	BYRD CAMEX	115 67	4.2 2.4	13.5 5	22.4 7	10,602 13,000	52,896 30,000	4.16 2.4	R,L R.L	1	0.55929 0.55929	93.13 114.19	259.87 147.38	0	
32	CAMEX 115	118	13.2	16.8	28	12,650	71,450	13.2	R,L	Ė	0.55929	0.00	0.00	2	100
33 34	CAMPBELL STREET CANADIAN	115 67	12.5 2.4	15 10	25 10	18,192 15,350	65,727 55,490	12.5 2.4	R,L R,L	- 1	0.55929 0.55929	159.80 134.83	322.90 272.61	2 4	
35 36	CANYON EAST CANYON WEST	115 115	13.2 13.2	15 15	25 25	12,700 13,340	58,300 50,960	13.2 13.2	R,L R,L	!	0.55929 0.55929	111.56 117.18	286.42 250.36	2	
37	CAPITAN CARLISLE	69	13.2	15 33.3	25 36.6	10,610	57,270 58.368	13.2	R,L R.E	į	0.55929	93.20	281.36	3	
38 39	CARLSBAD WATER	115 67	12.5	3.75	3.75	12,592 6,912	20,909	12.5	R,E	i	0.55929 0.55929	110.61 60.72	286.75 102.72	2	
40 41	CARSON CO CEDAR LAKE EAST	115 66	13.8 12.5	10 2	12.5 2	16,667 4,000	56,431 25,000	13.2 12.5	R,L R.E	I E	0.55929 0.55929	146.40 0.00	277.23 0.00	2 1	100
42 43	CENTRE ST CHANNING T1	67 230	13.8 34.5	12 16.8	22.4 28	20,560 17,700	43,351 63,100	13.2 33	R,L R,L	- !	0.55929 0.55929	180.60 155.48	212.97 310.00	2 2	
44	CHANNING T2	230	34.5	16.8	28	17,700	63,100	33	R,L	į	0.55929	155.48	310.00	1	
45 46	CHERRY CHINA DRAW T1	115 115	13.2 12.47	15 16.8	25 28	18,449 11,700	67,706 67,200	13.2 12.5	R,L R,L	- 1	0.55929 0.55929	162.06 102.77	332.63 330.14	2	
47 48	CHINA DRAW T2 CLIFFSIDE	115 68.8	12.47 4.36	16.8 7.5	28 10.5	11,200 12,678	65,800 44,698	12.5 4.16	R,L R.L	-	0.55929 0.55929	98.38 111.36	323.26 219.59	2	
49 50	COBLE COBURN CREEK	67 118	12.5 13.2	10 16.8	11 28	16,500 11,700	55,000 69,000	12.5 13.2	R,E R,L	E	0.55929 0.55929	82.61 102.77	154.02 338.98	2 2	43
51	CONWAY	115	13.8	12	20	21,840	48,390	13.2	R,L	į	0.55929	191.84	237.73	2	
52 53	COOPER RANCH CORTEZ	115 115	13.2 4.2	12 5	22.4 6.25	17,615 10,530	56,447 27,280	12.5 4.16	R,E R,L	-	0.55929 0.55929	154.73 92.50	277.31 134.02	2 0	
54 55	COTTONWOOD #1 COULTER	66 115	12.5 13.8	1.5 15	1.88 25	3,158 25,000	9,745 75,000	12.5 13.2	R,E R,L	-	0.55929 0.55929	27.74 219.60	47.88 368.46	2	
56 57	COUNTY LINE CRMWA #1	69	12.47	18.75	25 9.37	36,600	89,810	12.5	R,L R.L	Ė	0.55929	80.37 180.01	110.30	1	75
58	CRMWA #2	115 115	4.16 4.16	7.5 5	6.25	20,493 16,255	50,307 36,145	4.16 4.16	R,L	i	0.55929 0.55929	142.78	247.15 177.57	0	
59 60	CRMWA #3 CRMWA #4	115 115	4.16 4.16	5 5	6.25 6.25	14,481 15,785	35,758 35,824	4.16 4.16	R,L R,L	-	0.55929 0.55929	127.20 138.66	175.67 176.00	0	
61 62	CRMWA 21 (Adobe Creek) 13 CRMWA 21 (Adobe Creek) 4	67 67	13.2 4.2	10 7.5	14 8.4	23,000 10,000	80,000 32,000	13.2 4.16	R,E R.E	- !	0.55929 0.55929	202.03 87.84	393.02 157.21	1 1	
63	CRMWA 22	69	4.2	3.75	4.687	7,900	24,500	4.16	R,E	į	0.55929	69.39	120.36	0	
64 65	CRMWA 23 CROUSE HINDS	67 115	13.8 13.8	15 12	28 20	24,060 19,600	66,861 63,100	13.2 13.2	R,L R,L	i	0.55929 0.55929	211.34 172.17	328.47 310.00	0	
66 67	CURRY CO DALHART 12.5 KV	67 67	24 12.5	12 12	20 22.4	18,465 15,855	52,230 50,503	22 12.5	R,L R.L	-	0.55929 0.55929	162.20 139.27	256.60 248.11	4 2	
68 69	DALHART 2.4 KV DALHART 35 KV	67 67	2.4 34.5	3.75 7.5	4.68 7.5	11,960 17,590	38,450 42,475	2.4 33	R,E R,L	- !	0.55929 0.55929	105.06 154.51	188.90 208.67	4 2	
70	DAMRON	69	13.2	7.5	10	17,250	55,850	13.2	R,L	į	0.55929	151.52	274.38	1	
71 72	DAWN DEAFSMITH	115 115	13.2 13.8	7.5 12	9.375 20	7,870 19,600	23,170 63,100	13.2 13.2	R,L R,E	Ë	0.55929 0.55929	69.13 0.00	113.83 0.00	2 1	100
73 74	DEXTER 34.5 KV DEXTER 4.16 KV	69 66	34.5 4.2	5.6 3.75	7 3.75	7,047 7,894	32,076 24,364	33 4.16	R,L R,E	-	0.55929 0.55929	61.90 69.34	157.58 119.69	1 2	
75 76	DIEKEMPER DIMMITT F	66 67	4.2	1.5	1.5	2,105	6,497	4.16	R,E	į	0.55929	18.49	31.92 339.82	1 2	
77	DIMMITT S	67	12.5	10	12.5	9,216	27,879	12.5	R,E	i	0.55929	80.96	136.97	2	
78 79	DOLLARHIDE DOSS 12.5 KV	115 69	13.2 12.5	12 16.8	22.4 28	11,100 9,851	46,800 71,031	12.5 12.5	R,E R,L	1	0.55929 0.55929	97.50 86.53	229.92 348.96	3	
80 81	DOSS 22 KV DRINKARD	67 115	24.9 13.2	12 12	20 22.4	18,330 11,190	62,470 38,840	22 13.2	R,L R,L	!	0.55929 0.55929	161.01 98.29	306.90 190.81	2	
82	DUMAS 19TH 12.5 KV	115	12.5	12	20	19,400	63,400	12.5	R,L	į	0.55929	170.41	311.47	3	
83 84	DUMAS 19TH 35 KV DUVAL #3	115 67	34.5 4.2	12 5	20 7	20,700 10,526	51,675 32,485	33 4.16	R,L R,L	i	0.55929 0.55929	181.83 92.46	253.87 159.59	2 1	
85 86	EAST CLOVIS EAST DENVER CITY	118 67	13.2 12.5	16.8 10	28 12.5	8,768 16,500	67,351 55,000	12.5 12.5	R,L R,E	i i	0.55929 0.55929	77.02 144.94	330.88 270.20	3	
87 88	EAST LEVELLAND EAST PLAINVIEW	69 68.8	13.2	12 15	22.4 16.8	9,400 19,370	42,300 71,767	12.5 12.5	R,E R,L	1	0.55929 0.55929	82.57 170.15	207.81 352.58	2	
89	EAST PLANT	115	13.2	15	28	11,415	59,261	13.2	R,L	į	0.55929	100.27	291.14	4	
90 91	EAST SANGER ELWOOD	115 67	12.5 12.5	12 10	20 12.5	19,859 16,500	64,143 55,000	12.5 12.5	R,L R,E	!	0.55929 0.55929	174.44 144.94	315.12 270.20	2 1	
92 93	ESTACADO #1 ESTACADO #2	115 115	13.2 13.2	15 15	28 28	11,680 15,000	52,670 55,700	13.2 13.2	R,L R,L	- 1	0.55929 0.55929	102.60 131.76	258.76 273.64	3	
94	ETTER RURAL E. ETTER RURAL W	115	34.5	12	20	23,520	49,700	33	R,L	Ē	0.55929	142.55	168.47	2	31
95 96	EUNICE	115 115	34.5 13.2	15 15	25 25	15,250 11,750	64,030 52,460	33 12.5	R,L R,L	E !	0.55929 0.55929	92.43 103.21	217.05 257.73	1	31
97 98	EXELL FAIN	115 115	12.5 12.5	10 7.5	12.5 9.375	29,500 11,480	65,000 45,380	12.5 12.5	R,E R,L	!	0.55929 0.55929	259.13 100.84	319.33 222.94	2 1	
99 100	FARMERS FARWELL	115 67	13.2	15 2.5	25 2.5	18,239 6,334	65,335 19,792	13.2	R,L R,E	i	0.55929 0.55929	160.21 55.64	320.98 97.23	3	
100		37	2.7	2.3	2.3	3,304	.5,132	2.7	,∟		0.00029	33.04	31.23	-	

10 PETAL COLUMN 10 12 10 12 15 15 15 15 15 15 15	Line No.	1	Voltage High Side, kV 2	Low Side, kV 3	Ratings Nominal MVA 4	Max MVA 5	No Load Losses WATTS 6	Full Load Losses WATTS 7	Low Side Class 8	Verify Flag R.L,E 9	Exclude Flag 10	Primary Load Factor 11	No Load Losses MWH 12	Full Load Losses MWH 13	Number of Feeder Circuits 14	Percent Transf. Excluded 15
100 Company 100 Compan										R,L R.I	I F					45
Second 1	103	FRIONA RURAL	115	22.9	12	20	21,350	49,200	22	R,L	Ī	0.55929	187.54	241.71	2	.0
Company Comp											-					
Separation 19		GARZA S	72		11.2	14	9,304	47,534		R,L	!	0.55929				
100 100	108	GREYHOUND	118	13.2	17.5	29.5	1,170	67,500		R,L	i	0.55929	10.28	331.61	1	
111 HOLDECTON 16 12 1 2 10 13 1 5 5 5 5 1 5 5 5 1 5 5 5 5 1 5 5 5 5																
Fig.	111	HART INDUSTRIAL	67	12.5	5	6.25	12,425	31,575	12.5	R,L	į	0.55929	109.14	155.12	2	
Fig. Memory 16 14 12 12 13 14 15 15 15 15 15 15 15											i					
161 MICHARD PARK 162 132 25 416 20 20 100 20 100 120 120 120 120 120 12	114	HEREFORD	118	13.2	16.8	28	16,000	82,000		R,E	1	0.55929	140.54	402.85	2	
DECOLOR 198 12	116	HIGHLAND PARK	115	13.8	25	41.6	30,680	101,010	13.2	R,E	Ė	0.55929	134.75	248.12	2	50
119 HePPLAND 120 110 1											-					
191 March 192 193 194 19	119	HOPI	69	13.2	16.8	28	9,927	70,540	12.5	R,L	į	0.55929	87.20	346.55	3	
120 MC-24											-					
SECK 68 155 68 7.56 11,460 36,464 125 R.E.						5	7,789	20,101		R,L	1	0.55929				
120 1/4/19 1/4 1					6			36,845			i					
Property											!					
1929 NESER 198 132 163 20 16,000 12,50 R.L. 1 0,02003 140,504 140,005 2 141,005 141,	127	KINGSMILL	69	13.2	16.8	28	16,300	67,300	13.2	R,L	į	0.55929	143.18	330.63	5	
120 CHES C											!					
AREA MERCEDITH	130	KITE			12			55,630		R,L	!	0.55929	156.36			
AWRENCE PK E																
LAWRENCE PKW MF 2		LARIAT									!					
BARDAD 115 125 10 125 17615 56,447 125 124 125	135	LAWRENCE PK W #2			15	25		71,126		R,L	i					
Sept											I F					68
LEVELLAND CITY	138	LEHMAN	115	12.5	12	20	19,400	63,000	12.5	R,L	Ī	0.55929	170.41	309.51	2	00
LIPSCOMB 12.5 NV																
LITTLEFELD CUTY 67		LIPSCOMB 12.5 KV		13.2	5.6	7	2,161	6,482	13.2		!	0.55929		31.84		
LIVINGSTON RIDGE											-					
LOCKNEY RURAL											!					
LINN	146	LOCKNEY RURAL	69	12.5	2.5	2.5	4,608	13,940	12.5	R,E	i	0.55929	40.48	68.48	2	
LYONS											-					
MALJAMAR #Z	149	LYONS	67	13.8	12	20	21,550	52,560	13.2	R,L	į	0.55929	189.30	258.22	2	
MALLET 152 MALLET 157 13.8 5 5 10.641 39.077 12.5 R.L. 1 0.55922 93.47 19.98 2																57
McCLELLAN (GROOM PLMP STATION)	152										!	0.55929				
166 MCLEAN RUBAL		McCLELLAN (GROOM PUMP STATION)									i					
IDD AM 83 - In Switcher area											I F					57
159 MIDDLETON	157	MID AM #3 -in Swisher area	67	2.4	5	5.6	14,150	42,000	2.4	R,E		0.55929	124.29	206.34	0	0.
MILLEN		MID-AM #2 MIDDLETON								R,L R.L						
162 MONROE 66 22 10 13.3 20.880 47,900 22 R.E. 1 0.55929 18165 235.32 1						20				R,L	!					
164 MOORE CO											i					
166 MORTON										R,L R I	-					
167 MULESHOE CITY	165	MORTON	67	2.4	5	6.25	10,526	32,485	2.4	R,E	į	0.55929	92.46	159.59	2	
169 MULESHOE WATERIELD @ Bailey Co 66 12.5 1.5 1.5 2.765 8.364 12.5 R.L 1 0.55929 24.29 41.09 1																
170 MURPHY											!					
172	170	MURPHY	115	22.86	20	33	12,592	58,368	22	R,E	i	0.55929	110.61	286.75	3	
173											!					
175 NPLAINVIEW 67 12.5 10 10 16.500 55.000 12.5 R.E I 0.55929 144.94 270.20 2 176 NAVAJO MALAGA 66 4.16 3 3 6,316 19.491 4.16 R.E I 0.55929 55.48 95.75 0 177 NM POTASH 69 13.8 7.5 10.5 16.680 44.960 12.5 R.E I 0.55929 146.52 220.88 0 178 NORRIS ST 115 13.2 12 20 13.396 37.753 12.5 R.L I 0.55929 117.67 185.47 2 179 NORTH CANAL 115 13.2 15 25 15.291 56.220 12.5 R.L I 0.55929 117.67 185.47 2 179 NORTH CANAL 115 13.2 16.8 28 11,300 66.100 12.5 R.L I 0.55929 134.32 276.20 3 180 NORTH LOVING 118 13.2 16.8 28 10,000 69.000 12.5 R.L I 0.55929 87.84 338.98 2 181 OCHOA 118 13.2 16.8 28 9.851 64.252 12.5 R.L I 0.55929 87.84 338.98 2 182 OCOTILLO 118 13.2 16.8 28 9.851 64.252 12.5 R.L I 0.55929 87.84 338.98 2 183 OLTON 67 12.5 7.5 7.5 13.825 41.819 12.5 R.E I 0.55929 121.44 205.45 2 184 OSAGE 118 13.2 16.8 28 11.789 60.542 12.5 R.L I 0.55929 121.44 205.45 2 185 OZARK MAHONING #2 67 2.4 5 5.6 9.501 29.887 2.4 R.L E 0.55929 103.55 297.43 4 186 PACIFIC 115 12.5 12 20 19.300 65.500 12.5 R.L E 0.55929 77.84 115.79 1 186 PALIDON 115 12.5 12 20 19.300 65.500 12.5 R.L E 0.55929 77.84 115.79 1 188 PALA BERRO 115 12.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7	173	N HOBBS #1	115	12.5	12	20	21,320	41,510	12.5	R,E	į	0.55929	187.27	203.93	3	
176 NAVAJOMALAGA 66 4.16 3 3 6.316 19.491 4.16 R.E 1 0.55929 55.48 95.75 0 177 NA POTASH 69 13.8 7.5 10.5 16.680 44.960 12.5 R.E 1 0.55929 176.67 185.47 2 178 NORTH CANAL 115 13.2 12 20 13.396 37.753 12.5 R.L 1 0.55929 117.67 185.47 2 179 NORTH CANAL 115 13.2 15 25 15.291 56.220 12.5 R.L 1 0.55929 143.52 276.20 3 180 NORTH LOVING 118 13.2 16.8 28 11.300 66.100 12.5 R.L 1 0.55929 99.26 324.74 2 181 OCHOA 118 13.2 16.8 28 10.000 69.000 12.5 R.L 1 0.55929 99.26 324.74 2 181 OCHOA 118 13.2 16.8 28 9.851 64.252 12.5 R.L 1 0.55929 99.26 334.74 2 182 OCOTILLO 118 13.2 16.8 28 9.851 64.252 12.5 R.L 1 0.55929 99.26 334.74 2 183 OLTON 67 12.5 7.5 7.5 13.825 41.819 12.5 R.L 1 0.55929 121.44 205.45 2 184 OSAGE 118 13.2 16.8 28 11.789 60.542 12.5 R.L 1 0.55929 121.44 205.45 2 185 OZARK MAHONING #2 67 2.4 5 5.6 9.501 29.687 2.4 R.L E 0.55929 0.00 0.00 0 100 186 PACIFIC 115 13.2 7.5 10.5 8.520 23.570 13.2 R.L E 0.55929 74.84 115.79 1 188 PARMER CO 115 13.2 7.5 10.5 8.520 23.570 13.2 R.L 1 0.55929 74.84 115.79 1 189 PCA #2 67 13.2 16 8.24 13.82 95.11 13.2 R.L 1 0.55929 121.44 467.31 2 189 PCA #2 67 13.2 16.8 28 10.330 65.333 13.2 R.L 1 0.55929 121.44 467.31 2 189 PCA #2 67 13.2 16.8 28 10.330 65.333 13.2 R.L 1 0.55929 121.44 467.31 2 189 PCA #2 67 13.2 16.8 28 10.330 65.333 13.2 R.L 1 0.55929 121.44 467.31 2 189 PCA #2 67 13.2 16.8 28 10.330 65.333 13.2 R.L 1 0.55929 136.86 136.97 3 191 PERINTETER 118 13.2 16.8 28 10.330 65.333 13.2 R.L 1																
178 NORRIS ST						3	6,316	19,491			!	0.55929		95.75	-	
180 NORTH LOVING 118 13.2 16.8 28 11,300 66,100 12.5 R.L I 0.55929 99.26 324,74 2 181 OCHOA 118 13.2 16.8 28 10,000 69,000 12.5 R.L I 0.55929 92.6 324,74 2 183 OLTON 67 12.5 7.5											i					
181 OCHOA 118 13.2 16.8 28 10,000 69,000 12.5 R.L I 0,55929 87.84 338.98 2 182 OCOTILLO 118 13.2 16.8 28 9,851 64,252 12.5 R.L I 0,55929 87.84 338.98 2 183 OLTON 67 12.5 7.5 13,825 41,819 12.5 R.L I 0,55929 10.35 297.43 4 184 OSAGE 118 13.2 16.8 2.8 11,789 60,542 12.5 R.L I 0,55929 10.0 0.0 0.00 </td <td></td> <td>!</td> <td></td> <td></td> <td></td> <td></td> <td></td>											!					
183 OLTON 67 12.5 7.5 7.5 13.825 41.819 12.5 R.E I 0.55929 121.44 205.45 2 184 OSAGE 118 13.2 18.8 28 11,789 60.542 12.5 R.L I 0.55929 10.35 297.43 4 186 PACIFIC 115 12.5 12 20 19,300 65,500 12.5 R.L E 0.55929 0.00 0.00 0.00 100 187 PALO DURO 115 13.2 7.5 10.5 8.520 23,570 13.2 R.L I 0.55929 174.84 115.79 1 188 PARMER CO 115 13.2 7.5 10.5 8.520 23,570 13.2 R.L I 0.55929 74.84 115.79 1 189 PCA#2 67 13.2 16 22.4 13,825 95,121 13.2 R.L I 0.55929 <td>181</td> <td>OCHOA</td> <td>118</td> <td>13.2</td> <td>16.8</td> <td>28</td> <td>10,000</td> <td>69,000</td> <td>12.5</td> <td>R,L</td> <td></td> <td>0.55929</td> <td>87.84</td> <td>338.98</td> <td>2</td> <td></td>	181	OCHOA	118	13.2	16.8	28	10,000	69,000	12.5	R,L		0.55929	87.84	338.98	2	
184 OSAGE 118 13.2 18.8 28 11,789 60,542 12.5 R.L I 0.59929 103.55 297.43 4 185 OZARK MAHONING #2 67 2.4 5 5.6 9,501 29,887 2.4 R.L E 0.55929 103.55 297.43 4 186 PACIFIC 115 12.5 12 20 19,300 65,500 12.5 R.L E 0.55929 108.50 20.94 2 36 187 PALO DURO 115 13.2 7.5 17.5 17.800 40,490 22 R.E I 0.55929 174.84 115.79 1 188 PARMER CO 115 12.5 5 6.25 9,216 27.871 13.2 R.E I 0.55929 174.44 467.31 2 189 PCA #2 67 13.2 16 22.4 13.825 95.121 13.2 R.E I 0.55																
186 PACIFIC 115 12.5 12 20 19,300 65,500 12.5 R.L E 0.55929 108.50 205.44 2 36 187 PALO DURO 115 13.2 7.5 10.5 8,520 23,570 13.2 R.L I 0.55929 156.36 198.92 2 188 PARMER CO 115 22 7.5 7.5 17,800 40,490 22 R.E I 0.55929 156.36 198.92 2 189 PCA #2 67 13.2 16 22.4 13,282 95,121 13.2 R.L I 0.55929 156.36 198.92 2 190 PERRI 115 12.5 5 6.25 9,216 27,879 12.5 R.E I 0.55929 80.96 136.97 3 191 PERIMETER 118 13.2 16.8 28 10,330 65,333 13.2 R.L E 0.55929 </td <td>184</td> <td>OSAGE</td> <td>118</td> <td>13.2</td> <td>16.8</td> <td>28</td> <td>11,789</td> <td>60,542</td> <td>12.5</td> <td>R,L</td> <td>1</td> <td>0.55929</td> <td>103.55</td> <td>297.43</td> <td>4</td> <td></td>	184	OSAGE	118	13.2	16.8	28	11,789	60,542	12.5	R,L	1	0.55929	103.55	297.43	4	
187 PALO DURO 115 13.2 7.5 10.5 8,520 23,570 13.2 R.L I 0.55929 74.84 115.79 1 188 PARMER CO 115 22 7.5 7.5 17.5 17.800 40,490 22 R.E I 0.55929 156.36 198.92 2 189 PCA #2 67 13.2 16 22.4 13,825 95.121 13.2 R.L I 0.55929 121.44 467.31 2 190 PERRY 1 15 12.5 5 6.25 9.216 27.879 12.5 R.L I 0.55929 80.96 136.973 3 191 PERRITION 115 13.2 16.8 28 10.330 65.333 13.2 R.L E 0.55929 80.00 10.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 10.0 10.0																
189 PCA #2 67 13.2 16 22.4 13.825 95.121 13.2 RL I 0.55929 121.44 467.31 2 190 PERRIT 115 125 5 6.25 9.216 27.879 12.5 R.E I 0.55929 8.09 136.97 3 191 PERRITON N 115 12.5 7.5 11.72 9.800 36,700 12.5 R.L I 0.55929 8.00 0.0 0.00 0 100 192 PERRYTON S 115 12.5 7.5 11.72 9.800 36,700 12.5 R.L I 0.55929 8.00 10.0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0							8,520	23,570		R,L		0.55929	74.84			
190 PEARL 115 12.5 5 6.25 9.216 27.879 12.5 R.E I 0.55929 80.96 136.97 3 191 PERRIMETER 118 13.2 16.8 2.8 10,330 65,333 13.2 R.L E 0.55929 80.0 100 0.00 100 192 PERRYTON N 115 12.5 7.5 11.72 9,800 36,700 12.5 R.L I 0.55929 86.08 180.30 2 193 PERRYTON S 115 12.5 7.5 10.5 15,500 58,000 12.5 R.L I 0.55929 86.08 180.30 2 194 PHILLIP PUMP 69 2.4 2.5 2.8 5,109 21,081 2.4 R.L I 0.55929 44.88 103.57 0 195 PHILLIPS PUMP 2 69 2.4 2.5 2.8 4,837 21.307 2.4 R.L I	189	PCA #2	67	13.2	16	22.4	13,825	95,121	13.2	R,L		0.55929	121.44	467.31	2	
192 PERRYTON N 115 12.5 7.5 11.72 9.800 36,700 12.5 R.L I 0.55929 86.08 180.30 2 194 PHILLIP PUMP 69 2.4 2.5 2.8 5,109 21,081 2.4 R,L I 0.55929 44.88 103.57 0 195 PHILLIP PUMP 69 2.4 2.5 2.8 5,109 21,081 2.4 R,L I 0.55929 44.88 103.57 0 195 PHILLIP PUMP 69 2.4 2.5 2.8 4,837 21,307 2.4 R,L I 0.55929 44.88 103.57 0 196 PIERCE 115 13.8 15 25 23,053 68,991 13.2 R,L I 0.55929 83.45 145.85 2 197 PLAINVIEW CITY E Transformer 65 2.4 7.5 7.5 9,501 29,687 2.4 R,E I 0.5592											I E					100
194 PHILLIP PUMP 69 2.4 2.5 2.8 5,109 21,081 2.4 R.L I 0.55929 44.88 103.57 0 195 PHILLIPS PUMP 2 69 2.4 2.5 2.8 4,837 21,307 2.4 R.L I 0.55929 42.49 104.68 0 196 PIERCE 115 13.8 15 25 23,053 68,991 13.2 R.L I 0.55929 202.50 38.94 3 197 PLAINVIEW CITY E Transformer 65 2.4 7.5 7.5 9,501 29,687 2.4 R.E I 0.55929 83.45 145.85 2 198 PLANTY RURAL 115 12.5 5 5 11,720 28,660 12.5 R.L I 0.55929 83.45 145.85 2 199 PLANTY RURAL 115 12.5 5 5 11,720 28,660 12.5 R.L I 0.5592	192	PERRYTON N	115	12.5	7.5	11.72	9,800	36,700	12.5	R,L	1	0.55929	86.08	180.30	2	100
195 PHILLIPS PUMP 2 69 2.4 2.5 2.8 4,837 2,1307 2.4 R.L I 0.55929 42.49 104.68 0 196 PIERCE 115 13.8 15 25 23.053 68.991 13.2 R.L I 0.55929 20.250 338.94 3 197 PLAINVIEW CITY E Transformer 65 2.4 7.5 7.5 9.501 29.687 2.4 R.E I 0.55929 83.45 145.85 2 198 PLAINVIEW CITY W Transformer 66 2.4 3.75 3.75 9.501 29.687 2.4 R.E I 0.55929 83.45 145.85 2 199 PLANY K URAL 115 12.5 5 5 11,720 28,660 12.5 R.L I 0.55929 83.45 145.85 2																
197 PLAINVIEW CITY E Transformer 65 2.4 7.5 7.5 9,501 29,687 2.4 R.E I 0.55929 83.45 145.85 2 198 PLAINVIEW CITY W Transformer 66 2.4 3.75 3.75 9,501 29,687 2.4 R.E I 0.55929 83.45 145.85 2 199 PLANT X RURAL 115 12.5 5 5 11,720 28,660 12.5 R.L I 0.55929 102.95 140.80 2	195	PHILLIPS PUMP 2	69	2.4	2.5	2.8	4,837	21,307	2.4	R,L	i	0.55929	42.49	104.68	0	
198 PLAINVIEW CITY W Transformer 66 2.4 3.75 3.75 9,501 29,687 2.4 R,E I 0,55929 83.45 145.85 2 199 PLANT X RURAL 115 12.5 5 5 11,720 28,660 12.5 R,L I 0.55929 102.95 140.80 2																
193 FLUND A NORTH 113 12.5 5 5 11,720 28,880 12.5 K,L I 0.50929 102.95 140.80 2 200 PORTALES#1 67 4.2 7.5 9.375 12,000 48,000 4.16 R,E I 0.55929 105.41 235.81 3	198	PLAINVIEW CITY W Transformer	66	2.4	3.75	3.75	9,501	29,687	2.4	R,E		0.55929	83.45	145.85	2	
										R,E						

Line No.	1	Voltage High Side, kV 2	Low Side, kV 3	Ratings Nominal MVA 4	Max MVA 5	No Load Losses WATTS 6	Full Load Losses WATTS 7	Low Side Class 8	Verify Flag R,L,E 9	Exclude Flag 10	Primary Load Factor 11	No Load Losses MWH 12	Full Load Losses MWH 13	Number of Feeder Circuits 14	Percent Transf. Excluded 15
201 202	PORTALES #2 A PORTALES #2 B	67 67	12.47 4.2	10 5	14 5	6,316 8,777	19,491 40.107	4.16 4.16	R,L R.L	I I	0.55929 0.55929	55.48 77.10	95.75 197.04	1 2	
203	PORTALES SOUTH	67	4.16	7.5	9.375	12,000	44,565	4.16	R,L	į	0.55929	105.41	218.94	2	
204 205	PORTALES WATER FIELD POST CITY (Garza #3)	115 67	12.5 4.2	10 5	14 5	11,700 10,304	33,600 34,922	13.2 4.16	R,L R,L	i	0.55929 0.55929	102.77 90.51	165.07 171.56	2	
206 207	POTASH JUNCTION PRENTICE W	67 115	12.5 13.2	10 15	12.5 28	14,470 12,281	58,190 52,074	12.5 13.2	R,L R,L	I E	0.55929 0.55929	127.10 7.55	285.88 17.91	1 1	93
208 209	PRICE PRINGLE INT	118 115	13.2 34.5	17.5 16.8	29.5 28	11,700 13,106	67,500 68,952	12.5 33	R,L R,L	1	0.55929 0.55929	102.77 115.12	331.61 338.75	3	
210	PUCKETT WEST	115	13.2	15	25	15,460	58,647	13.2	R,L	į	0.55929	135.80	288.12	3	
211 212	PULLMAN RIAC EAST	115 67	13.2 4.2	15 5	25 5.25	11,990 10,526	52,620 32,485	13.2 4.16	R,L R,L	i i	0.55929 0.55929	105.32 92.46	258.51 159.59	3	
213 214	RIAC WEST RILEY	69 67	4.2 12.5	7.5 3.75	9.375 5	11,800 6,912	44,605 20,909	4.16 12.5	R,L R,E	!	0.55929 0.55929	103.65 60.72	219.14 102.72	2 2	
215	RIVERVIEW	115	13.2	15	25	16,074	56,237	13.2	R,L	į	0.55929	141.19	276.28	3	
216 217	ROBERTS CO ROSWELL CITY N	67 115	4.16 12.5	5 15	6.25 25	6,851 17,636	19,040 65,206	13.2 12.5	R,E R,E		0.55929 0.55929	60.18 154.91	93.54 320.34	2	
218 219	ROSWELL CITY S ROXANA	115 69	12.5 13.8	15 10	25 14	17,600 10,742	65,000 23,613	12.5 13.2	R,E R,E	!	0.55929 0.55929	154.60 94.36	319.33 116.01	2 2	
220 221	RUSSELL SUB E TRANSFORMER RUSSELL SUB W TRANSFORMER	115 115	12.5	12	20 28	20,200 12,369	63,100 51,686	12.5	R,L R.L	E E	0.55929	63.88 39.11	111.60	1 2	64 64
222	S FLOYDADA	66	13.2 22	15 5	5	10,100	32,392	13.2 22	R,L	Ī	0.55929	88.72	91.41 159.14	2	04
223 224	S HOBBS E S HOBBS W	115 115	13.2 12.5	12 12	20 20	14,677 18,500	40,275 57,000	12.5 12.5	R,L R,L	E E	0.55929 0.55929	128.92 35.75	197.86 61.61	2	78
225 226	S PLAINVIEW SAGE BRUSH	67 115	12.5 22.86	10 30	14 50	16,500 20,600	55,000 91,000	12.5 22	R,E R.L	1	0.55929 0.55929	144.94 180.95	270.20 447.06	3	
227	SAMSON	115	13.2	12	20	18,820	46,500	12.5	R,L	į	0.55929	165.31	228.45	2	
228 229	SAND DUNES SEMINOLE INTG	67 115	12.5 22.86	7.5 16.8	8.4 28	9,500 12,592	30,000 58,368	12.5 22	R,L R,L	i	0.55929 0.55929	83.45 110.61	147.38 286.75	3 2	
230 231	SHAMROCK PUMP SHELL C3	66 115	2.4 4.16	1 10	1 14	2,534 12,852	7,917 31.876	2.4 4.16	R,E R.L	I E	0.55929 0.55929	22.25 80.15	38.89 111.19	0	29
232 233	SHERMAN CO SLATON	115 69	34.5 22.9	12 10	12 10	27,100 13.067	53,900 35.044	33 22	R,L R,L	!	0.55929 0.55929	238.05 114.78	264.80 172.16	3 2	
234	SLATON CITY	67	4.2	3.75	3.75	7,894	24,364	4.16	R,E	į	0.55929	69.34	119.69	2	
235 236	SLAUGHTER SMITH	67 67	2.4 4.2	3.75 3.75	4.2 3.75	6,960 7,894	22,330 24,364	2.4 4.16	R,L R,E	i i	0.55929 0.55929	61.14 69.34	109.70 119.69	1 2	
237 238	SONCY SOUTH GEORGIA EAST	67 115	13.8 13.8	20 15	20 25	24,981 21,120	94,630 56.040	13.2 13.2	R,L R,L	!	0.55929 0.55929	219.43 185.52	464.90 275.31	4	
239	SOUTH GEORGIA WEST	118	13.2	16.8	28	9,052	75,940	13.2	R,L	į	0.55929	79.51	373.08	3	
240 241	SOUTH LOVING SOUTHEAST	69 115	13.2 13.2	11.2 15	17.5 25	7,835 18,480	43,091 50,440	13.2 13.2	R,L R,L	i	0.55929 0.55929	68.82 162.33	211.70 247.80	3 2	
242 243	SOUTHLAND SPEARMAN INTERCHANGE	69 67	2.4 34.4	1.5 10	1.5 10	3,158 14,320	9,745 61.030	2.4 33	R,E R.L	!	0.55929 0.55929	27.74 125.79	47.88 299.83	1	
244 245	SPEARMAN SUB EAST XFMR SPEARMAN SUB WEST XFMR	115 115	4.16 4.16	7.5 7.5	10.5 10.5	12,416 13,440	40,872 41,855	4.16 4.16	R,L R.L	I	0.55929 0.55929	109.06 118.06	200.80 205.63	2 2	
246	SPRING DRAW	118	13.2	16.8	28	11,713	67,783	13.2	R,L	į	0.55929	102.89	333.00	3	
247 248	SPRINGCREEK SPRINGLAKE	67 67	13.2 13.2	7.5 7.5	9.375 7.5	15,760 11,060	41,150 52,193	13.2 13.2	R,E R,L	i i	0.55929 0.55929	138.44 97.15	202.16 256.41	2	
249 250	SUDAN RURAL SUNSET T1	66 115	12.5 13.2	2.5 15	2.5 28	4,608 15,300	13,940 46,900	12.5 13.2	R,E R.L	l I	0.55929 0.55929	40.48 134.40	68.48 230.41	2	
251	SUNSET T2	118	13.2	16.8	28	14,300	63,300	13.2	R,L	į	0.55929	125.61	310.98	2	
252 253	TEAGUE TENNECO	115 69	12.5 13.2	10 15	14 25	13,610 11,170	30,300 57,590	12.5 13.2	R,E R,L	i	0.55929 0.55929	119.55 98.12	148.86 282.93	2 1	
254 255	TEXACO TEXAS FARMS	67 115	12.5 13.2	12 7.5	20 9.375	20,146 7,670	52,610 23,270	12.5 13.2	R,L R.L	E I	0.55929 0.55929	21.24 67.37	31.02 114.32	2 1	88
256 257	TMC TOKIO	67 67	4.2 12.5	10 5	12.5 6.25	15,600 9,216	54,420 27,879	4.16 12.5	R,L R,E	I	0.55929 0.55929	137.03 80.96	267.35 136.97	0	
258	TRANSPETCO	67	4.2	7.5	7.5	11,657	37,611	4.16	R,L	i	0.55929	102.40	184.78	2	
259 260	TUCO TWEEDY	67 115	12.5 13.2	10 12	13.3 20	16,050 10,260	58,110 33,790	12.5 13.2	R,L R,L	I E	0.55929 0.55929	140.98 19.83	285.48 36.52	2	78
261 262	UNITED SALT URTON	69 115	12.4 12.5	0.75 12	0.75 12	1,382 21,940	4,182 63,559	12.5 12.5	R,E R,L	!	0.55929 0.55929	12.14 192.72	20.54 312.25	1 2	
263 264	VAN BUREN #1 VAN BUREN #2	67 67	13.2 13.8	15 15	25 25	29,725 23,760	70,460 62,700	13.2 13.2	R,L R.L	I	0.55929 0.55929	261.10 208.71	346.16 308.03	3	
265	VEGA	69	13.2	11.2	14	10,575	43,151	13.2	R,L	į	0.55929	92.89	211.99	2	
266 267	VICKERS W ANTON	69 66	23.9 22	10 6	14 6	23,600 11,394	50,236 30,261	22 22	R,L R,E	l I	0.55929 0.55929	207.30 100.09	246.80 148.67	1	
268 269	W BENDER W BORGER	115 115	13.2 13.2	12 15	22.4 25	11,190 14,838	38,840 55,493	13.2 13.2	R,L R.L	l I	0.55929 0.55929	98.29 130.34	190.81 272.63	2	
270	W CLOVIS 13.2 KV	115 67	13.2	15	25	12,160	55,680 47.800	13.2	R,L R.L	į	0.55929	106.81 94.87	273.54	2	
271 272	W CLOVIS 23 KV W LITTLEFIELD	69	24 12.5	12 1.5	22.4 1.5	10,800 2,765	8,364	22 12.5	R,E	i	0.55929 0.55929	24.29	234.83 41.09	1	
273 274	W MULESHOE W PLAINVIEW	69 67	13.2 12.5	11.2 12.5	1400 20	9,800 16,500	66,850 55,000	12.5 12.5	R,L R,E	1	0.55929 0.55929	86.08 144.94	328.42 270.20	2 4	
275 276	WADE WARD	118 115	13.2 12.5	5.6 4	7	2,088 13,610	6,265 30,300	12.5 12.5	R,E R.L	1	0.55929 0.55929	18.34 119.55	30.78 148.86	1	
277	WASSON	67	2.4	2	2	5,160	15,661	2.4	R,L	į	0.55929	45.33	76.94	0	
278 279	WATERFIELD WEATHERLY	67 67	13.8 13.8	10 10	12.5 11.2	13,670 15,760	68,760 41,150	13.2 13.2	R,L R,E	i	0.55929 0.55929	120.08 138.44	337.80 202.16	3	
280 281	WELLMAN WESTRIDGE	67 69	12.5 13.2	5 12	6.25 20	5,000 9,020	15,000 45,460	12.5 13.2	R,E R,L	I I	0.55929 0.55929	43.92 79.23	73.69 223.34	1 2	
282	WHERRY HOUSING WHITAKER	67 115	12.5 13.8	3 15	3.65 25	5,530 22,520	16,728 72,200	12.5 13.2	R,E R,L	1	0.55929 0.55929	48.57 197.82	82.18 354.70	2	
284	WHITE CITY	67	12.5	2.5	2.5	4,608	13,940	12.5	R,E	į	0.55929	40.48	68.48	2	
285 286	WHITEFACE WHITEHEAD AMOCO	67 67	12.5 2.4	10 3.75	10 4.69	14,695 7,120	57,235 27,771	12.5 2.4	R,L R,E		0.55929 0.55929	129.08 62.54	281.18 136.43	2 1	
287 288	WHITHARRAL WHITTEN	67 115	4.16 12.5	2.5 10	3.125 12.5	6,560 21,360	16,503 64,570	4.16 12.5	R,L R,L	l I	0.55929 0.55929	57.62 187.63	81.08 317.22	1 2	
289 290	WILDORADO WILLS OIL	67 67	12.5 12.5	10 1.5	10	15,984 2,730	59,797 7,800	13.2 12.5	R,L R,E	!	0.55929 0.55929	140.40 23.98	293.77 38.32	2	
291	WOOD DRAW	118	13.2	16.8	28	8,989	67,373	13.2	R,L	!	0.55929	78.96	330.99	3	
292 293	YANCY YELLOW HOUSE	67 66	4.16 12.5	2 3.75	2 5	5,160 10,992	15,536 32,937	4.16 12.5	R,L R,E	1	0.55929 0.55929	45.33 96.55	76.33 161.81	0 1	
294 295	ZAVALLA ZIA	67 115	12.5 13.2	10 10	12.5 14	18,680 22,080	51,100 39,216	12.5 12.5	R,L R,E	l I	0.55929 0.55929	164.09 193.95	251.04 192.66	2	
296	ZODIAC	67	4.16	10	11.2	19,282	64,592	4.16	R,L	i	0.55929	169.37	317.33	2	
297 298						No Load	Full Load	Total				No Load	Load	Total	
299 300						Losses MW	Losses MW	Losses MW				Losses MWH	Losses MWH	Losses MWH	
301 302		Total nomin	nal ratinge	3,043.580 M	/A	3.65		16.52				32,101	63,229	95,330	
303	Sum of demands at Prima	ary and belov	v from "H"	2,253.641 M	N	2.00	.2.07	. 0.02				JE, 101		55,550	
304 305	System at peak Sum of demands adjusted			47.291 M 2,206.351 M											
306 307		Hours	in Period	8784											
308															

Line No.	1	Voltage High Side, kV 2	Low Side, kV 3	Ratings Nominal MVA 4	Max MVA 5	No Load Losses WATTS 6	Full Load Losses WATTS 7	Low Side Class 8	Verify Flag R,L,E 9	Exclude Flag 10	Primary Load Factor 11	No Load Losses MWH 12	Full Load Losses MWH 13	Number of Feeder Circuits 14	Percent Transf. Excluded 15
309	!														
310															
311															
312	Summary Information														
313	KV Level	33	22	13.2	12.5	4.16	2.4	Total							
314	Total Nominal MVA by Voltage	153.30	327.00	1,151.70	1,091.75	218.48	83.85	3,026.08		MVA					
315	Load by Voltage	111.77	238.42	839.72	796.01	159.30	61.14	2,206.35		MW Load					
316	Load on transformers without feeders	0.00	0.00	23.69	8.33	54.98	17.29	104.29		MW Load A	t the transfo	mer			
317	Total Feeders	19.00	50.00	205.00	224.00	47.00	28.00	573.00		Number of F	eeders				
318	Feeders excluding partial feeders	18.07	50.00	196.09	212.94	47.00	28.00	552.10		All feeders le	ess % of tran	sformer not i	ncluded		
319	Load on Feeders	111.77	238.42	816.02	787.68	104.32	43.85	2,102.06		MW Load o	n feeders				

Appendix J Distribution Primary Loss

Primary Level Frament of Transformers Sec. Distribution Lines 450.871 Kw (498.161 Demand at Level 47.294 Kw (47.294 Subtract Dist Convolution Transformers) 450.871 Injected into Level 47.294 Kw (47.294 Subtract Dist Convolution Lines) 490.871 Injected into Level 47.294 Kw (47.294 Subtract Dist Convolution Lines) 490.871 Injected into Level 47.294 Kw (47.294 Mr) 470.4794 Mr)	from App. H ccted Gen at Pk Hour from Level 3	om App. H sted Gen from Level 3			, Se,	Onms per Feeder, Watts 23.71 833.093.97		3.27 325,140.48			3.360,846.93	0,000,0	Total Primary Loss(MW)							
ution 450,871 Kw (a) 4 n Transformers 2,206,351 Kw (a) 4 n Lines 2,206,351 Kw (a) 3,704,7 n Lines 4,161,409,160 Kwh (a) 3,704,7 n Lines QCP (a) 4,161,409,160 Kwh (a) 3,265,508,888 Kwh (a) No. of NW Per (a) Current (a) Typical (a) A,3265,508,888 Kwh (a) No. of NW Per (a) Current (a) Typical (a) A,3265,508,888 Kwh (a) A,3265,508,888 Kwh (a) No. of NW Per (a) Current (a) Typical (a) A,161,409,160 Kwh (a) A,161,409,160 Kwh (a) A,100 (a) 196.09 4,16 108,22 1/0 A,100 (a) A,100	Demand at Level 4 i Subtract Dist Conne Injected into Level 4	Energy at Level 4 fr Subtract Dist Conne Injected into Level 4			Avg. Feeder	Lengtn, n							-							
ution Transformers Transformers Transformers Lines 2,206,351 Kw 1,114,734 Kw 1,114,734 Kw 1,114,734 Kw 1,114,734 Kw 1,114,734 Kw 1,1632,404,736 Kw 1,160.09 No. of MW Per Amps 1,619 H82.02 212.94 196.09 4,16 196.09 4,16 182.02 212.94 3,70 1,57 376.72 552.10 Finergy Losses Tall Primary 10,632,404,736 KW 10,632,404,736 KW 10,632,404,736 KW 196.09 1,57 10,632,404,736 KW 197 H81 Primary 10,632,404,736 KW	498,161 47,291 450,871	3,704,794,414 439,285,526 3,265,508,888			O. W. Complete		1.12	0.306	0.306	0.306	760.0									
ution In Transformers In Lines In Curr Reeders In Curr Reeders In Curr Reeders In Curr Reeders In Curr Reeder In Cosses In Curr Reeder In Cur	ξ & & ϔ Σ & & ½	Kwh Kwh Kwh Kwh			Typical	Conductor 1/0	1/0	336	336	336	0/4					KWH				ММН
uution no Transformers no Lines In Line	450,871 640,746 1,114,734 2,206,351	3,265,508,888 3,205,486,688 4,161,409,160 10,632,404,736	S		Current	Amps 108.22	125.14	182.02	170.86	308.05	3/0./2					10,632,404,736		0.5486	0.3753	675,624
Level 4 - Primary Level Level 4 - Primary Distribution Level 5 - Sec. Distribution Transforme Level 6 - Sec. Distribution Lines Finergy at Primary Level Level 4 - Primary Distribution Level 5 - Sec. Distribution Transforme Level 6 - Sec. Distribution Transforme Level 6 - Sec. Distribution Lines Fotal Energy Low Side	গ্ৰ	52	Demand Losse	@ CP	MW Per	Feeder 6.19					ı									
Demand at Primary Level Level 4 - Primary Distr Level 5 - Sec. Distribut Level 6 - Sec. Distribut Level 4 - Primary Level Level 4 - Primary Level Level 4 - Primary Distr Level 5 - Sec. Distribut Level 6 - Sec. Distribut Level 6 - Sec. Distribut Total Energy 3.3.00 11.18 22.00 23.84 13.20 816.0 12.50 787.7 4.16 104.3 2.40 4.18 Coad Factor - Based on T Demand and Energy Ab. Oss Factor Primary Energy Losses	el bution ion Transforme ion Lines	ibution ion Transforme ion Lines			No. of	9					L C	332.10					. !	otal Primary		
Demand at F Level 4 - F Level 5 - S Level 6 - S Total Deman Since 1 - F Level 4 - F Level 4 - F Level 5 - S Since 2 - S Since	rimary Leve Primary Distr ec. Distributi ec. Distributi d	imary Level Primary Distr ec. Distributi ec. Distributi			Load	=					2	7 102.						Based on T		rgy Losses
	Demand at P Level 4 - F Level 5 - Si Level 6 - Si Total Deman	Energy at Pri Level 4 - F Level 5 - Si Level 6 - Si Total Energy			Low Side	v oitage 33.0(22.00	13.2(12.5	4.0	7.7					Total Sales		Load Factor - Demand an	Loss Factor	Primary Ene

Appendix K Distribution Line Transformer Loss

Line No			Demand L	_osses							
1 2											
3 4	Commercial customers r	nay come oi	nly off the t		servic	e drops.					
5 6	Residential	301,809	meters	Adjusted Meters 331,812		97,184	trans.	3.4	41427	mtr/trans.	
7	Commercial									mtr/trans.	
8 9		79,198		49,195		45,116	tians.	1.1	J904 I	mu/trans.	
10 11	3 Ph Commercial	49,195	meters								
12 13											
14	Residential and small	commercial		1,114,734	KW		4,161,409,160	KWH		(Level 6)	
15 16	Comi	mercial Load	d	640,746	KW		3,205,486,688	KWH		(Level 5)	
17 18	Total	Load		1,755,480	ĸw		7,366,895,848	KWH			
19	. • • • • • • • • • • • • • • • • • • •			1,100,100			1,000,000,010				
20 21	Load/Residential Custon	ner		3.36	KW		Load/transformer		11.47	KW	
22 23	Load/Commercial Custo	mer		13.02	KW		Load/transformer		14.20	KW	
24											
25 26	Typical Transformer Los	ses		NL watts			FL watts			KVA Transformer	
27 28			207	NL watts		892	FL watts		100	KVA Transformer	
29 30	Residential Transformer	Losses(Wat	tts)	189.33							
31	Commercial Transforme	r Losses(Wa	atts)	304.28							
32 33											
34 35	No Load Losses(KW)			Residential 7,385.98		mercial ,339.01					
36 37	Load Losses(KW)			18,399.57	13	,728.12					
38							-				
39 40	Total Losses(KW)			25,785.55	23	,067.13					
41 42	Total Line Transformer	Losses (K)	W)			48,853					
43			F								
44 45			Energy Lo	osses							
46 47	Total Sales			7,366,895,848	KWH						
48 49	Load Factor - Based on	Total Secon	darv	0.4777							
50	Demand and Energy A		aai y								
51 52	Loss Factor			0.3031							
53	Total Dist. Line Transfo	rmer Losse	es	130,063	MWF	I					

Appendix L Secondary and Service Loss

Secondary Demand Losses

Line No. 1 2 3 4 5 6 7 8 9	Demand Served at Secondary Level Level 5 - Sec. Distribution Transformers Level 6 - Sec. Distribution Lines Total Demand Energy Served at Secondary Level Level 5 - Sec. Distribution Transformers Level 6 - Sec. Distribution Lines Total Energy			640,746 1,114,734 1,755,480 3,205,486,688 4,161,409,160 7,366,895,848	KW KWH KWH	
11	Secondary Conductor - 60 ' of 1/0 Conduc	tor				
12 13	Resistance 0.0127 ohms					
14 15	Load /Residential Customer	3.36	ΚW	(From Appendix K)		
16	Load /Nesidential Gustomer	3.30	IXVV	(i form Appendix it)		
17	Load /Commercial Customer	13.02	KW	(From Appendix K)		
18 19						
20	Losses for secondary run	14.00	amps		4.98	watts loss
21	,		•			
22		. 0				•
23	Number of Residential Customers Served Assumes that 1 meter was served at trans		dary		234,628	Customers
24 25	Assumes that I meter was served at trans	iomer				
26	To	tal Secor	ndarv L	.oss	1,168	KW
27			,		,	
28						
29						
30						
31 32	Se	ervice Dei	mand I	000		
33	36	i vice Dei	manu L	-033		
34	Resistance Values					
35						
36	Residential Service	0.02028	ohms			
37	65' of #2 Triplex					
38 39	Commercial Service	0.00636	ohme			
40	30' of #1/0 Quad	0.00030	OHHIO			
41						
42	Residential	331,812	mete	rs	14.00	amps/mtr
43	0	10 105			04.00	, .
44 45	Commercial	49,195	mete	rs	31.33	amps/mtr
46						
47	Residential Loss/Meter	7.95	watts		2,637	kw
48						
49	Commercial Loss/meter	18.73	watts		922	kw
50						
51 52	To	tal Servi	ce Los	ses	3,559	kw
53		7.tu: 00: V:	00 200		0,000	
54						
55	Se	condary	and Se	ervice Energy Losses	5	
56						
57	Total Sales			7,366,895,848	K/V/LI	
58 59	i Utai Jales			1,300,893,848	LVVI	
60	Load Factor - Based on Total Secondary			0.4777		
61	Demand and Energy Above			3		
62	Loss Factor			0.3031		
63	Total Consendant and LOCAL STATE			4 ====	IZM/	
64	Total Secondary and Service Demand L	.oss		4,726	ĸW	
65 66	Total Secondary and Service Energy Lo	SS		12,583	MWH	

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Demand Briefly MW Factored KWH Lose Demand Energy Parcent	State Stat	SOUTH	SOUTHWESTERN PUBLIC SERVICE COMPANY SUMMARY OF LOSS EVALUATION	SLIC SERVICE OSS EVALUA	E COMPAN TION	_					
Demand Fine by MWH Adjusted Fine by Loss Adjusted Fine by Loss Percent Percent Factored KWH Loss Demand Fine by Loss Fine by Loss Percent Percent Factored KWH Loss Demand Fine by Loss Percent Factored KWH Loss Demand Fine by Loss Percent Percent Factored KWH Loss Demand Fine by Loss Percent Factored KWH Loss Demand Factored KWH Percent Factored KWH Loss Demand Factored KWH Percent Factored KWH Percent Factored KWH Loss Demand Factored KWH Percent Factored KWH	Domand Energy MWH Energy Percent Percent Per		JAN - DEC 20	116							
Percent of Total Losses Percent Perc	Demand Fine graph Percent of Total Losses Factored KWH Loss Demand Fine graph Factored KWH Loss Total Loss KWh KWh </th <th></th>										
MW MWHH Adjusted MWH Demand Fine gy Factored KWH Loss Demand Fine gy Fine gy Percent Percent Factored KWH Loss Demand Fine gy Factored KWH Losd Domand Fine gy Post of KWH Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent Percent	Particle					Percent o	f Total Losses				
8.26 81,914 80,473 1.88 4.20 80,472,979 4 4.735 364,686 362,22 10.77 18.71 358,252,288 2 138.79 913,763,47 86,532 357,844 81 851,578 10.77 18.71 18.71 358,252,288 2 138.79 103,252,76 19.19 19.19 61,909 60,820 4.37 3.18 60,820,099 3 25 61 103,252,76 10.320,891 6 2.21 19.382 19.041 0.50 0.99 19.040,983 5 48.85 127,752,89 1.27 11.11 10.50 0.99 19.040,983 5 48.85 127,775,891 10.320,895 6 48.85 127,775,891 10.320,895 6 48.85 127,775,891 10.320,895 6 48.85 127,775,891 10.320,895 6 48.85 127,775,891 10.320,895 6 48.85 12,830 10.99 11.99 22,830,107 10.320,895 11.99 22,830,107 10.320,895 11.99 22,830,107 10.320,895 11.99 22,830,107 10.320,895 11.99 10.34 66.53,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.67 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 6653,738 46.84 34.87 663,738 46.84 34.87 67 67	8.26 81,914 80,473 1.88 4.20 80,472,979 1 0.00 47.35 394,668 3.56,222 10.77 18.71 389,22.28 2.88 2.22.28		Demand MW	Energy MWH	Adjusted Energy MWH	Demand Percent	Energy Percent	Factored KWH	Loss	Demand Total Loss KW	Energy Total Loss kWh
8.26 81,914 80,473 1.88 4.20 80,472,979 1 0.00 4.35 36,468 382,222 1.88 4.20 80,472,979 15.09 1	8.26	omponent								į	
8.26 81,914 80,472 188 4.20 80,472.979 1 0.00 4.735 364,668 358,252 10.77 18.71 358,252,268 2 138.79 913,763,47 (6.23) 357,874 351,579 15.09 18.36 351,578,600 3 25.61 103,252,76 (6.22) 19.04 0.60 80.0 19.040,983 5 48.85 127,775,28 12.04,96 6.651 6.534 0.18 0.34 6.533,894 6.532 2.543 0.18 0.34 6.5533,894 6.532,239 22,830 1.19 22,830,107 1.10 0.59 1.19 22,139 1.19 2	8.26 81.914 80.473 1.88 4.20 80.472.979 1 0.00 47.35 364.688 388.222 10.77 1877 358.22.288 2 138.79 913,763.47 19.19 61.909 60.820 4.37 3.18 60.820.288 3 1.578.600 2.12 18.634 18.307 0.48 0.99 19.040.933 5 48.85 127,752.89 1.27 11.16 10.921 0.07 0.14 2.630.895 6 4.73 12.361.94 2.54 47.41 4.668 0.12 0.24 4.657.80 0.99 11.90 22.830.107 2.54 21.905 21.519 0.58 11.2 22.830.107 2.04.96 675.624 663.738 46.64 34.67 663.738 16.97 11.27.752.81 2.04.96 675.624 663.738 46.64 34.67 663.738 11.261.948 4.39.46 1.914.545 1.914.545 1.914.545										
8.2.6 8.1,14 80,472,979 1.88 4.20 80,472,979 1.88.79 47.35 36,666 36,626 10,77 18.71 356,252.286 2 138.79 66.35 357,874 351,578 15.09 18.36 351,578,600 3 25.61 19.19 61,909 60,820 4.37 3.18 60,820,099 3 25.61 2.12 118,634 18.307 0.48 0.99 19,400,983 5 48.85 1.27 11,116 10,921 0.50 0.99 19,400,983 5 48.85 1.27 11,116 10,921 0.07 0.14 2,630,895 6 4.73 0.30 2,678 2,631 0.07 0.14 2,630,895 6 4.73 0.40 6,651 6,534 0.18 0.34 6,530,894 6 4.73 0.80 6,651 6,534 0.18 0.34 6,530,095 6 4.73 0.80 </td <td>47.35 84.668 80.473 1188 4.20 80.472.879 2 138.79 66.32 364.668 80.423 10.77 118.71 836.26.268 2 251.49 16.09 18.36 60.820.099 3 25.61 66.32 10.77 18.71 81.71 80.822.268 2 251.49 16.09 18.36 60.820.099 3 25.61 66.32 10.74 18.30 6.49 19.040.983 5 48.85 11.27 11.116 10.921 0.29 0.57 10.920.881 5 48.85 10.00 6.66.51 65.34 0.18 0.34 65.33.694 42.490 1.68 2.22 42.490.199 10.70 0.14 4.657.903 10.70 0.14 4.657.9</td> <td>es</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>0.00</td> <td>0</td>	47.35 84.668 80.473 1188 4.20 80.472.879 2 138.79 66.32 364.668 80.423 10.77 118.71 836.26.268 2 251.49 16.09 18.36 60.820.099 3 25.61 66.32 10.77 18.71 81.71 80.822.268 2 251.49 16.09 18.36 60.820.099 3 25.61 66.32 10.74 18.30 6.49 19.040.983 5 48.85 11.27 11.116 10.921 0.29 0.57 10.920.881 5 48.85 10.00 6.66.51 65.34 0.18 0.34 65.33.694 42.490 1.68 2.22 42.490.199 10.70 0.14 4.657.903 10.70 0.14 4.657.9	es							-	0.00	0
4.35 364,668 356,222 10.77 18.71 336,222,268 2 138.79 66.32 357,874 351,579 16.39 60.820,099 3 25.61 19.19 61,909 60.820 4.37 3.18 60.820,099 3 25.61 2.12 18,634 18,307 0.48 0.96 18,306,549 2.21 19,382 19,041 0.50 0.99 19,040,983 5 48.85 1.27 11,116 10,921 0.29 0.57 10,920,881 0.30 2,678 2,631 0.07 0.14 2,630,895 6 4.73 0.80 6,651 6,534 0.18 0.34 6,533,694 0.52 4,741 4,668 0.12 0.24 4,657,903 0.52 4,741 4,668 0.12 0.24 4,657,903 0.52 4,741 4,668 0.12 0.24 4,657,903 0.52 4,741 4,668 0.12 0.24 4,657,903 0.53 20,339 33,76 4.89 93,653,226 1.76 17,276 16,972 0.40 0.89 16,971,664 0.80 16,971,664 0.80 16,871,684 0.80 16,871,684 0.80 17,775,281 0.80 16,948,829 0.90 1.19 22,361,948 0.90 1.19 22,361,948 0.90 1.19 22,830,107 0.90 1.19 22,830,107 0.90 1.19 22,830,107 0.90 0.90 1.19 22,830,107 0.90 0.90 1.19 22,830,107 0.90 0.90 1.19 22,830,107 0.90 0.90 1.19 22,830,107 0.90 0.90 1.19 22,830,107 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90	47.35 364,668 358,252 10.77 18.71 368,222,268 2 138.79 61,909 60,820 4.37 3.16 60,820,999 3 25.61 22.12 18.634 18.307 0.48 0.96 18.306,549 22.1 19,822 10.77 0.44 0.96 18.306,549 7.2 2.1 19,822 10,921 0.29 0.97 19,040,983 5 48.85 1.2 11,116 10,921 0.29 0.97 10,920,881 6 4.73 0.30 2,678 2,631 0.07 0.14 2,630,895 6 4.73 0.80 6,651 6,534 0.18 2.22 42,480,219 4.36 23,239 22,830 0.99 1.19 22,830,107 0.52 4,741 4,658 0.12 0.24 4,667,903 2.54 21,905 21,519 0.68 11.12 21,519,365 1.76 17,276 16,972 0.40 0.89 93,653,226 1.76 17,276 16,972 0.40 0.89 93,653,226 4.73 12,362 1.08 0.65 12,775,281 4,89 93,633,236 4.39.46 1,948,829 1.2,362 1.08 0.65 12,361,948 4.39.46 1,948,829 1.394,545 1,914,545 1,914,544,850		8.26	81,914	80,473	1.88	4.20	80,472,979		;	
2.12	212 18,634 18,307 0.48 0.96 18,306,549 3 25,61 18,106,109 0 3 25,61 18,109 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0		47.35	364,668	358,252	10.77	18.71	358,252,268	7	138.79	913,763,470
2.12	2.12 18,634 18,307 0.48 0.96 18,306,549 4 221.49 1.27 11,116 10,921 0.29 0.57 11,920,881 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 5 48.85 19,040,983 172,775,281 48.85 19,044,848 11,246,548 19,048 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,246,548 11,346,548		19 19	557,674 61,909	876,166	13.09	3.18	000,076,156	~	25.61	103 252 764
2.12 18,634 18,307 0.48 0.96 18,306,549 48.85 2.21 1,1416 10,921 0.29 19,040,983 5 48.85 2.21 11,116 10,921 0.29 0.57 10,920,981 6 473 48.85 11,116 10,921 0.29 0.57 10,920,981 6 473 41.8 2.631 0.07 0.14 2,630,896 6 473 42,480 1.68 2.22 42,480,219 2.24,830 0.99 1.19 22,830,107 2.54 21,905 21,519 0.58 1.12 21,519,395 1.76 17,775 16,972 0.89 0.89 1.19 21,519,395 1.77 0.89 0.89 0.89 0.89 0.863,226 4.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0	212 18,634 18,307 0,48 0,96 18,306,549 4,885 1,171 11,116 10,921 0,29 0,57 10,920,881 5 48,85 11,1716 10,921 0,29 0,57 10,920,881 5 48,85 11,116 10,921 0,29 0,57 10,920,881 5 48,85 11,116 10,921 0,29 0,57 10,920,881 6 4,73 17,75 11,116 10,920,881 6 5,346 11,19 1,914,545 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,544,850 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,545 1,914,544,850 1,914,545 1,914,545 1,914,544,850 1,914		2	5	20,00	è	5	66,620,00	•	2	100,502,104
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0.80 6,651 6,534 0.18 0.34 6,533,694 439.46 7,40 43,241 42,480 1.68 2.22 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 42,480,219 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 46,57,903 47,51,519,395 47,51,519,395 47,51,519,395 47,51,519,395 47,51,519,395 47,51,519,395 47,52,519 47,52,519 47,52,519 47,52,519 47,52,519 47,52,519 47,73 41,54,545 41,914,545 <td< td=""><td>439.46 0.80 0.80 0.80 0.80 4.3.241 4.2.480 1.68 2.22 4.2.480,219 4.3.64 4.3.641 4.3.643 4.3.641 4.3.643 4.3.641 4.3.643 4.3.644 4.3.644,850</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	439.46 0.80 0.80 0.80 0.80 4.3.241 4.2.480 1.68 2.22 4.2.480,219 4.3.64 4.3.641 4.3.643 4.3.641 4.3.643 4.3.641 4.3.643 4.3.644 4.3.644,850										
0.80 6,651 6,534 0.18 0.34 7.40 43,241 42,480 1.68 2.22 4.36 23,239 22,830 0.99 1.19 0.52 4,741 4,658 0.12 0.24 2.54 21,905 21,519 0.58 1.12 1.76 17,276 16,972 0.40 0.89 1.8 16.52 95,330 93,653 3.76 4.89 204.96 675,624 663,738 46.64 34.67 4.73 12,583 12,362 1.08 0.65 4.39,46 1,948,829 -34,284 1,914,545 1,914,545	0.80 6,651 6,534 0.18 0.34 7.40 43,241 42,480 1.68 2.22 4.36 23,239 22,830 0.99 1.19 0.52 4,741 4,658 0.12 0.24 2.54 21,905 21,519 0.58 1.12 1.76 16,972 0.40 0.89 8rs 16,52 95,330 93,653 3.76 4.89 4.85 130,063 127,775 11.12 6.67 4.73 12,583 12,362 1.08 0.65 4.39,46 1,948,829 -34,284 1,914,545 1,914,545 1.59	- Load								439.46	1,914,544,850
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16.52 95,330 93,653 3.76 4.89 204.96 675,624 663,738 46.64 34.67 6 48.85 130,063 127,775 11.12 6.67 1 4.73 12,583 12,362 1.08 0.65 439.46 1,948,829 -34,284 1,914,545 1,914,545 1,914,545	16.52 95,330 93,653 3.76 4.89 204.96 675,624 663,738 46.64 34.67 6 48.85 130,063 127,775 11.12 6.67 1 4.73 12,583 12,362 1.08 0.65 439.46 1,948.829 -34,284 1,914,545 1,914,545 1,914,545 1,9		1.76	17,276	16,972	0.40	0.89	16,971,664			
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1,914,545	1,914,545 1,914,545	i Losses Losses	439.46	1,948,829 -34,284							
				1,914,545	1,914,545			1,914,544,850			
			- 1004O	4 048 820							

Appendix N

Powerflow Study Loss Results

Case Name: 2016MDWGFinal-16S_7_6003_edited.sav Case Title 1: "2016 MDWG FINAL WITH 2015 SERIES MMWG FINAL" Case Title 2: "MDWG 2016S WITH MMWG 2016S" Bus Range: 522800 - 528799 * * * * * * * * * * LOSSES BY ELEMENT CLASS * * * * * * * * * ------ AUTOTRANSFORMER LOSSES (MW) ------[345/230 kV] [345/115 kV] [230/115 kV] [230/69 kV] [115/69 kV] [TOTAL 0.0 7.399254 0.0 4.360944 12.56414 ----- TRANSMISSION LINE LOSSES (MW) ------[345 kV] [230 kV] [115 kV] [69 kV] [TOTAL] 8.262287 47.34864 66.32214 19.1898 141.1229 ----- CASE TOTALS -----TOTAL AREA LOSSES: 153.687MW TOTAL 345kV LINES: 10 TOTAL 345/230kV TRANSFORMERS: 7 TOTAL 230kV LINES: 79 TOTAL 345/115kV TRANSFORMERS: 0 TOTAL 115kV LINES: 391 TOTAL 69kV LINES: 288 TOTAL 230/115kV TRANSFORMERS: 53 TOTAL 230/69kV TRANSFORMERS: 0 TOTAL 115/69kV TRANSFORMERS: 86

Case Name: 2016MDWGFinal-16G_6_Jan-Feb_3379_edited_07172017.sav Case Title 1: "2016 MDWG FINAL WITH 2015 SERIES MMWG FINAL" Case Title 2: "MDWG 2016G WITH MMWG 2016L" Bus Range: 522800 - 528799 * * * * * * * * * LOSSES BY ELEMENT CLASS * * * * * * * * ----- AUTOTRANSFORMER LOSSES (MW) ------[345/230 kV] [345/115 kV] [230/115 kV] [230/69 kV] [115/69 kV] [TOTAL] 8.118386 0.673998 0.0 4.880167 0.0 2.564221 ----- TRANSMISSION LINE LOSSES (MW) ----------- CASE TOTALS -----TOTAL AREA LOSSES: 79.97969MW TOTAL 345kV LINES: 10 TOTAL 345/230kV TRANSFORMERS: 7 TOTAL 230kV LINES: 79 TOTAL 345/115kV TRANSFORMERS: 0

TOTAL 115kV LINES: 387 TOTAL 230/115kV TRANSFORMERS: 53

TOTAL 69kV LINES: 289 TOTAL 230/69kV TRANSFORMERS: 0 TOTAL 115/69kV TRANSFORMERS: 86

Case Name: 2016MDWGFinal-16G_6_Mar-May_3323_edited_07172017.sav Case Title 1: "2016 MDWG FINAL WITH 2015 SERIES MMWG FINAL" Case Title 2: "MDWG 2016G WITH MMWG 2016L" Bus Range: 522800 - 528799 * * * * * * * * * LOSSES BY ELEMENT CLASS * * * * * * * * ----- AUTOTRANSFORMER LOSSES (MW) ------[345/230 kV] [345/115 kV] [230/115 kV] [230/69 kV] [115/69 kV] [TOTAL 0.764193 0.0 4.626019 0.0 2.540981 7.931192 ----- TRANSMISSION LINE LOSSES (MW) ------[345 kV] [230 kV] [115 kV][69 kV] [TOTAL] 9.852043 48.48065 41.44 6.09039 ----- CASE TOTALS -----TOTAL AREA LOSSES: 113.7943MW TOTAL 345kV LINES: 10 TOTAL 230kV LINES: 79 TOTAL 345/230kV TRANSFORMERS: 7

TOTAL 115kV LINES: 387

TOTAL 69kV LINES: 289

TOTAL 345/115kV TRANSFORMERS: 0

TOTAL 230/115kV TRANSFORMERS: 53

TOTAL 230/69kV TRANSFORMERS: 0 TOTAL 115/69kV TRANSFORMERS: 86

Case Name: 2016MDWGFinal-16S_6_June-Aug_4432_edited.sav Case Title 1: "2016 MDWG FINAL WITH 2015 SERIES MMWG FINAL" Case Title 2: "MDWG 2016S WITH MMWG 2016S" Bus Range: 522800 - 528799 * * * * * * * * * LOSSES BY ELEMENT CLASS * * * * * * * * * ----- AUTOTRANSFORMER LOSSES (MW) ------[345/230 kV] [345/115 kV] [230/115 kV] [230/69 kV] [115/69 kV] [TOTAL 0.853081 0.0 5.503023 0.0 3.201583 9.557688 ----- TRANSMISSION LINE LOSSES (MW) ------[345 kV] [230 kV] [115 kV][69 kV] [TOTAL] 7.400779 40.52235 43.1105 10.91577 101.9494 ----- CASE TOTALS -----TOTAL AREA LOSSES: 111.5071MW TOTAL 345kV LINES: 10 TOTAL 345/230kV TRANSFORMERS: 7 TOTAL 230kV LINES: 79 TOTAL 345/115kV TRANSFORMERS: 0 TOTAL 115kV LINES: 391 TOTAL 230/115kV TRANSFORMERS: 53 TOTAL 230/69kV TRANSFORMERS: 0 TOTAL 115/69kV TRANSFORMERS: 86 TOTAL 69kV LINES: 288

Appendix O Energy Loss Factors

Line No. 1		SOUT EN	HWESTERN PUBL IERGY LOSS FACT 2 MONTHS ENDING	SOUTHWESTERN PUBLIC SERVICE COMPANY ENERGY LOSS FACTOR CALCULATION 12 MONTHS ENDING DECEMBER 2016	_		
3 Loss Factor Calculation 4	u i	Total Ge	Total Generation Inputs =	31,758,276,076 kWh	Vh		
n w ∼ ∞ c	Loss Factor to Gross up to Gen	Loss factor to gross up 1 level 1/(1-loss %)	% loss by level	KWH Flow into each level	KWH Loss by Level	KWH Sales by loss level	Loss Check Loss fac X sales
10 Sales at the Generator Generator Generator	1.000000	1.000000	0.00000%	31,758,276,076	0	8,295,082	8,295,082
13 14 Sales @ 115, 230 & 345 KV 15 Level 2	5 KV 1.029633	1.029633	2.877997%	31,749,980,994	913,763,470	13,821,244,766	14,230,809,712
16 17 Sales @ 69 KV 18 Level 3	1.035919	1.006105	0.606835%	17,014,972,758	103,252,764	4,942,501,116	5,120,030,814
19 20 Sales @ Primary (33kv - 2.4kv) 21 Level 4	. 2.4kv) 1.105898	1.067553	6.327826%	11,969,218,878	757,391,388	3,704,794,414	4,097,124,733
22 23 Secondary Sales @ the Transf. 24 Level 5	Transf. 1.125047	1.017315	1.702074%	7,507,033,076	127,775,281	3,205,486,688	3,606,323,182
25 Sales served by secondary lines 27 Level 6	ary lines 1.128389	1.002971	0.296182%	4,173,771,108	12,361,948	4,161,409,160	4,695,688,321
28 33 32 32	Total	1.064152	6.028491%	31,758,276,076	= 1,914,544,850 + Check usi	4,850 + 29,843,731,226 Check using rounded factors	31,758,271,843 -4,233
33 34 Composite Factors 5 & 6 to Gen. 35	6 to Gen. 1.126935	1.019023	1.866746%	1.019023 1.866746% 7,507,033,076	140,137,228	7,366,895,848	

Loss factor calculation for gross up to a target level equals the product of loss factors for each level up through the target level.

Appendix P Demand Loss Factors

Line No.			SOUTI DEI 12	HWESTERN PUBLI MAND LOSS FACT ? MONTHS ENDINC	SOUTHWESTERN PUBLIC SERVICE COMPANY DEMAND LOSS FACTOR CALCULATION 12 MONTHS ENDING DECEMBER 2016	>		
ა 4 დ	Loss Factor Calculation		Total Ger	Total Generation Inputs = Svetem Peak Hr	6,003,000 Kw	.		
9								
~ 8		Loss Factor to Gross up to Gen	gross up 1 level 1/(1-loss %)	% loss by level	KW Flow into each level	KW Loss by Level	KW Demand by loss level	Loss Check Loss fac X sales
6 5								
2 7 2	Sales at the Generator @ Generation	1.000000	1.000000	%00000000	6,003,000	0	0	0
ω 4 ή	Sales @ 115, 230 & 345 KV	1.023667	1.023667	2.311973%	6,003,000	138,788	2,244,415	2,297,533
<u>ი</u> 9	Level z							
71 87	Sales @ 69 KV Level 3	1.030961	1.007126	0.707520%	3,619,798	25,611	1,090,485	1,124,247
2 2 2 2	Sales @ Primary (33kv - 2.4kv) Level 4	1.131015	1.097049	8.846390%	2,503,702	221,487	436,754	493,975
2 2 2 2	Secondary Sales @ the Transf. Level 5	1.161769	1.027192	2.647180%	1,845,461	48,853	640,746	744,399
78 7 8 8	Sales served by secondary lines Level 6	1.166539	1.004106	0.408905%	1,155,862	4,726	1,114,734	1,300,380
53	Total		1.078990	7.320754%	5,966,598	= 439,465 +	5,527,133	5,960,535
3 8	Composite Factor Levels 5 and 6	1.164833	1.029901	2.903288%	1,845,461	53,579	1,755,480	

12 MONTHS ENDING DECEMBER 2016

s Level	Energy Loss Factors	1.126935	1.126935	1.126935	1.126935	1.105898		1.029633	1.035919	1.126935	1.126935	1.126935	1.126935	1.105898	1.126935	1.105898	1.029633	1.035919
Rate Class Loss Factors by Loss Level	Demand Loss factors E	1.164833	1.164833	1.164833	1.164833	1.131015		1.023667	1.030961	1.164833	1.164833	1.164833	1.164833	1.131015	1.164833	1.131015	1.023667	1.030961
Rate (Loss Level	9	9	9	5	4		7	လ	9	9	9	9	4	2	4	2	က
		Residential Lighting	Residential Space Heating	Small General Service	General Service - Secondary	General Service - Primary	Large General Service	Transmission Backbone	Sub-Transmission	Street Lighting	Area Lighting	Small Municipal and School	Large Municipal	Large Municipal - Primary	Large Schools	Interruptible Service -SAS 4	Wholesale - Service -115 kV	Wholesale - Service -69 kV
Line No.	- N W	4	2	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20

* For Levels 5 & 6, the Composite Factors used in billing applicatons are stated.